

EX.6

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ONTARIO HYDRO'S PLAN
TO SERVE CUSTOMERS'
ELECTRICITY NEEDS

PLAN
ANALYSIS

PROVIDING THE BALANCE OF POWER

This "Plan Analysis" is one of a series of documents issued under the title, "Providing the Balance of Power: Ontario Hydro's Plan to Serve Customers' Electricity Needs." It provides technical details and supporting analyses for Hydro's proposed plan to meet the future electricity needs, and the alternatives that were considered. A more comprehensive discussion of the background to, and the elements of, these plans is provided in the "Demand Supply Plan" Report.

Another document, "Overview", presents in a more abbreviated and somewhat different form the main features of the proposed plan, the alternatives, and the considerations that went into their development.

A fourth document, "Environmental Analysis", analyzes the environmental impact of the Proposed Demand/Supply plan and the alternatives. These documents will be filed with the Minister of the Environment for a public hearing before the Environmental Assessment Board. Prior to that hearing, these documents will be subject to government review. As well, they will be the focus of a public information program held early in 1990.

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3. RELIABILITY
4. FORMULATION AND DESCRIPTION OF PLANS
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6. ENERGY PRODUCTION
7. ACID GAS CONTROL
8. COSTS
9. FINANCIAL IMPACT ASSESSMENT

1. INTRODUCTION

This report focuses on the formulation, description and analysis of the five Major Supply Cases. The rationale for selecting Candidate Plans or the Proposed Plan is provided in the Demand/Supply Report (DSP). It's recommended that the DSP Report be read first. Keeping a copy close at hand would also be useful, as there are numerous references to the DSP Report in this analysis. Definitions of many of the technical terms used in this report are provided in the glossary of the DSP Report.

There are 4 major differences between this report and the DSP Report:

- . Cases and evaluation results are described for two load forecast paths that branch from the median forecast; one lies between the upper and median forecasts; the other lies between the lower and median forecasts. In all, five load forecast paths are assumed: median, branch upper, upper, branch lower and lower.
- . Results are more fully presented. The DSP Report often summarizes results by five year periods. This report provides annual results. This report also provides more detailed results, such as fossil energies by fuel type, and costs under specific conditions.
- . Certain aspects of plan development are covered in more detail, such as reliability, acid gas control and transmission.
- . The main models used to simulate the electricity system and to carry out the economic evaluation are described.

During the formulation of plans, certain data was updated, specifically customer response to demand management initiatives, the non-utility generation forecast, hydroelectric sites and the cost of options.

The data used in this analytic work and the DSP Report were current at the time the work was carried out. Because these documents were completed at different times, there are some differences between the data used in each report. These differences are noted and explained in this report. The differences are small and would not affect the nature of the Cases developed or the results of the evaluation of the Cases.

Along with this introduction, there are eight chapters:

Chapter 2 -- System Modelling: describes the principal model used to simulate how a balanced mix of demand and supply options meet customer needs. This model receives data from many sources and, in turn, is the source of much data for subsequent evaluations in areas such as economics, finance and acid gas.

Chapter 3 -- Reliability: describes the generation reliability standard used to assess Hydro's ability to meet customer needs continually. Using two demand/supply cases, the standard is applied in a reliability analysis to find the generating reserve margin to apply in formulating all cases.

Chapter 4 -- Formulation and Description of Plans: begins with some background on how Hydro arrived at the five Cases presented in the DSP Report. However, the main purpose of this chapter is to describe how each of the five Cases respond to changes in load forecast, particularly the branch upper and branch lower forecasts. By considering load forecast changes, Hydro ensures its plans have flexibility.

Chapter 5 -- Transmission: describes the radial and inter-area transmission associated with certain sites and the sequence in which sites may be developed.

Chapter 6 -- Energy Production: describes, year by year, the energy provided by Non-Utility Generators (NUGs), the Manitoba Purchase, hydraulic, nuclear and fossil generation for all five load paths and five Cases.

Chapter 7 -- Acid Gas Control: describes acid gas control planning and the control plan assumed in the DSP Report. Energy derived from oil, natural gas and coal is presented. Energy from coal is further divided by application: e.g. low sulphur content, stations equipped with scrubbers.

Chapter 8 -- Costs: begins with the source of cost data and traces the application of those data. The principal cost model is described -- how it receives the data inputs and the many cost results that are derived from it. The principles of the allocation of present value costs and the cost risk assessment method are explained. Specific results are also presented for the branch load forecast paths.

Chapter 9 -- Financial Impact Assessment: deals with rate and borrowing requirements.

2. SYSTEM MODELLING

- 2.0 INTRODUCTION**
- 2.1 MODELLING OVERVIEW**
- 2.2 DEMAND SUBMODEL**
- 2.3 SUPPLY SUBMODEL**
- 2.4 FINANCE SUBMODEL**
- 2.5 ACID GAS AND SECONDARY NUCLEAR
SALES MODELLING**
- 2.6 REVIEW**

2.0 INTRODUCTION

This chapter describes the computer modelling of the Ontario electric supply system as used for the Demand/Supply Plan. These models simulate the load to be supplied and schedule generation to supply it. They also track associated demand and supply costs, and determine acid gas emissions, coal blending and secondary nuclear sales. Additional models used for costing are discussed in Chapters 8 and 9.

2.1 MODELLING OVERVIEW

The primary model used for evaluation of the Demand/Supply Plans was the Load Management Strategy Testing Model (LMSTM) developed for the Electric Power Research Institute in 1984 (EPRI EA-2396, 1984). It was first used by Ontario Hydro in the preparation of the Draft Demand/Supply Planning Strategy. For the Demand/Supply Plan, the original LMSTM model was enhanced to determine fuel blending to meet acid gas limits and secondary nuclear sales.

The enhanced version of LMSTM is one of several models used to analyze the plan. The primary functions of LMSTM were modelling of demand management and generation dispatch, and the calculation of fuel costs. It was also used for the calculation of costs common to all plans. The costs of new supply resources were entered directly into the Risk Assessment Model (RAM) (see Chapter 8). The corporate financial and rate impacts were also obtained separately (see Chapter 9).

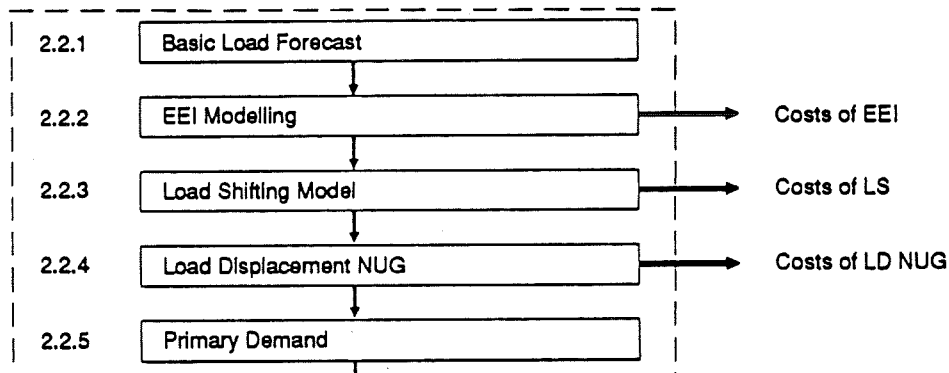
LMSTM is an integrated planning model which models both demand and supply options. It consists of three submodels--demand, supply and finance. The logic flow among these submodels, and the sections of this chapter in which each submodel is described, are shown in Figure 2.1-1. A more comprehensive discussion is in the EPRI report referenced above.

The demand submodel accepts as input the basic load forecast, then subtracts the impact of demand management programs and load displacement non-utility generation, to derive the primary load forecast. This submodel also calculates the costs of demand management. This submodel is described in more detail in Section 2.2.

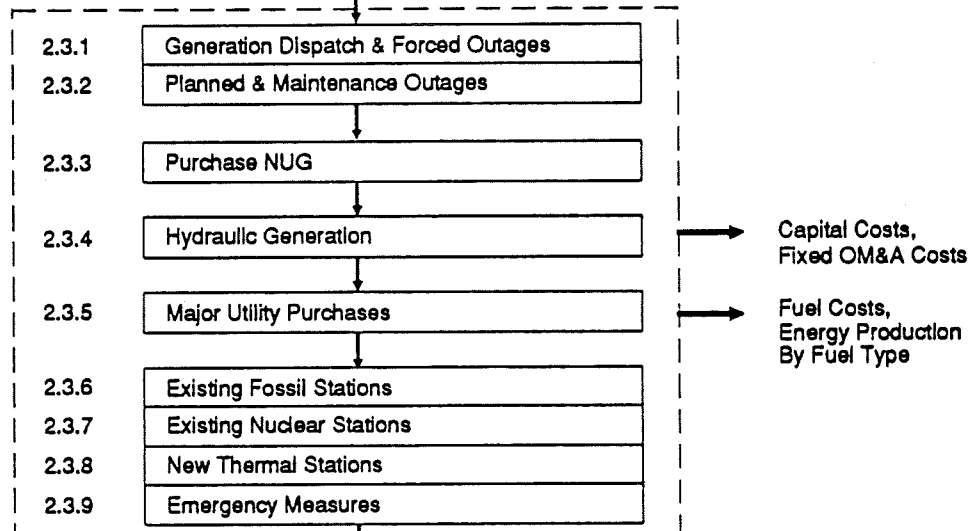
The supply submodel starts with the primary demand calculated in the demand submodel and the characteristics and costs of existing and new generating units. It simulates the scheduling of the production from these units; produces the capital, fixed operating and fuel costs of these units; and calculates expected energy generation by fuel type. Section 2.3 provides more detail on the supply submodel.

Figure 2.1-1
System Modelling Overview

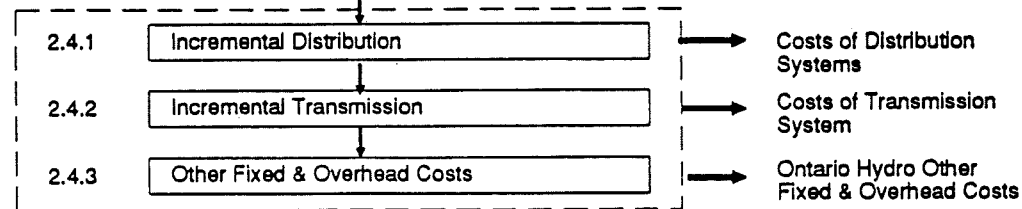
2.2 DEMAND SUBMODEL



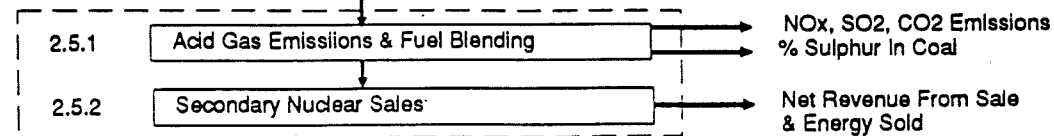
2.3 SUPPLY SUBMODEL



2.4 FINANCE SUBMODEL



2.5 ACID GAS & SECONDARY SALES



The use of the LMSTM finance submodel is described in Section 2.4. This submodel includes the calculation of overhead and other fixed costs, transmission and distribution costs and fixed costs related to existing assets such as existing generation stations or office buildings.

Finally, acid gas emission calculations, coal blending and secondary nuclear sales are calculated, based on fuel cost and energy production by fuel type from the supply submodel.

2.1.1 Modelling Constraints

LMSTM has an annual resolution of demand, generation available and costs. This results in a number of constraints. The load shapes represent a seasonal pattern over a year with average load growth. As load growth from year to year changes, the relative demand across months would also change. For example, with high load growth, the December peak would be much higher than the preceding January peak. With low load growth, they would be almost the same. This changing of the seasonal pattern within a year cannot be modelled. However, it is quite small, compared to the effect of annual load growth.

The annual resolution also means that generating units may only be added as of January first of each year. Thermal units are usually scheduled to come on line in October. For modelling purposes these units were added as of the following January. In general, units with in-service dates before July first were modelled as starting the preceding January. Those with later in-service dates were modelled as starting the following January.

Starting units only in January also constrained the costing of major outages, such as rehabilitations and retubing. Therefore, the costs of these outages were modelled either as a fixed OM&A expense for shorter outages, or as a capital expense, if the duration exceeded a full year. The costs of outages spanning a year or more, such as nuclear retubing, were modelled as a capital cost and depreciated over the remaining life of the station. The costs of shorter outages were expensed as fixed OM&A.

All projects of a particular type are modelled with a similar construction expenditure pattern. These patterns actually do change with in-service date, because the underlying inflation rate is forecast to change from year to year over the planning period. This effect is insignificant, however, except for projects with long construction schedules, such as major new supply. These capital costs were used for calculation of the avoided costs. However, this constraint did not impact on the main financial analysis, because the major capital programs were modelled directly in RAM to assist with risk assessment.

Another constraint on financial modelling of capital costs is that the real discount rate cannot change over the planning period. This restriction is reflected through the calculation of the levelized capital cost, which is an Ontario Hydro modification to the original LMSTM program. The real discount rate actually varies from 6% in 1992 to 4.5% beyond 2010. A constant real discount rate of 5% was used for the calculation of all capital costs in the system modelling.

The inter-area transmission was included directly in RAM to reduce the number of system simulations required. The inter-area transmission alters the cost for a specific site for a specific type of new generation, but has no effect on other costs or demand or supply modelling. Rather than run the production simulation for each combination of new generation siting, the costs of inter-area transmission were included as part of the risk analysis and calculation of final costs.

2.2 DEMAND SUBMODEL

LMSTM is specifically designed for modelling the impact of demand management programs on utility load. Demand is represented by daily load shapes (24 hourly demands) for 4 typical days in each season. The typical days, or day types, represent high-demand weekdays, mid-demand weekdays, other (low-demand) weekdays, and weekends and holidays. The number of days represented by each day type in each season is shown in Figure 2.2-1. The fractional numbers of days in each type is due to averaging over the seven days of the week on which a year may start.

In this type of load representation the differences in energy demand across the day types reflect the effects of day-to-day weather variation (high-demand weekdays would reflect colder temperatures in winter and hotter temperatures in summer) and the effects of the day of the week (weekday versus weekend). If weather or day of the week alters the relative demands among the hours within a day, this is modelled by having different load shapes for each of the day types. Differences from season to season represent differences in weather over a year and influences such as the hours of sunlight, daylight savings time, and the summer vacation period.

Before proceeding it is necessary to define some terminology. The load shape is the pattern of how the demand for electricity varies from hour to hour. It must be scaled up or down from year to year by the demand or energy forecast. To illustrate, the basic loads for the three years shown for each day type on Figure 2.2-2 all have the same load shape. That is, the ratio of the load in each hour to average load for the day is the same for all three years. They differ because the load shape has been scaled by the forecast demand in each of the three years. The primary demands also shown on Figure 2.2-2 have different load shapes in the three years as a result of load reductions from efficiency improvements, load shifting and load displacement non-utility generation.

Figure 2.2-1

**Season and Day-Type Classification
For System Simulation
(Number of Days in Each)**

Day Type	Season				Total
	Winter	Spring	Summer	Fall	
HIGH Weekday	37.51	20.13	37.82	20.13	115.59
MID Weekday	65.34	31.72	65.88	31.72	194.66
LOW Weekday	12.10	6.10	12.20	6.10	36.50
WEEKEND	6.05	3.05	6.10	3.05	18.25
Total	121.00	61.00	122.00	61.00	365.00

Winter = January, February, March, December

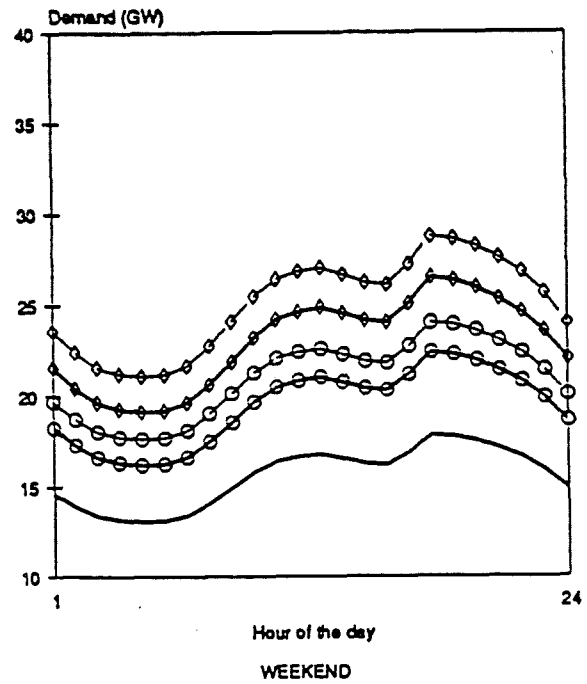
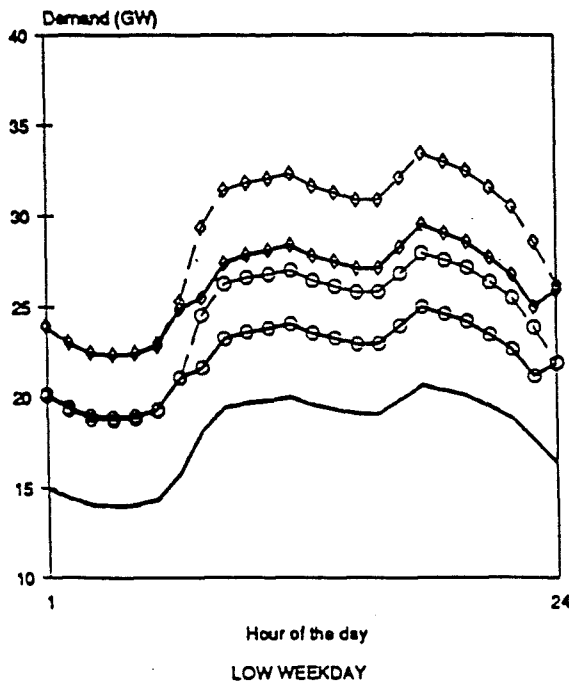
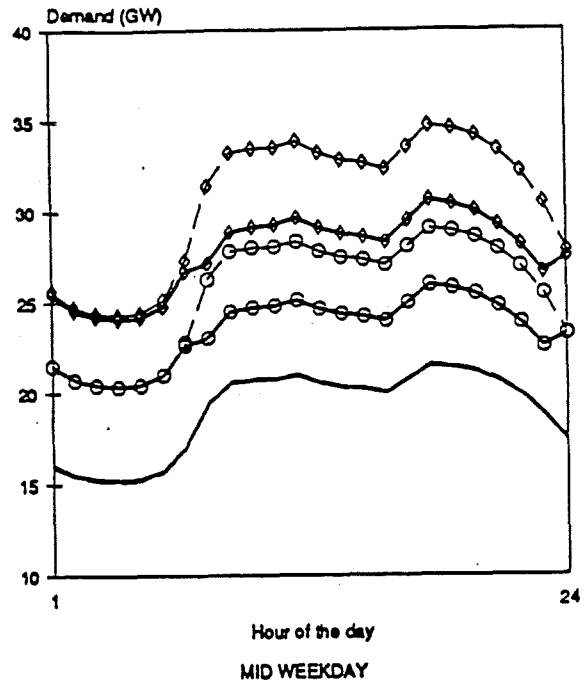
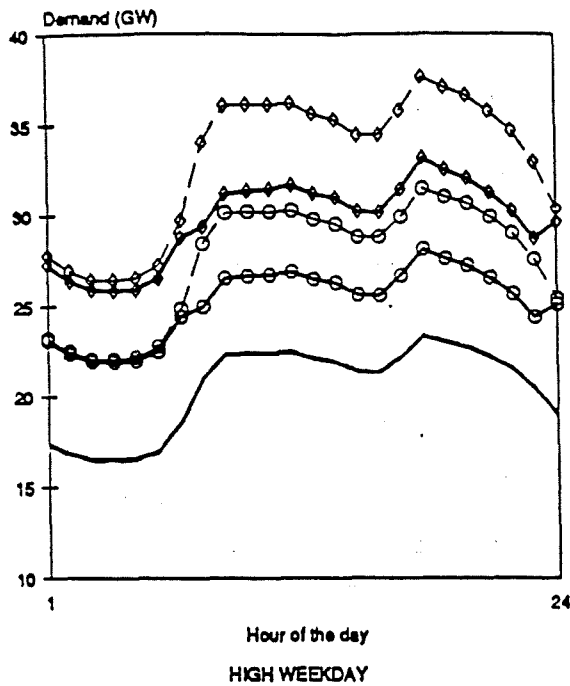
Spring = April, May

Summer = June, July, August, September

Fall = October, November

Figure 2.2-2(a)
Basic & Primary Load Shapes
in System Simulation

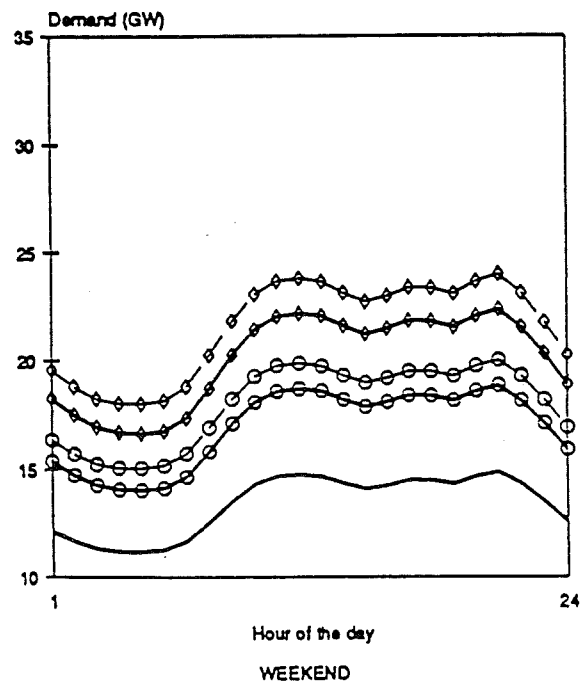
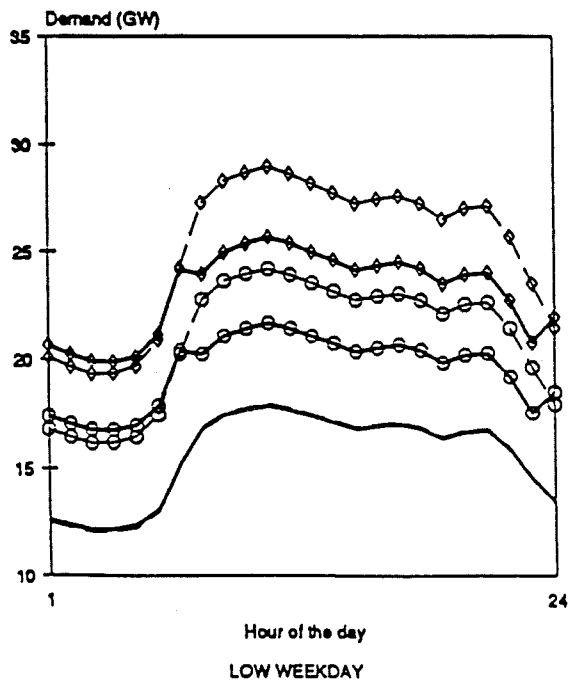
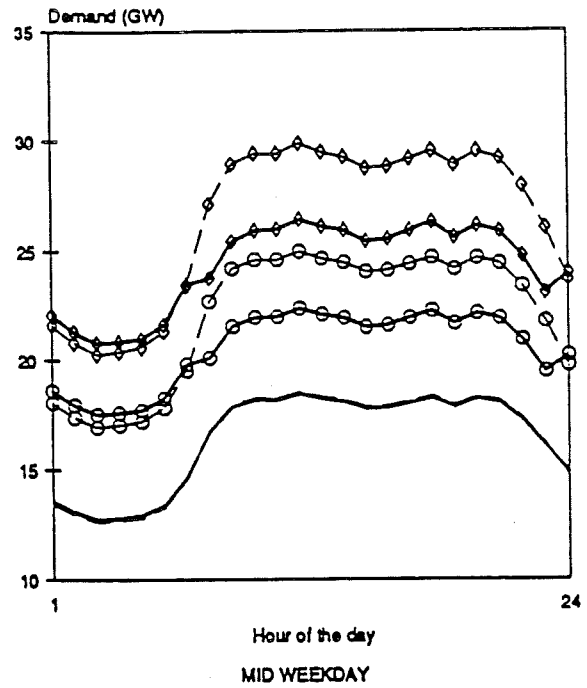
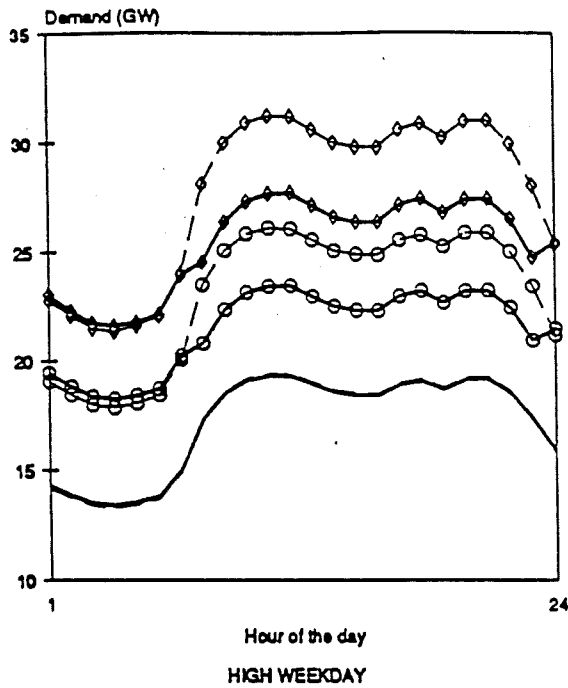
WINTER



—◇— BASIC 2010 —○— BASIC 2000 - - - BASIC 1989
 —◇— PRIMARY 2010 —○— PRIMARY 2000 ——— PRIMARY 1989

Figure 2.2-2(b)
Basic & Primary Load Shapes
in System Simulation

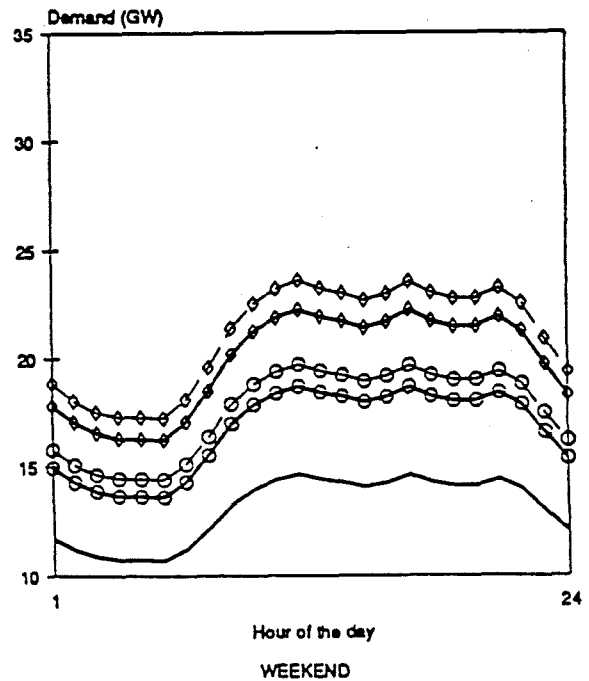
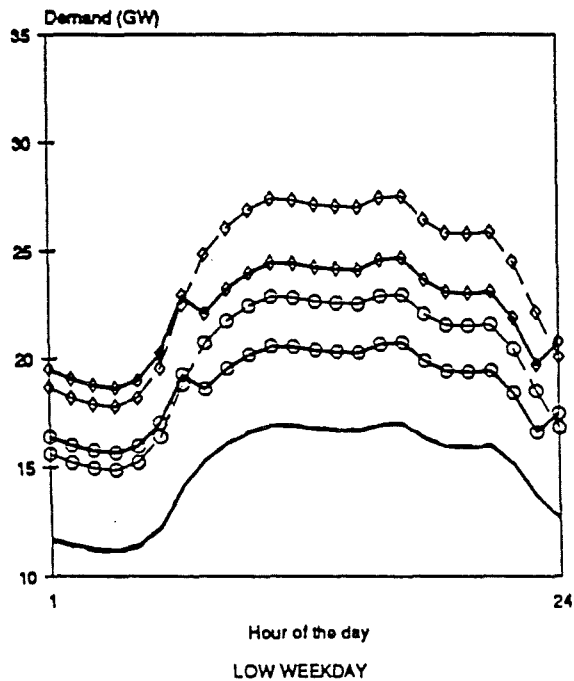
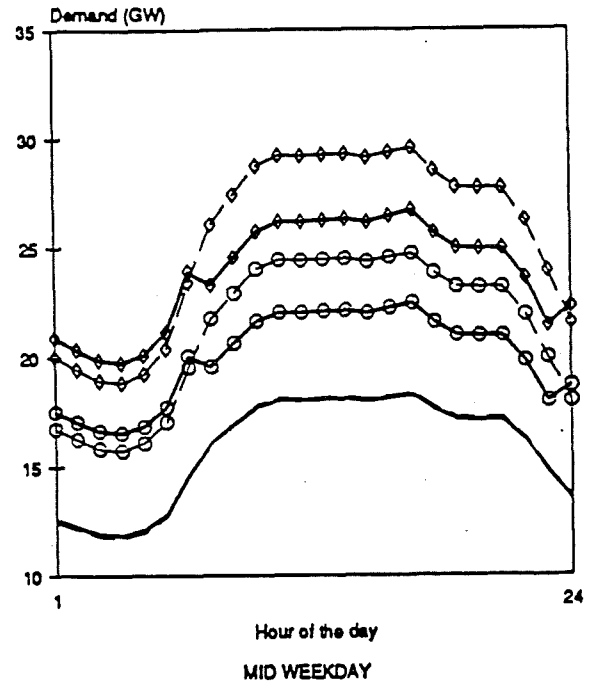
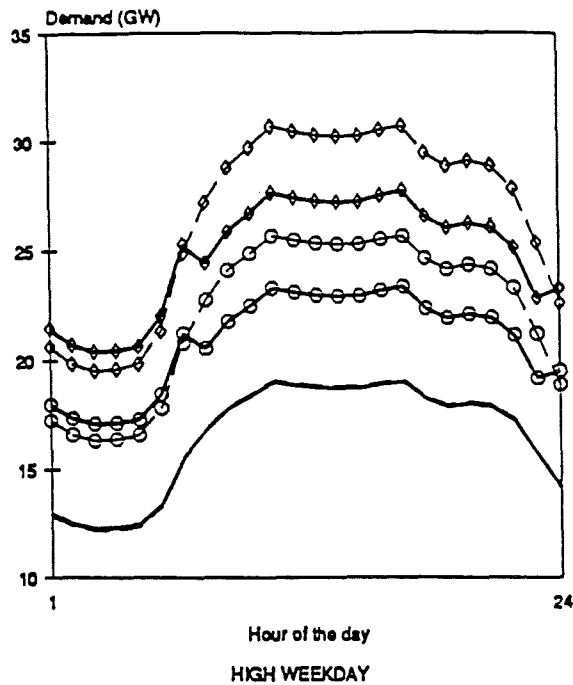
SPRING



◇ BASIC 2010 ○ BASIC 2000 - - BASIC 1989
 ◇ PRIMARY 2010 ○ PRIMARY 2000 — PRIMARY 1989

Figure 2.2-2(c)
Basic & Primary Load Shape
in System Simulation

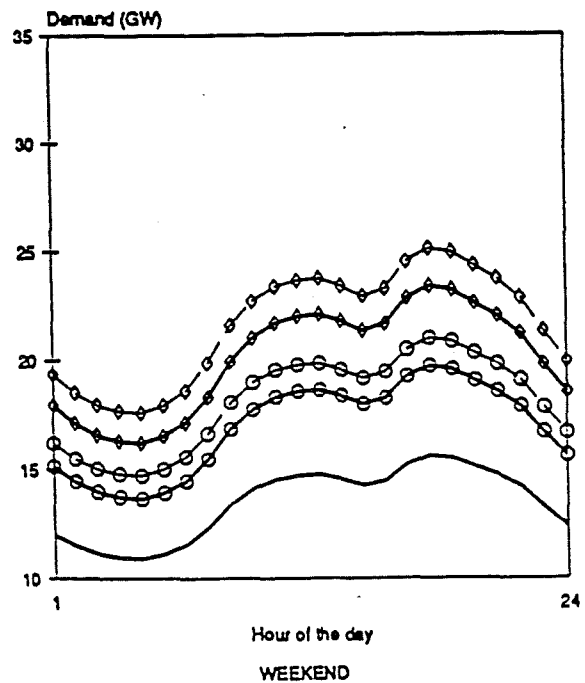
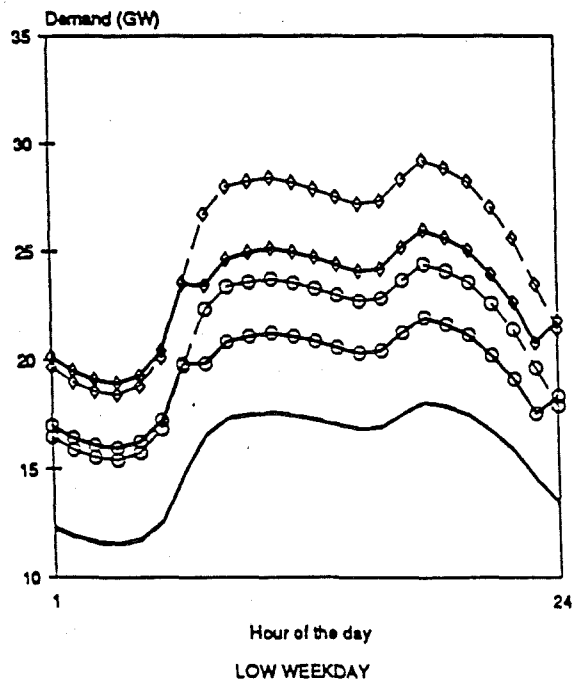
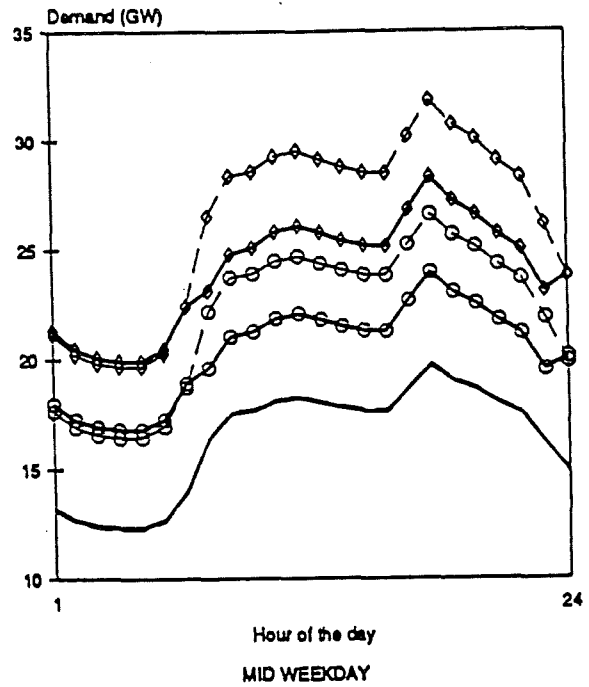
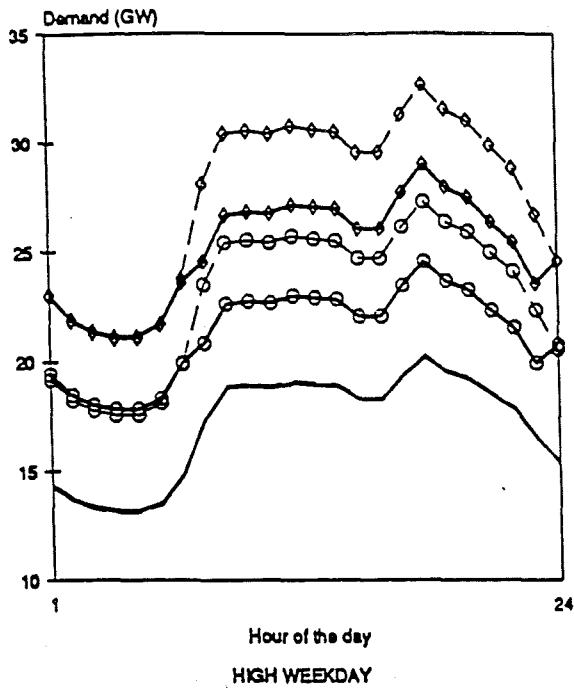
SUMMER



◇ BASIC 2010 ○ BASIC 2000 - - BASIC 1989
 ◇ PRIMARY 2010 ○ PRIMARY 2000 — PRIMARY 1989

Figure 2.2-2(d)
Basic & Primary Load Shape
in System Simulation

FALL



—◇— BASIC 2010 —○— BASIC 2000 - - - BASIC 1989
 —◇— PRIMARY 2010 —○— PRIMARY 2000 — PRIMARY 1989

The electricity basic demand for each day type is built from five different end-use load shapes representing different appliances or customer classes:

- residential domestic load,
- residential space heating,
- residential water heating,
- general class load (commercial & small industrial customers),
- direct customers (mainly large industrial customers).

To model demand management, the above end-use shapes were used and two other specific shapes were created:

- flat load (constant throughout the day)
- off-peak load (11 PM to 7 AM for recovering shifted load).

Demands created by adding together these various load shapes may also be grouped into customer classes:

- municipal residential
- rural residential
- general class
- direct customers.

These classes were used in this study to calculate distribution costs, which are only applicable for the loads in the first three classes.

The demand in each hour is created in stages. First, the basic load forecast is modelled as a sum of the five end-use shapes. This provides a separate estimate of basic load for each of the 384 typical hours (24 hours per day times 4 typical days times 4 seasons) (Section 2.2.1).

Next, load shapes (384 hours each) for electrical efficiency improvements (Section 2.2.2), load shifting (2.2.3) and load displacement non-utility generation (2.2.4) are created separately. Finally, these are subtracted from the basic load to create the primary load shape. This primary load is fed into the supply submodel, where it is met by supply resources.

2.2.1 Basic Load Forecast

The basic load forecast modelled is from the Load Forecast Report No.881212 published in April 1989. The five end-use loads were initially combined in the proportion of total system load forecast to come from each end-use. The proportion of energy consumed under these load shapes was modified to create the same one-hour December peak demand and annual energy as predicted in the load forecast. The resulting load shapes are shown in Figure 2.2-2 for 1989, 2000 and 2010.

The long-run (post 1994) basic load forecast is prepared using only one annual load shape for all years. So, basic load in LMSTM was also modelled using only one load shape for all years. The short-run forecast (up to 1994), which is also modelled in

shape for all years. The short-run forecast (up to 1994), which is also modelled in LMSTM, has different load shapes so the modelling has some deviations from the load forecast in the early years. The maximum deviation is in 1989, when modelled peak demand is 0.6% higher than the forecast and energy use is 0.1% lower. After 1995, differences in both of these indicators are less than 0.03%.

2.2.2 Electrical Efficiency Improvements

Electrical efficiency improvements (EEI) are modelled as a load reduction from the basic load shape. They were compiled from the general class end-use shape and the residential domestic and space heating end-use shapes. The proportion of efficiency improvement modelled with each of these load shapes was determined so that the one-hour and sixteen-hour winter peaks and the annual energy reduction were as specified for the year 2000, a benchmark year in the demand management plan.

The effect of EEI programs is shown for the year 2000 in Figure 2.2-3. The load shape of EEI was not changed from year to year, but the load reduction from EEI was increased annually. Yearly peak reductions from EEI programs, as produced by the system simulation, are shown in Figure 2.2-4.

The incremental capital cost of EEI is estimated to be 900 \$89/kW (\$900 per kW in 1989 dollars) with Hydro offering an incentive of 351 \$89/kW. After the 11-year life assumed for all EEI, the full \$900 is paid by the participant. Hydro also incurs an administration OM&A cost of 350 \$89/kW at the time of the first investment in EEI. This administration cost is not incurred when the equipment is replaced. All costs were escalated by the Ontario CPI.

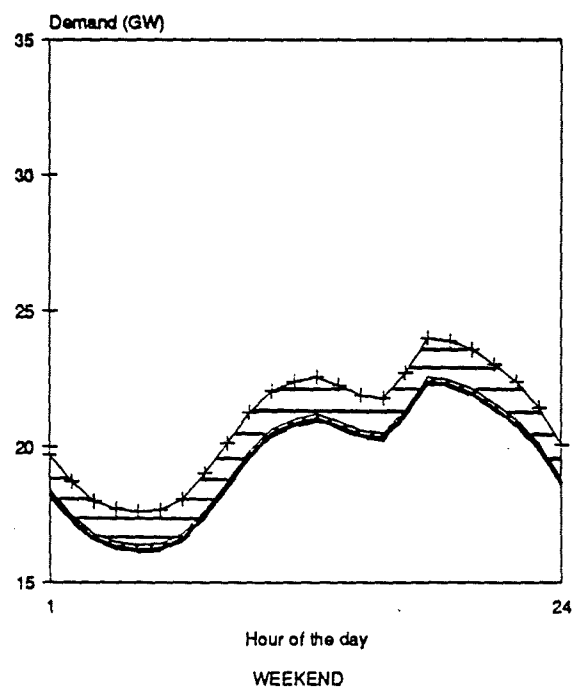
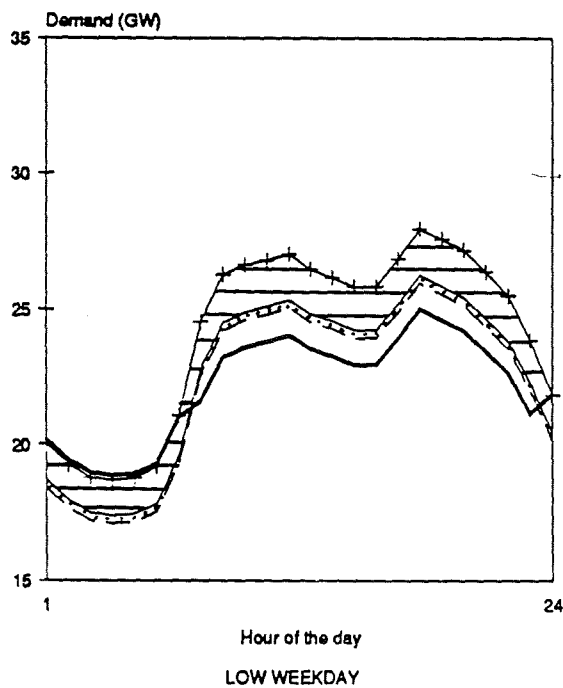
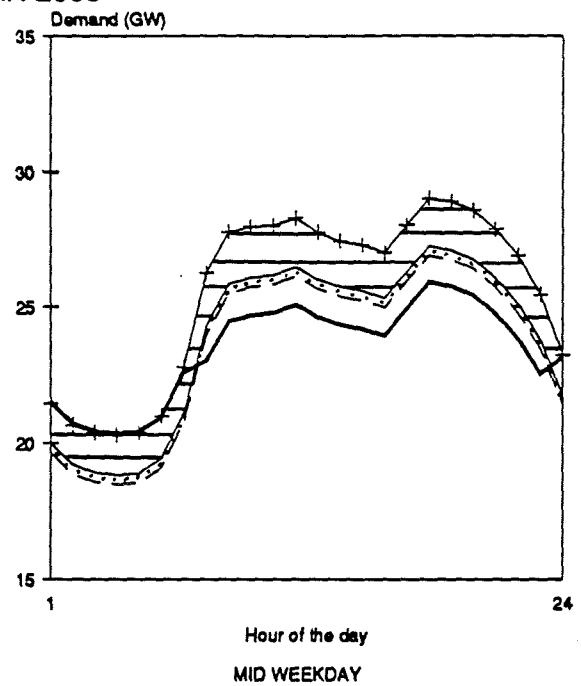
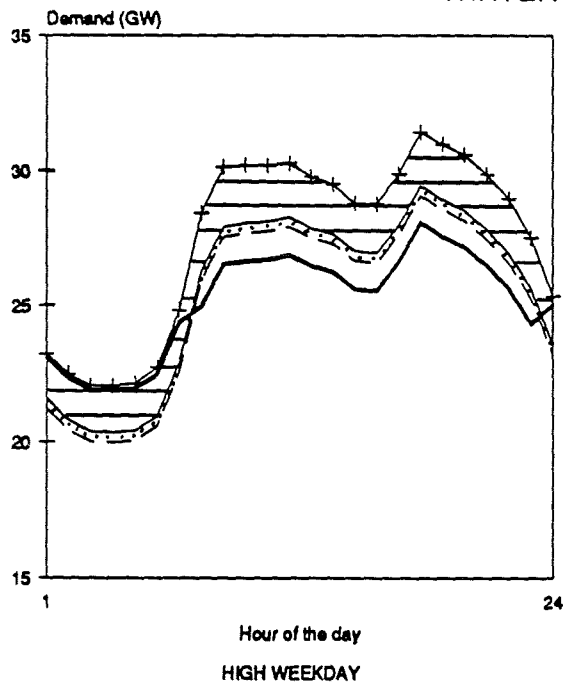
2.2.3 Load Shifting

Modelling load shifting is more complicated because the load must first be removed from the peak period (7 AM to 11 PM) of the three typical weekdays, and then be added to the off-peak (11 PM to 7 AM) period of these days. Some of the energy removed from the peak periods is also recovered on the weekends, which are off peak for all hours. The total amount of energy consumed is not changed as with EEI, but is only shifted to weekday nights and weekends.

Two load shapes were used to model the load removed from the peak periods--general class and direct customer load. This reflects that the majority of load shifting is expected to come from commercial and industrial customers. The proportion of the load shifting represented by each of the load shapes is shown in Figure 2.2-5. The division between these reflects the proportion of load shifting expected to come from direct customers and large users (direct customer end-use shape), versus smaller commercial, industrial and residential customers.

Figure 2.2-3(a)
Load Shape Modifications
for EEI, LD NUG and LS

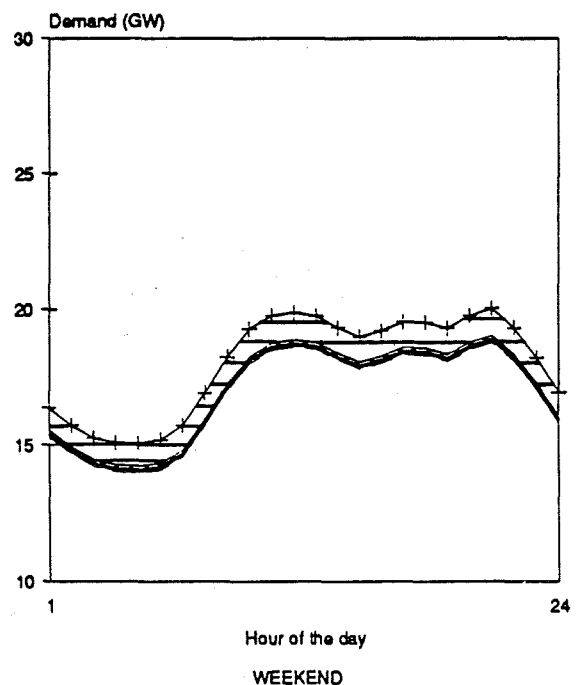
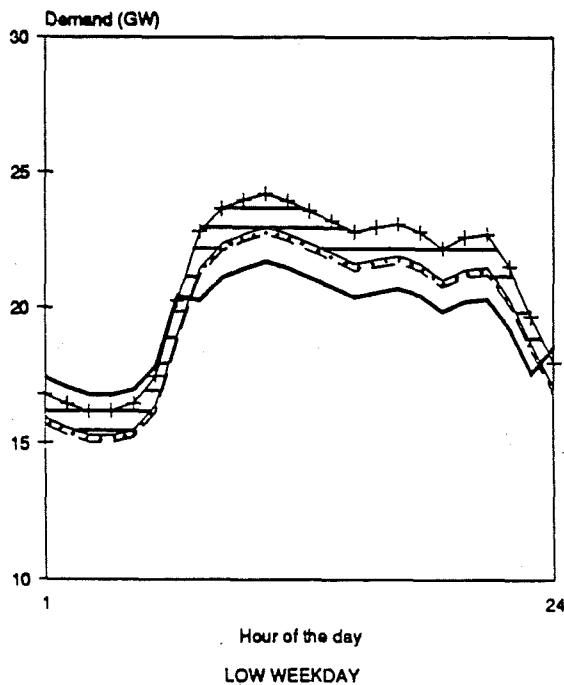
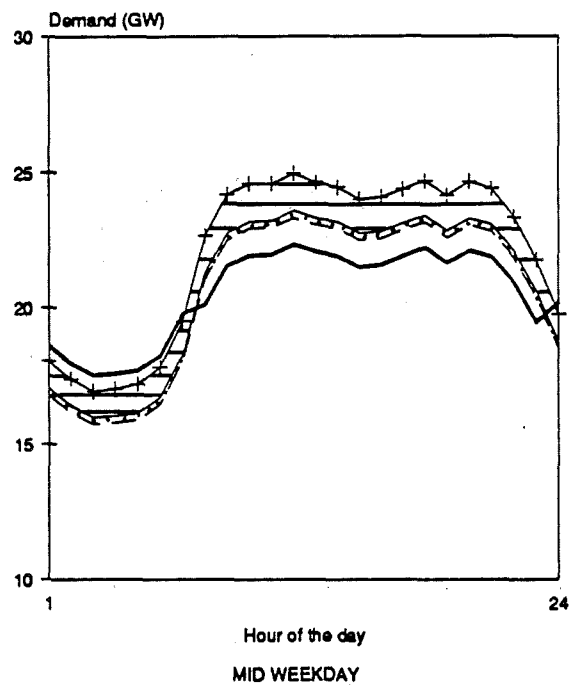
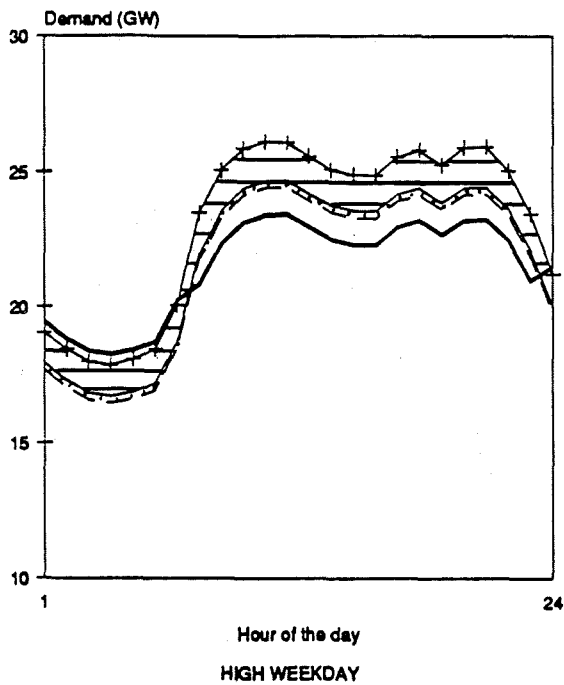
WINTER - YEAR 2000



++ BASIC DEMAND	EEI
— PRIMARY DEMAND	LD NUG

Figure 2.2-3(b)
Load Shape Modifications
for EEI, LD NUG and LS

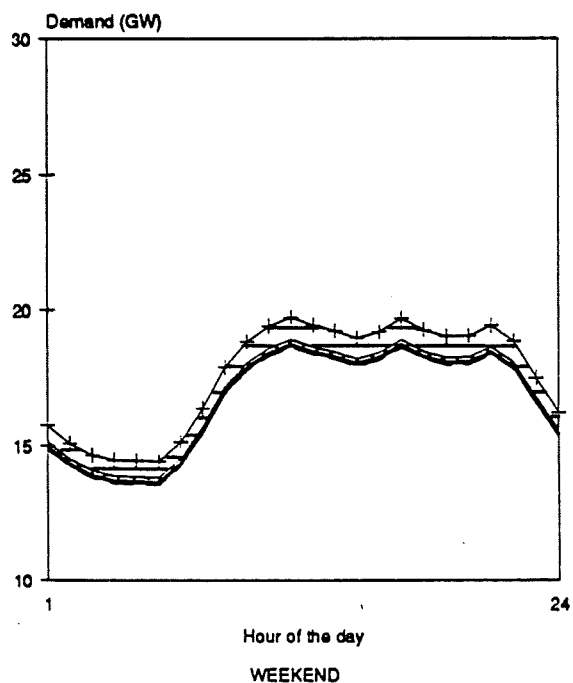
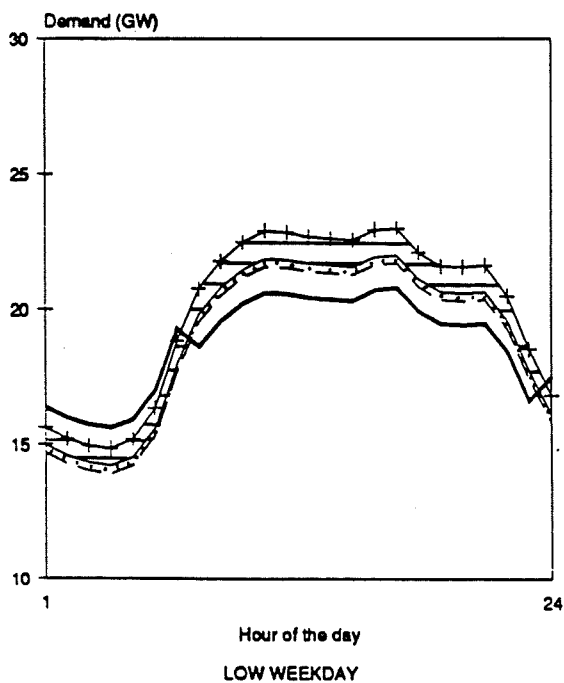
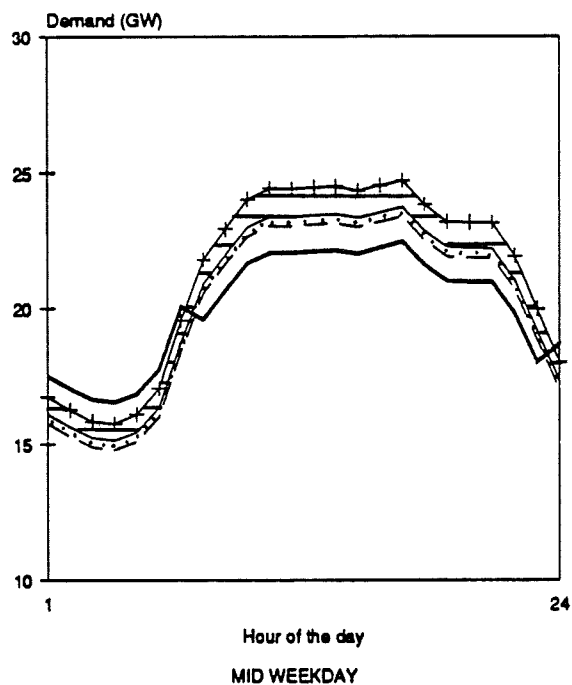
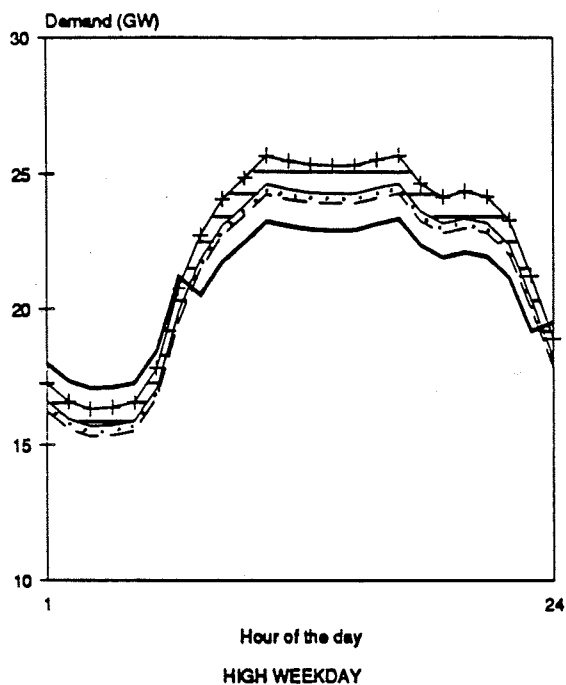
SPRING - YEAR 2000



++ BASIC DEMAND	EEI
— PRIMARY DEMAND	LD NUG

Figure 2.2-3(c)
Load Shape Modifications
for EEI, LD NUG and LS

SUMMER - YEAR 2000



++ BASIC DEMAND
— PRIMARY DEMAND

EEI
LD NUG

Figure 2.2-3(d)
Load Shape Modifications
for EEI, LD NUG and LS

FALL - YEAR 2000

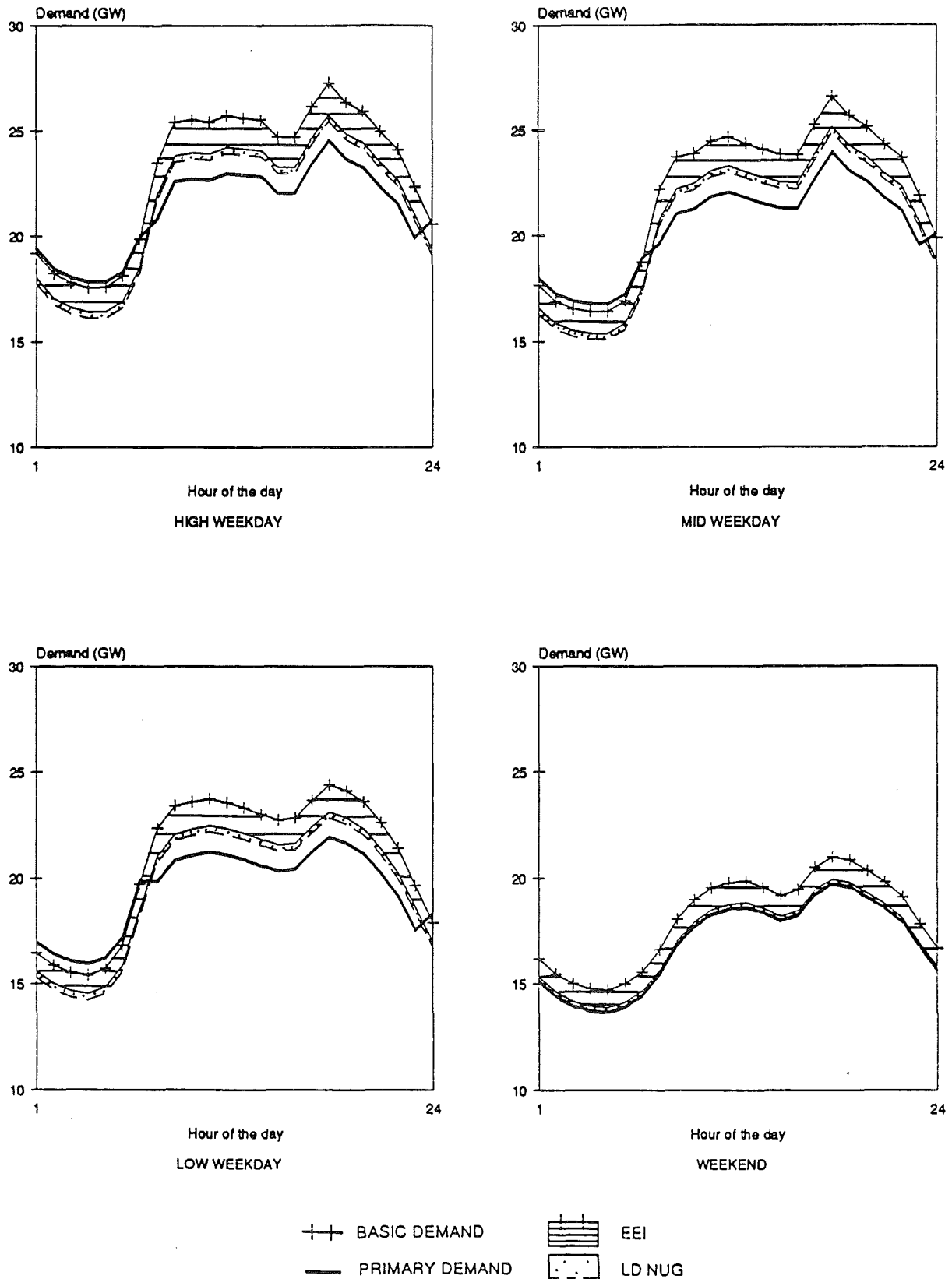


Figure 2.2-4
Demand Management Savings as Produced By System Simulation
 (Cumulative Values As Of December One-Hour Peak)

YEAR	LOWER LOAD FORECAST				BRANCH LOWER LOAD FORECAST				MEDIAN LOAD FORECAST				BRANCH UPPER LOAD FORECAST				UPPER LOAD FORECAST			
	EEI (MW)	LS (MW)	LD NUG (MW)	TOTAL (MW)	EEI (MW)	LS (MW)	LD NUG (MW)	TOTAL (MW)	EEI (MW)	LS (MW)	LD NUG (MW)	TOTAL (MW)	EEI (MW)	LS (MW)	LD NUG (MW)	TOTAL (MW)	EEI (MW)	LS (MW)	LD NUG (MW)	TOTAL (MW)
1989	14	78	23	115	14	81	23	118	14	81	23	118	14	81	23	118	14	84	23	121
1990	36	161	90	287	45	172	90	307	45	171	90	306	45	172	90	307	56	180	90	326
1991	62	246	144	452	77	265	144	486	78	266	144	488	77	265	143	485	98	282	144	524
1992	101	387	210	698	126	424	210	760	126	423	210	759	126	424	210	760	158	455	210	823
1993	146	519	272	937	183	581	275	1039	183	582	275	1040	183	581	275	1039	229	735	276	1240
1994	251	576	288	1115	314	656	300	1270	314	656	300	1270	314	656	300	1270	393	728	307	1428
1995	400	620	288	1308	500	717	325	1542	500	717	325	1542	500	717	325	1542	625	795	342	1762
1996	640	663	288	1591	779	765	240	1784	800	776	340	1916	822	787	340	1949	1000	870	362	2232
1997	880	707	288	1875	1051	813	354	2218	1100	836	354	2290	1154	858	354	2366	1375	946	369	2690
1998	1120	749	288	2157	1315	858	364	2537	1400	893	364	2657	1495	927	364	2786	1749	1017	362	3128
1999	1360	790	288	2438	1574	899	368	2841	1700	946	368	3014	1830	989	368	3187	2125	1100	355	3580
2000	1600	800	288	2688	1809	950	340	3099	2000	1000	368	3368	2185	1050	348	3583	2500	1200	348	4048
2001	1663	820	288	2771	1882	965	320	3167	2100	1020	361	3481	2314	1074	341	3729	2624	1220	341	4185
2002	1725	840	288	2853	1956	980	300	3236	2200	1040	355	3595	2447	1098	334	3879	2750	1240	334	4324
2003	1788	860	281	2929	2028	995	281	3304	2300	1060	347	3707	2580	1122	327	4029	2875	1260	327	4462
2004	1850	880	274	3004	2102	1010	274	3386	2400	1080	339	3819	2714	1146	320	4180	3000	1280	320	4600
2005	1913	900	267	3080	2177	1025	267	3469	2500	1100	332	3932	2850	1170	313	4333	3125	1300	313	4738
2006	1974	920	260	3154	2253	1040	260	3553	2600	1120	325	4045	2980	1194	306	4480	3250	1320	306	4876
2007	2038	940	253	3231	2328	1055	253	3636	2700	1140	318	4158	3134	1218	299	4651	3375	1340	299	5014
2008	2100	960	246	3306	2403	1071	246	3720	2800	1160	311	4271	3252	1242	292	4786	3500	1360	292	5152
2009	2163	980	239	3382	2476	1085	239	3800	2899	1180	303	4382	3390	1266	285	4941	3625	1380	285	5290
2010	2225	1000	232	3457	2548	1102	232	3882	3000	1200	296	4496	3532	1290	278	5100	3750	1400	278	5428
2011	2288	1020	225	3533	2619	1115	225	3959	3101	1221	290	4612	3674	1314	271	5259	3875	1420	271	5566
2012	2350	1041	218	3609	2688	1131	218	4037	3200	1240	282	4722	3819	1338	264	5421	4000	1440	264	5704
2013	2412	1060	211	3683	2755	1145	211	4111	3298	1260	275	4833	3965	1362	252	5579	4123	1460	252	5835
2014	2475	1080	204	3759	2823	1161	204	4188	3400	1280	268	4948	4117	1387	240	5744	4250	1480	240	5970

Figure 2.2-5

Modelling of Load Shifting
(Percent of Load Shifting From Each Group)

Year	Direct & Large Users	General Class
1989	100%	0%
1990	100%	0%
1991	91%	9%
1992	69%	31%
1993	55%	45%
1994	53%	47%
1995	52%	48%
1996	50%	50%
1997	47%	53%
1998	45%	55%
1999	43%	57%
2000	42%	58%
2001	42%	58%
2002	42%	58%
2003	42%	58%
2004	42%	58%
2005	42%	58%
2006	42%	58%
2007	42%	58%
2008	42%	58%
2009	42%	58%
2010	43%	58%
2011	43%	57%
2012	43%	57%
2013	43%	57%
2014	43%	57%

The costs of load shifting were approximated by assuming that all shifting comes from the implementation of TOU rates. Only the smaller customers require an investment in metering equipment by Hydro to convert them to TOU rates. All participants incur costs to shift load. The total costs by year are shown in Figure 2.2-6.

The meter conversion costs incurred by Hydro are 400 \$89/meter capital and 150 \$89/meter OM&A for general class customers, and 80 \$89/meter capital and 100 \$89/meter OM&A for residential class customers. The meters are assumed to have a 33 year life so these expenses are incurred only once per customer during the planning period.

To shift load, the participant will also have to make capital investments. For example, to shift electricity use for water heating to the off-peak demand period a tank large enough to supply hot water throughout the peak demand period must be purchased. This cost is modelled as 300 \$89/kW when the shifting occurs. This equipment is replaced at this same cost every 11 years. All costs are escalated by the Ontario CPI.

The proportion of energy represented by each load shape was altered so that the demand shifted off the one-hour winter peak in the year 2000 is precisely as shown in the demand management plan. Slightly (less than 1%) more is shifted from the sixteen-hour winter peak.

Ninety-five percent of the energy removed from the peak period was added back in the weekday off-peak and five percent was recovered on weekends. The energy recovered in the weekday off-peak was added equally in each of the off-peak hours. The energy recovered on the weekend was added with the end-use load shape for that customer. The net effect of load shifting is shown in Figure 2.2-3 as the difference between the dashed line and primary demand.

2.2.4 Load Displacement Non-Utility Generation

There are two types of non-utility generation--"load displacement" and "purchase". Load displacement non-utility generation reduces demand much as does EEI, so it is modelled in the demand submodel. Purchase non-utility generation is modelled as a supply-side resource in the supply submodel.

The modelling of load displacement non-utility generation considers dependable demand reduction and average capacity factor (hours of operation per year). Dependable demand reduction is the amount that may be depended upon to be available at peak. This amount is modelled as being available during all hours on the winter and summer high-demand weekdays (peak days).

Figure 2.2-6

Costs of Load Shifting

Year	Load Shifted (MW)	Participant's Costs		Hydro Family Costs	
		Capital (M89\$)	OM&A (M89\$)	Capital (M89\$)	OM&A (M89\$)
1989	80	24.0	0.0	0.0	0.0
1990	169	26.7	0.0	0.0	0.0
1991	263	28.2	0.0	46.4	17.4
1992	421	47.4	0.0	49.4	18.5
1993	580	47.7	0.0	52.4	19.7
1994	655	22.5	0.0	62.8	29.8
1995	715	18.0	0.0	14.0	11.9
1996	775	18.0	0.0	14.7	12.5
1997	835	18.0	0.0	15.4	13.2
1998	892	17.1	0.0	8.0	3.9
1999	946	16.2	0.0	8.3	4.0
2000	1000	40.2	0.0	8.5	4.1
2001	1020	32.7	0.0	5.1	2.4
2002	1040	34.2	0.0	5.2	2.5
2003	1060	53.4	0.0	5.3	2.5
2004	1080	53.7	0.0	5.3	2.6
2005	1100	28.5	0.0	5.4	2.6
2006	1120	24.0	0.0	5.5	2.7
2007	1140	24.0	0.0	5.6	2.7
2008	1160	24.0	0.0	5.7	2.8
2009	1180	23.1	0.0	5.8	2.8
2010	1200	22.2	0.0	6.0	2.9
2011	1220	46.2	0.0	6.1	2.9
2012	1240	38.7	0.0	6.2	3.0
2013	1260	40.2	0.0	6.3	3.0
2014	1280	59.4	0.0	6.4	3.1

The total energy generated by non-utility generators over the year is less than would be obtained by running at the dependable demand reduction for all hours. This is modelled by reducing the amount of generation on all days other than the winter and summer peak days. The proportion of dependable capacity available on each day type is shown in Figure 2.2-7. The effect of load displacement non-utility generation is shown in Figure 2.2-3.

The cost of non-utility generation is modelled as 940 \$89/kW capital cost, with Ontario Hydro offering to cover 12% of that cost. This was based on a contract under negotiation early in 1989. These capital costs are escalated by the Ontario CPI. The fixed OM&A cost was estimated as 135 \$89/kW/yr. This is based on OM&A being 3% of capital cost, natural gas fuel at 2.8 \$88/MCF, a heat rate of 5400 Btu/kWh and an 80% average capacity factor. As the majority of this OM&A cost is made up of gas fuel costs, it is escalated by the same rate as natural gas fuel for CTUs.

2.2.5 Primary Demand

The primary demand is also represented by 384 hourly demands as are the individual loads described above. As noted previously, it is created by subtracting the electrical efficiency improvement load, the load shifting load and the load displacement non-utility load from the basic demand. Primary demand is input to the supply submodel. Primary demand for the year 2000 is shown in Figure 2.2-3; primary demand in 1989, 2000 and 2010 is shown in Figure 2.2-2.

2.3 SUPPLY SUBMODEL

The supply submodel simulates the supply of primary demand through purchase non-utility generation, purchases from neighbouring utilities, existing and new hydraulic generation, nuclear generation, and fossil generation. The supply submodel also calculates the fuel and OM&A costs of all generation, the capital cost of new generation, and the cost of emergency measures.

The main inputs of the supply submodel are the primary forecast from the demand submodel and the characteristics of the generation system, such as rated capacity; forced outage rate; planned outage schedule (by season); and fuel, OM&A and capital (new generation only) unit costs of both new and existing generation. The main outputs are capital and OM&A costs of supply options, fuel costs, and expected energy production by fuel type.

Figure 2.2-7

**Availability of Load Displacement Non-Utility Generation
As Modelled in System Simulation
(Fraction of Dependable Capacity by Day Type)**

Day Type	Season			
	Winter	Spring	Summer	Fall
HIGH Weekday	1.00	0.70	1.00	0.70
MID Weekday	0.95	0.70	0.95	0.70
LOW Weekday	0.80	0.70	0.80	0.70
WEEKEND	0.80	0.70	0.80	0.70

2.3.1 Generation Dispatch and Forced Outages

To make modelling of the generation dispatch more manageable, the supply model first groups the individual units as shown in Figure 2.3-1. To improve the modelling of dispatch, and because energy production and costs are also reported in these groups, the dispatch groups are divided by fuel type.

Figure 2.3-1 also shows the loading order of the dispatch groups. Non-utility generation is used first, followed by purchases, hydraulic, nuclear, coal, gas and oil. Each is used to the maximum before the next is drawn on. The loading of generation on a typical day is shown in Figure 2.3-2.

The loading order as shown in Figure 2.3-1 is based approximately on using the lowest operating cost units first. There are exceptions, however. Hydro is obligated to buy non-utility generation at all times regardless of cost, and lignite is the first coal unit loaded until the Manitoba purchase starts. The order of gas and oil generation changes as the fuel prices change. Gas is listed first as it has the lower fuel cost until late in the planning period.

Depending on the modelling of forced outages, a dispatch group is either set at its average availability or it is represented by several different outage levels. Most of the groups are set at their average available capacity by multiplying their capacity by their average availability. These groups are then always modelled at this average availability. For example, the Lignite group has an installed capacity of 535 MW and an average availability of 92.8% (an average forced outage rate of 7.2%). This group would be modelled as always having 496 MW ($535 \text{ MW} * 0.928$), its average available capacity.

The other dispatch groups are modelled by several different levels of outages. For example, the existing nuclear group could be modelled by four different levels of outages--19 of 20 units available, 18 of 20, 17 of 20, and 15 of 20. The existing nuclear group has 14 182 MW of installed capacity averaging 709 MW in each of 20 units. So, the four levels above would have available capacities of 13 472 MW, 12 764 MW, 12 055 MW, and 10 637 MW. The probability of each of these different levels occurring is also calculated.

Dispatch groups are modelled with different levels until up to 32 different outage states are formed by the combination of all the different outage levels of the dispatch groups. In addition to the four levels with which the nuclear is modelled in the example above, the existing coal generation may be modelled with four levels and the oil group with two levels. This results in the 32 different outage states ($4 \text{ nuclear} * 4 \text{ coal} * 2 \text{ oil}$). The probability of each outage state may also be calculated.

Figure 2.3-1

System Simulation Generation Groups in Dispatch Order

Dispatch Order	Generation Dispatch Group	Existing Units in Group
1	Purchased Non-utility Generation	
2	Major Purchases	
3	Existing Hydraulic	
4	New Hydraulic	
5	Old Nuclear including Darlington	Pickering, Bruce, Darlington
6	New Nuclear	
7	Lignite-fired units *	Atkokan, Thunder Bay 2&3
8	New pulverized US coal	
9	IGCC units	
10	New pulverized Western Canadian coal	
11	Existing Coal units with FGD and CPM	Lambton, Nanticoke, Lakeview
12	Existing Coal units with FGD only	
13	Existing Coal units with CPM only	
14	Other Existing Coal units	
15	Lignite-fired units *	
16	Combined Cycle units	
17	Gas-fired CTU **	
18	Oil-fired Boiler-type units **	Lennox
19	Oil-fired CTU	
20	Emergency Measures	Purchases, Interruptibles, Voltage

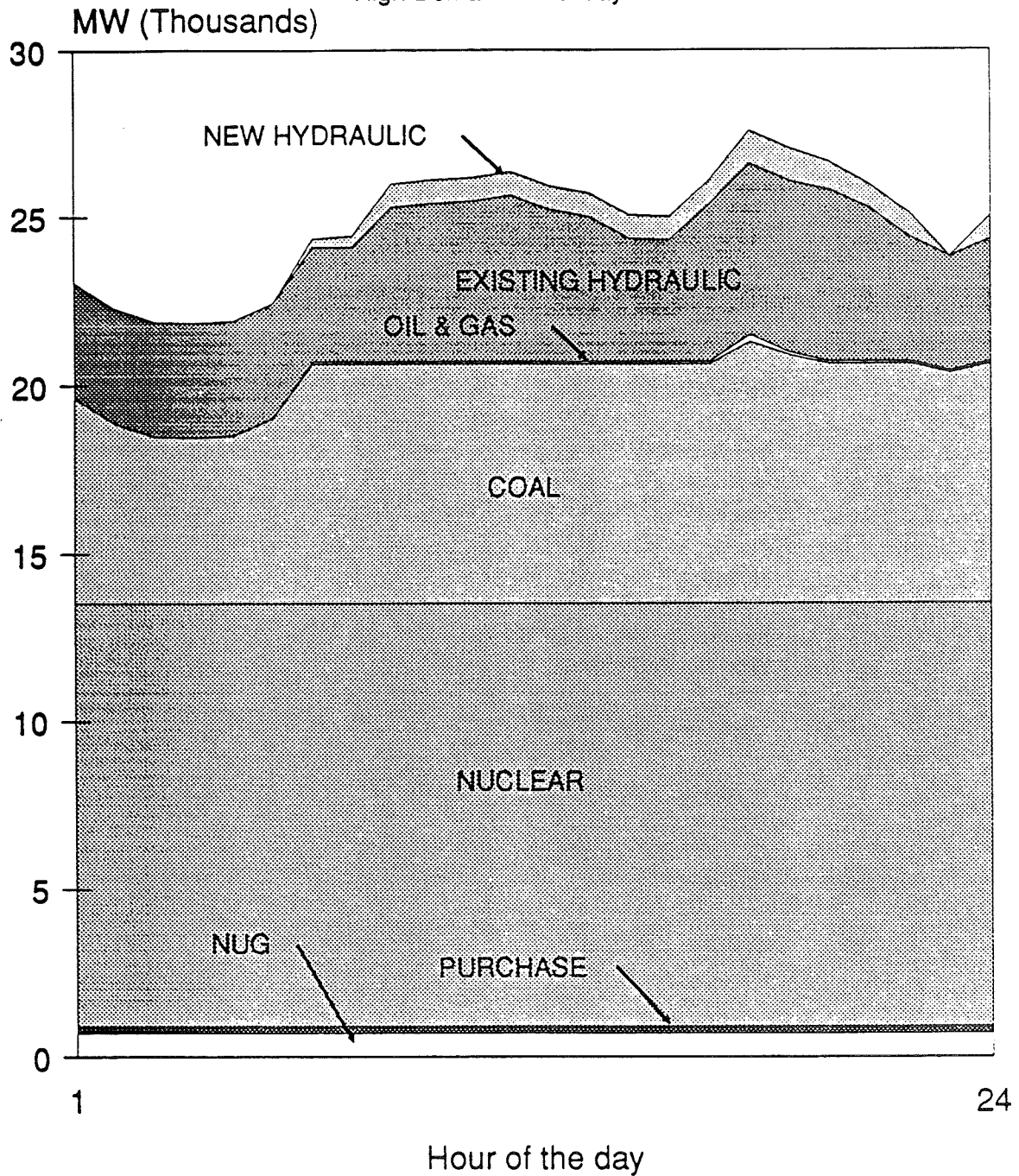
FGD = Flue Gas Desulphurization (Scrubbers)

CPM = Combustion Process Modification (includes low NO burners)

* Changes loading order from first coal unit loaded to last coal unit loaded in 2000, because of Manitoba purchase.

** Order determined by relative costs of oil and gas. Order reverses in later years of study period.

Figure 2.3-2
Example of Generation Dispatch
Year 2000 Winter
High Demand Weekday



For each outage state, the units are dispatched for all day types in all seasons to determine the energy generation from each dispatch group. The energy produced in each state from each group is then averaged across states, based on the probabilities of the outage states. This creates the expected energy production for each dispatch group for that year. The fuel cost is then determined by multiplying the expected energy production by the unit fuel costs.

2.3.2 Planned and Maintenance Outages

Generation outages are classified into three categories--planned, maintenance and forced. Each is modelled differently in LMSTM. Planned outages are scheduled a year or more in advance and tend to be of durations ranging from a few weeks to two or more months. (Unit rehabilitations and retubing are longer duration planned outages. They are addressed in the sections on the specific generation types with which they are associated.) Planned outages are entered directly into LMSTM and are scheduled evenly over the Spring, Summer, and Fall seasons, so that the same amount of generation of each generation type is on planned maintenance in each of these seasons. No planned maintenance is scheduled in the Winter season.

Forced outages are unplanned and occur at random. These are modelled directly by LMSTM as described in the previous section.

Maintenance outages occur at random, but can be delayed until a lower demand period. If the unit would not have been in use in this lower demand period, then the maintenance outage has no effect on the production from this unit. For peaking generation such as Lakeview, therefore, maintenance outages do not affect energy production.

For other, non-peaking, units maintenance outages are considered to occur randomly in all hours of the year. They are modelled as planned outages in all seasons, effectively derating the unit's capacity by the expected time on maintenance outage. For example, if a unit is expected to be down on maintenance outage one day a month, then 4 days of outage would be modelled in each of Winter and Summer, and 2 days of outage would be modelled in each of Spring and Fall.

All reliability indices for existing stations are based on "1988 Forecast of Reliability Studies for Use in Corporate Planning Studies", published in March 1989. For new thermal units reliability indices are based on the Ontario Nuclear Cost Inquiry or the Thermal Cost Review.

2.3.3 Purchase Non-Utility Generation

Purchase non-utility generation is modelled as a single generating unit which runs continually at 80% of installed capacity, has a fuel cost equal to Ontario Hydro's purchase rate and is the first generation dispatched. The full amount of non-utility generation available is always purchased.

2.3.4 Hydraulic

New and existing hydraulic are modelled separately in LMSTM, but are dispatched in a similar manner. Both are dispatched within any season, using a process known as peak shaving. This type of dispatch uses hydraulic generation to create the flattest possible load shape for remaining generation to supply. This produces the lowest cost generation schedule pattern and the minimum unsupplied energy. See Figure 2.3-1, where the peaking hydraulic has been dispatched using peak shaving.

Hydraulic generation is modelled using median water flows to properly reflect the long-term average energy supply contribution of this resource. The capacities and energies used to model both the existing and new hydraulic generation are shown in Figure 2.3-3.

The modelled capacity of existing hydraulic generation available at peak is 500 MW less than the actual installed capacity. The full installed capacity is not available at peak due to physical restrictions such as seasonal and daily flow variations, maximum discharge rates and lags between upstream and downstream stations.

The site extensions at the Mattagami Complex and the developments at Little Jackfish, Niagara, and Big Chute plus Lake Gibson are modelled explicitly for capacity, energy, and in-service date. Other sites are approximated by additions of 200 MW of hydraulic capacity, with in-service dates to best match the Hydraulic Plan, and with energy availability at the average for later units in the plan. The unit availability of new hydraulic units is modelled as 93.2%, except for Niagara which is modelled at 90.0%. The modelling of the total Hydraulic Plan is shown in Figure 2.3-3.

The fuel costs of hydraulic are the water rental rates Hydro pays to the province. This rate is 3.12 \$89/MWh and escalates by Ontario CPI.

2.3.5 Major Utility Purchases

The energy production from the 1000 MW purchase from Manitoba is modelled in LMSTM, but the costs are input directly to RAM. The Manitoba purchase was modelled in the same way as the hydraulic generation discussed above. The annual capacity and energy values of this major utility purchase are shown in Figure 2.3-4.

Figure 2.3-3

Capacity and Energy of Existing and New Hydraulic Supply
In System Simulation

EXISTING HYDRAULIC

Year	Capacity (MW)	Energy by Season (GWh)			
		Winter	Spring	Summer	Fall
1989-2014	6500	11730	6799	11095	6011

NEW HYDRAULIC SUPPLY

Year	Capacity (MW)	Energy by Season (GWh)			
		Winter	Spring	Summer	Fall
1990	0	0	0	0	0
1991	0	0	0	0	0
1992	0	0	0	0	0
1993	16	32	16	33	16
1994	16	32	16	33	16
1995	82	63	32	64	32
1996	338	264	133	266	133
1997	518	475	239	479	239
1998	518	475	239	479	239
1999	1068	819	413	826	413
2000	1068	952	480	960	480
2001	1268	1037	523	1046	523
2002	1468	1122	566	1132	566
2003	1668	1208	609	1217	609
2004	1868	1293	652	1303	652
2005	2068	1378	695	1389	695
2006	2068	1378	695	1389	695
2007	2068	1378	695	1389	695
2008	2068	1378	695	1389	695
2009	2268	1463	738	1475	738
2010	2468	1548	781	1561	781
2011	2668	1634	823	1647	824
2012	2668	1634	823	1647	824
2013	2668	1634	823	1647	824
2014	2868	1719	866	1733	867

Figure 2.3-4

**Capacity and Energy of Manitoba Purchase
In System Simulation**

Year	Capacity (MW)	Energy by Season (GWh)			
		Winter	Spring	Summer	Fall
1990-2000	0	0.00	0.00	0.00	0.00
2001	200	555.12	277.92	555.84	277.92
2002	400	1110.24	555.84	1111.68	555.84
2003	800	2220.48	827.68	1519.36	781.68
2004-2014	1000	2775.60	1139.60	2019.20	1079.60

2.3.6 Existing Fossil Stations

Each fossil unit is modelled separately, even though units within stations have the same costs. Fixed OM&A are forecast from current costs and fuel costs are consistent with those used in the Thermal Cost Review. Figure 2.3-5 shows the capacities by station and by year, as used in the production simulations. Capacity reductions in later years reflect retirements.

Depending on the length of the outage involved, the costs of rehabilitating existing fossil stations are treated in one of two ways--as a fixed OM&A cost, if the outage is only several months; or as a capital cost, if the outage is modelled as one or more years in duration. The rehabilitation of Lambton was treated as planned outages with costs recovered in OM&A. The Lakeview rehabilitation costs are modelled as a capital expenditure and depreciated over the remaining life of the station. These rehabilitations and the retrofits of scrubbers (as in proposed plan median load growth) are also indicated in Figure 2.3-5.

When a unit of Lambton or Nanticoke has its combustion process modified to reduce NO_x , or when scrubbers are retrofit to reduce SO_2 , the unit is retired from service and a new one is added with revised characteristics and a capital cost equal to the cost of the modification.

2.3.7 Existing Nuclear Stations

Pickering A and B, Bruce A and B, and Darlington are existing Hydro nuclear units. The capital cost of Darlington is explicitly modelled because it comes into service after 1989. The capital costs of the other stations are included with other existing assets (see Section 2.4). Fuel costs are based on existing nuclear fuel contract prices and are adjusted to include fuel disposal costs. Fixed OM&A is modelled as a projection of ongoing costs and has not been levelized. Large-scale fuel channel replacement (retubing) is explicitly modelled.

Retubing is modelled by removing nuclear units from service for one to three years while they are being retubed. Such outages must be modelled as 12, 24 or 36 months (1, 2, or 3 years), while the actual retubing times of individual units are 19 to 31 months. The modelling of the total retubing schedule (see Figure 2.3-6) is designed to match the actual schedule as closely as possible.

Figure 2.3-5

Existing Fossil Station Capacity
As Modelled in System Simulation
(As in Proposed Plan)

Year	Lambton		Nanticoke		Lakeview		Thunder Bay		Lennox		Atikokan
	MW	Notes*	MW	Notes*	MW	Notes*	MW	Notes*	MW	Notes*	MW
1989	2100		4336		2282		320		1674		215
1990	2100		4336		2282		320		2232	DMB 3	215
1991	2100	RHB 1	4336		1998	RHB 5	320		2232		215
1992	2100	RHB 2	4336		1998	RHB 6	320		2232		215
1993	2100	RHB 3	4336		1993	RHB 1	320		2232		215
1994	2080	RHB 4	4336		1993	RHB 2	420	DMB 1	2232		215
		CPM 3 & 4									
		SCR 1 & 2									
1995	2070	CPM 1 & 2	4336		1714	RHB 3 & 4	420		2232		215
		SCR 3 & 4									
1996	2070		4336		1714	RHB 7 & 8	420		2232		215
1997	2070		4336		2282		420		2232		215
1998	2070		4326	CPM 1 - 4	2282		420		2232		215
1999	2070		4326		2282		420		2232		215
2000	2070		4326		2282		420		2232		215
2001	2070		4326		2282		420		2232		215
2002	2070		4326		1993	RET 1	420		2232		215
2003	2070		4326		1704	RET 2	420		2232		215
2004	2070		4326		1704		420		2232		215
2005	2070		4326		1136	RET 3 & 4	420		2232		215
2006	2070		4326		1136		420		2232		215
2007	2070		4326		852	RET 5	420		2232		215
2008	2070		4326		852		420		2232		215
2009	2070		4326		0	RET 6 - 8	420		2232		215
2010	0	RET 1 - 4	4326				420		2232		215
2011			4326				420		2232		215
2012			4326				420		2232		215
2013			3787				420		2232		215
2014			2168				420		2232		215

- * RHB = Rehab of indicated units
- DMB = Demothball indicated units
- CPM = Modify indicated units
- SCR = Retrofit scrubber on indicated units
- RET = Retire indicated units

Note: Keith, Hearn A(units 1-4) and Hearn B(units 5-8) are mothballed.
In case of demothballing their capacities would be:
Keith - 256 MW, Hearn A - 391 MW, Hearn B - 788 MW
Oil-fired CTUs at existing sations have a capacity of 253 MW.

Figure 2.3-6

Existing Nuclear Station Capacity
As Modelled In System Simulation
(As in Proposed Plan)

Year	Pickering A & B MW	Notes*	Bruce A & B MW	Notes*	Darlington MW	Notes*
1989	4124		6516		0	
1990	3609	RTB 3	6516	SLR 3 & 4	1762	INS 1 & 2
1991	3609	RTB 4	6516	SLR 1	2643	INS 3
		SLR 5				
1992	3609	RTB 4	6516		3524	INS 4
		SLR 6				
1993	4124		6516		3542	
1994	4124		6516		3524	
1995	4124		6516		3524	
1996	4124		6516		3524	
1997	4124		6516		3524	
1998	4124		6516	RFB 3	3524	
1999	4124		6516		3524	
2000	4124		6516		3524	
2001	4124		6516		3524	
2002	4124		5747	RTB 3	3524	
2003	4124		4978	RTB 2 & 3	3524	
2004	4124		5747	RTB 2	3524	
2005	4124		5747	RTB 2	3524	
2006	3608	RTB 5	6516		3524	
2007	3608	RTB 5	5747	RTB 1	3524	
2008	3608	RTB 6	4978	RTB 1 & 4	3524	
2009	3608	RTB 6	5747	RTB 4	3524	
2010	3608	RTB 7	5656	RTB 5	3524	
2011	2578	RTB 7	5656	RTB 5	3524	
		RET 1 & 2				
2012	2063	RTB 8	5656	RTB 6	3524	
		RET 3				
2013	2064	RET 4	5656	RTB 6	3524	
2014	2064		5656	RTB 7	3524	

* INS = In-service date of indicated units

SLR = Spacer location and relocation for indicated units

RFB = Repositioning end-fitting and bearings for indicated units

RTB = Indicated units down for retubing

RET = Retire indicated units

2.3.8 New Thermal Stations

All values for new fossil stations were based on the Thermal Cost Review. All 'Initial Capital' was modelled as a capital cost. All other costs excluding 'Fueling Costs', were levelized over the life of the station and included as fixed OM&A. Fuel costs are calculated in LMSTM based on expected energy generated. Unit fuel costs are as in the Thermal Cost Review.

Similarly, all values for new nuclear stations were based on the Nuclear Cost Inquiry data. Costs labelled 'Initial Capital' were included as a capital cost; used fuel management, transportation and repository costs were entered as variable operating costs. All other costs were annualized and included as fixed OM&A. Fuel costs are calculated in LMSTM based on expected energy generated. Unit fuel costs are based on Nuclear Cost Inquiry data.

As noted in Section 2.1.1 new units are constrained to start as of January 1. Also each unit is modelled with the same capital construction pattern. These patterns were developed in such a way that the sum of the patterns of the four units in a four unit station matched the supplied station construction pattern as closely as possible.

2.3.9 Emergency Measures

During the scheduling of generation, emergency measures are treated as the last generation loaded. The use of emergency measures is essentially the generation from this "unit". Emergency measures are emergency purchases, interruptible load cuts and voltage reductions, which add up to 2000 MW.

The cost of this energy is modelled as 11 \$89/MWh above the cost of CTU oil to ensure that load is supplied by oil generation before these measures are implemented.

2.4 FINANCE SUBMODEL

The main financial modelling processed through LMSTM is levelizing of capital costs. This is actually performed by a modification made by Ontario Hydro to the standard LMSTM code. It uses a constant 5% real discount rate to determine the equal real dollar annual payments (required to pay for an investment over its life). All capital costs are levelized in this way. The RAM was used for the main financial results (see Chapter 8).

The financial submodel was used to model distribution system, transmission system, overhead and other fixed costs. The modelling of demand management and load displacement non-utility generation costs is described with the demand submodel (Section 2.2) and Section 2.3 (supply submodel) contains the description of generation fixed and fuel costs. Other costs used for the detailed results are described in Chapters 8 and 9.

2.4.1 Incremental Distribution Costs

The distribution costs for Ontario Hydro's Rural Retail System and for all of the municipal utilities are modelled to reflect the total savings of demand management regardless of the retail supplier. Distribution costs are modelled in two ways. Incremental costs are proportional to primary load growth and other costs are entered directly as cash flows as described in Section 2.4.3.

The costs associated with new investment in distribution equipment required to meet growing demand and some of the fixed operating costs of the whole distribution system are modelled. These costs are proportional to primary demand in the two residential customer classes and the general customer class. Specifically, these costs are proportional to the peak demand of each class. The direct customer class does not require distribution equipment from Hydro.

The incremental distribution costs may be divided into energy-, demand-, and customer- related costs. As demand management is not designed to alter the number of customers in Ontario only energy- and demand- related distribution costs are modelled as incremental distribution. The costs of customer-related incremental distribution are included under overhead and other fixed costs (see Section 2.4.3).

OM&A costs of incremental (post 1989) distribution system expansions are estimated as 5.46 \$89/kW/yr. This OM&A cost is also applied to the existing distribution system. Incremental distribution investment has a capital cost of \$228 (1989 dollars) per kW of growth in the class peak demands. These values are based on an Ontario Hydro report, 'Estimation of Incremental Capacity Costs for Municipal Utilities', Aug. 1987.

2.4.2 Incremental Transmission Costs

Four different types of transmission costs are defined--radial transmission, inter-area transmission, incremental load-growth transmission and existing transmission. Incremental transmission is modelled as directly proportional to peak load growth. This is distinct from inter-area transmission which is related specifically to the location of new major supply. Radial transmission is specific to particular generating stations and is modelled as part of the capital cost of each new station. The costs of inter-area and radial transmission are input directly to RAM.

Incremental load-growth transmission was modelled in the system simulation. Its costs were divided into bulk transmission, with a capital cost of 135.7 \$89/kW and an OM&A cost of 4.87 \$89/kW/yr; and regional transmission, with a capital cost of 124 \$/kW.

Existing transmission costs were entered as overhead and other fixed costs described in Section 2.4.3.

2.4.3 Overhead and Other Fixed Costs

Overhead and other fixed costs are modelled as cash flows of both capital costs and fixed OM&A costs. These cash flows do not vary throughout the analysis and are input directly:

- Ontario Hydro, overhead and other fixed costs;
- Capital modification to existing generation not explicitly modelled in the supply submodel;
- Existing transmission system costs;
- Rural distribution, existing system and overhead costs; and,
- Municipal distribution, existing system and overhead costs.

These costs are shown in Figure 2.4-1.

Except for the municipal costs, all costs are based on the 1988 Ontario Hydro long-range financial plan. Municipal expenses were based on those reported in the 1987 Ontario Hydro Statistical Yearbook and then adjusted for load growth and inflation. From these values, the incremental distribution costs were subtracted to obtain the values shown in Figure 2.4-1. The costs shown for the rural retail system and for existing transmission were obtained in the same way.

2.5 ACID GAS AND SECONDARY NUCLEAR SALES MODELLING

An additional submodel written by Ontario Hydro starts with the LMSTM energy production and fuel cost output and determines acid gas and carbon dioxide emissions, revises the fuel cost of existing station to reflect coal blending, and estimates secondary nuclear sales.

2.5.1 Acid Gas Calculations and Fuel Blending

To determine emissions of SO₂, NO_x, and CO₂ from fossil stations the emission rates from the Thermal Cost Review were used. These are summarized in Figure 2.5-1.

Figure 2.4-1(a)

Overhead and Other Fixed Costs
In System Simulation

Capital Costs
(Millions of Current Dollars)

Year	Ontario Hydro				
	Overhead & Other Fixed Costs	Generation Capital Modifications	Transmission Other Fixed Costs	Distribution Systems	
				Rural Retail System	Municipal Utilities
1989	179	77	327	174	162
1990	164	77	519	155	51
1991	148	120	486	170	43
1992	217	360	366	187	46
1993	169	381	335	200	44
1994	171	371	452	215	68
1995	181	470	459	238	129
1996	194	451	487	259	153
1997	210	537	311	281	168
1998	227	534	438	304	155
1999	247	538	478	326	107
2000	268	578	401	350	86
2001	291	695	387	363	79
2002	316	654	414	413	175
2003	344	691	592	442	157
2004	374	731	1082	482	148
2005	407	771	496	527	183
2006	442	813	526	563	197
2007	479	857	555	611	247
2008	518	910	587	659	263
2009	562	962	587	714	301
2010	610	1016	587	773	315
2011	662	1073	587	837	349
2012	719	1134	587	907	381
2013	780	1198	587	982	416
2014 *	NA	NA	NA	NA	NA

* Capital costs in last year of planning period could not be modelled.

Figure 2.4-1(b)

Overhead and Other Fixed Costs
In System Simulation

OM&A Costs
(Millions of Current Dollars)

Year	Ontario Hydro				
	Overhead & Other Fixed Costs	Generation Capital Modifications	Transmission Other Fixed Costs	Distribution Systems	
				Rural Retail System	Municipal Utilities
1989	361	0	155	157	301
1990	384	0	166	169	326
1991	363	0	174	184	355
1992	421	0	179	201	387
1993	557	0	187	215	419
1994	577	0	192	234	455
1995	695	0	201	249	497
1996	719	0	211	265	547
1997	770	0	221	287	600
1998	823	0	233	309	658
1999	854	0	245	335	719
2000	891	0	260	367	783
2001	684	0	277	406	855
2002	738	0	297	442	934
2003	799	0	318	486	1020
2004	867	0	341	532	1111
2005	936	0	366	580	1210
2006	1010	0	392	635	1333
2007	1090	0	421	692	1470
2008	1175	0	451	755	1615
2009	1269	0	484	825	1785
2010	1371	0	519	901	1967
2011	1481	0	556	984	2167
2012	1600	0	596	1075	2386
2013	1728	0	640	1174	2628
2014	1867	0	686	1282	2845

Figure 2.5-1

Emission Rates for Fossil Stations
In System Simulation

Dispatch Group	Emission (MG/GWH)		
	SO2	NOX	CO2
Existing Coal units with FGD and CPM	1.64	1.12	860
Existing Coal units with FGD only	1.64	1.40	855
Existing Coal units with CPM only - High Sulphur Coal	16.70	1.36	825
- Low Sulphur Coal	5.30	1.36	825
- Western Can. Coal	2.30	1.36	930
- Natural Gas	0.00	1.44	473
Other Existing Coal units - High Sulphur Coal	16.70	1.70	820
- Low Sulphur Coal	5.30	1.70	820
- Western Can. Coal	2.30	1.70	925
- Natural Gas	0.00	1.80	470
New pulverized US coal *	1.64	0.25	860
New pulverized Western Canadian coal *	2.30	0.15	930
Lignite-fired units	4.30	1.30	935
Gas-fired CTU	0.00	1.20	470
Oil-fired Boiler-type units	2.80	1.30	670
IGCC units	0.47	0.25	810
Oil-fired CTU	1.60	1.90	0 **

* The emission rate for SO2 applies only after the year 2000

** Typographical error in input data file for system simulation.
Little effect on results as production from this group averages
less than 1 GWh/yr.

Based on meeting the acid gas emission limits, the sulphur content of coal burned in existing, unscrubbed coal stations is then determined. The revised fuel cost is then computed based on the types of coal used. This process provides for an emission reserve--energy production could be increased by 9 TWh without exceeding the acid gas limits.

2.5.5 Secondary Nuclear Sales

Surplus nuclear energy production may be sold to U.S. utilities at a price higher than the incremental production cost. This is computed by first determining available surplus nuclear energy. This is equal to the maximum possible nuclear production (total nuclear capacity * 84% average nuclear availability * 8760 hours) minus actual production. Units down for retubing are not included as part of total nuclear capacity and the average availability excludes retubing outages.

The amount actually sold is a percentage of the surplus energy which decreases as the surplus increases (see Figure 2.5-2). This is multiplied by the selling price to determine revenue. The nuclear production cost is subtracted to yield net revenue or profit from the sale. The selling price is approximated as half way between the energy production costs of coal generation and nuclear generation.

2.6 REVIEW

The system modelling is the source of energy production by fuel type, fuel costs, and costs which are common across all plans. Other models described in Chapters 8 and 9 perform further financial modelling to calculate plan costs, assess risk, and determine corporate financial impacts. The costs of major supply options and inter-area transmission are entered directly into these other models.

The system modelling is done with a version of LMSTM modified at Ontario Hydro. LMSTM is an integrated planning model which models both demand and supply resources. System modelling is divided into four main aspects:

- demand submodel;
- supply submodel;
- finance submodel;
- acid gas & secondary nuclear sales.

The **Demand Submodel** is structured specifically for modelling the demand reductions from demand management programs. Electricity demand is modelled by 16 different typical daily load shapes ($24 \times 16 = 384$ hours). This load model is specifically designed to facilitate the different effects of electrical efficiency improvements and load shifting over a day or week.

Figure 2.5-2

**Secondary Nuclear Sales Assumptions
in System Simulation**

Surplus (TWh)	Percent Sold of Last TWh	Percent Sold of Total TWh
1	70%	70%
2	70%	70%
3	60%	67%
4	60%	65%
5	50%	62%
6	50%	60%
7	50%	59%
8	40%	56%
9	40%	54%
10	40%	53%
11	40%	52%
12	40%	51%
13	40%	50%
14	35%	49%
15	35%	48%
16	35%	47%
17	35%	46%
18	35%	46%
19	35%	45%
20	35%	45%
21	35%	44%
22	35%	44%
23	35%	43%
24	25%	43%
25	25%	42%
26	25%	41%
27	25%	41%
28	25%	40%
29	25%	40%
30	25%	39%

The demand modelling starts with the basic load forecast. Demand reductions from electrical efficiency improvements, load shifting and load displacement non-utility generation are removed from the basic demand to create the primary demand.

The costs of demand management and load displacement non-utility generation are calculated in the demand submodel.

The **Supply Submodel** simulates the supply of primary demand through purchase non-utility generation, purchases from neighbouring utilities, existing and new hydraulic generation, nuclear generation, and fossil generation. It produces the expected energy production and fuel cost by fuel type. The capital and fixed costs of new supply for the financial analysis of plans are determined in other models.

Supply resources are combined into 20 different dispatch groups. For simulating dispatch these groups are either modelled at their average availability or with several different outage levels. The possible combinations of the outage levels create up to 32 outage states. Generation is dispatched in each of these states and then expected energy production by dispatch group is found by averaging across the possible states, in proportion probabilities of these states occurring. Forced, maintenance and planned outages are all modelled in generation dispatch.

Purchased non-utility generation is dispatched first. Next, new and existing hydraulic generation, and major utility purchases (Manitoba purchase) are dispatched by peak shaving. Thermal units are dispatched in the following order: old nuclear; new nuclear; lignite (until Manitoba purchase); new coal; existing coal; lignite (after Manitoba purchase); natural gas CTUs; oil (dispatched before natural gas after 2013); existing CTUs; and, emergency measures.

The **Finance Submodel** calculates the costs of incremental distribution and incremental transmission. It also determines the overhead and other fixed costs for Ontario Hydro, rural retail, municipalities, existing transmission, and capital modifications of existing generation.

Incremental distribution costs are those due to load growth. Distribution costs due to growth in the number of customers, and other costs of the rural retail system and the municipalities, are included as overhead and other fixed costs.

Transmission costs are defined as radial, inter-area, incremental load-growth, and existing. Radial and inter-area transmission costs are determined by the major supply plan and are input directly to the financial cost models. Incremental load-growth transmission costs are calculated in the system modelling. Costs of existing transmission are entered in the overhead and other fixed costs.

Acid Gas and Secondary Nuclear Sales modelling determines the SO₂, NO_x, and CO₂ emissions using the emission rates from the Thermal Cost Review. Then the sulphur content of coal burned at existing stations is determined such that the acid gas emission limits will be met if 9 TWh more energy must be generated.

Finally, the expected sales of surplus nuclear energy are calculated. The selling price is approximated as half way between the energy production costs of coal generation and nuclear generation.

3. RELIABILITY

- 3.0 INTRODUCTION
- 3.1 ONTARIO HYDRO'S BULK ELECTRICITY SYSTEM
- 3.2 A FIRST MEASURE OF PLAN EFFECTIVENESS
- 3.3 RELIABILITY AT WHAT COST?
- 3.4 RELIABILITY CRITERION
- 3.5 HISTORICAL GENERATION UNRELIABILITY
- 3.6 MEASURING RELIABILITY
- 3.7 MEETING THE RELIABILITY STANDARD
- 3.8 PLANNED RESERVE MARGINS
- 3.6 REVIEW

3.0 INTRODUCTION

To Hydro's customers, reliability means continuous, uninterrupted electricity service. Ontario Hydro, like all utilities responsible for electricity generation and transmission, strives to provide that service.

Over the past several years, the amount of energy not supplied to Hydro customers due to bulk electricity system failures has been below the limit set in Hydro's standards. Hydro provides this performance by ensuring Ontario has adequate facilities to supply demand throughout the province.

Reliability is also a function of the quality standards Hydro applies to everything it does to meet current and future electricity needs -- system design, equipment specifications and selection, construction, installation, training, planning, operation, maintenance and administration.

An interruption in electricity service can originate at a number of points -- generation, the high voltage transmission network, delivery to municipal utilities, large industrial customers and retail customers, and local distribution by municipal utilities. The focus in this analysis is on generation reliability.

3.1 ONTARIO HYDRO'S BULK ELECTRICITY SYSTEM

Hydro's electricity system, including some 80 generating stations and a high voltage transmission network, is integrated to allow the pooling of resources. Linkages exist within and between the East and West systems (See Figure 3-1 - Map of Ontario showing geographic location of east and west systems, plus simplified indication of where links exist between the two systems and other utilities.) As well, there are connections with neighbouring utilities in Manitoba, Quebec, New York and Michigan.

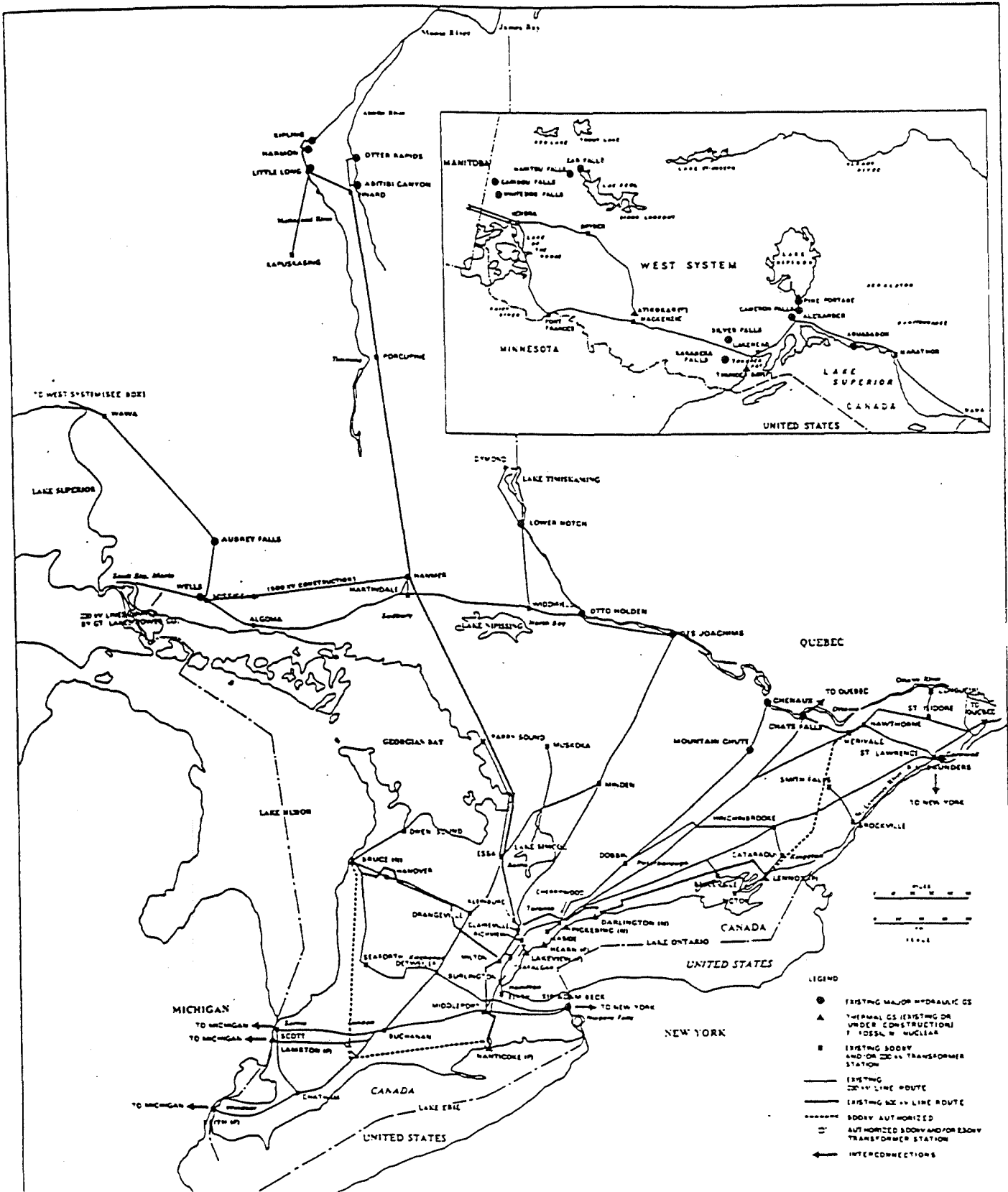
This integration allows Hydro to provide reliable electricity service with less generation than would be needed for a similarly sized unintegrated system, comprised of regional electricity generators unable to share resources.

3.2 A FIRST MEASURE OF PLAN EFFECTIVENESS

Reliability is a primary criterion for developing and evaluating cases. Because of its importance to customer satisfaction and its influence on plan development, it is examined early in the planning process. Two preliminary cases were selected for a

Figure 3-1

ONTARIO HYDRO
MAJOR 500 kV AND 230 kV LINE
ROUTES AND STATIONS
(AS OF MID 1987)



detailed evaluation of reliability. These are representative of cases considered in the Demand Supply Plan Report. Conclusions drawn from the results are valid for later versions of these two cases and all cases presented in Chapter 4.0, Formulation and Description of Plans.

The two cases studied were Case 6, the earlier version of Higher Fossil Case 26; and Case 8, the earlier version of the Proposed Major Supply Case. Both Cases 6 and 8 were modelled without the Manitoba purchase.

3.2.1 Key Generation Reliability Factors

The reliability of a particular generating station is a function of its design, age, operating history, maintenance practices, technology, fuel and size. Smaller stations, for example, tend to be more reliable than larger stations. Weather conditions can affect the performance of various stations -- a dry spell could lower water levels at a hydraulic station; cold weather could freeze a coal pile; weather inversion could trap emissions, forcing the curtailment of operations at certain stations.

Another key generation reliability factor is the difference between the actual and forecast load. These variances result when key variables such as the provincial economy deviate from the long-term forecast.

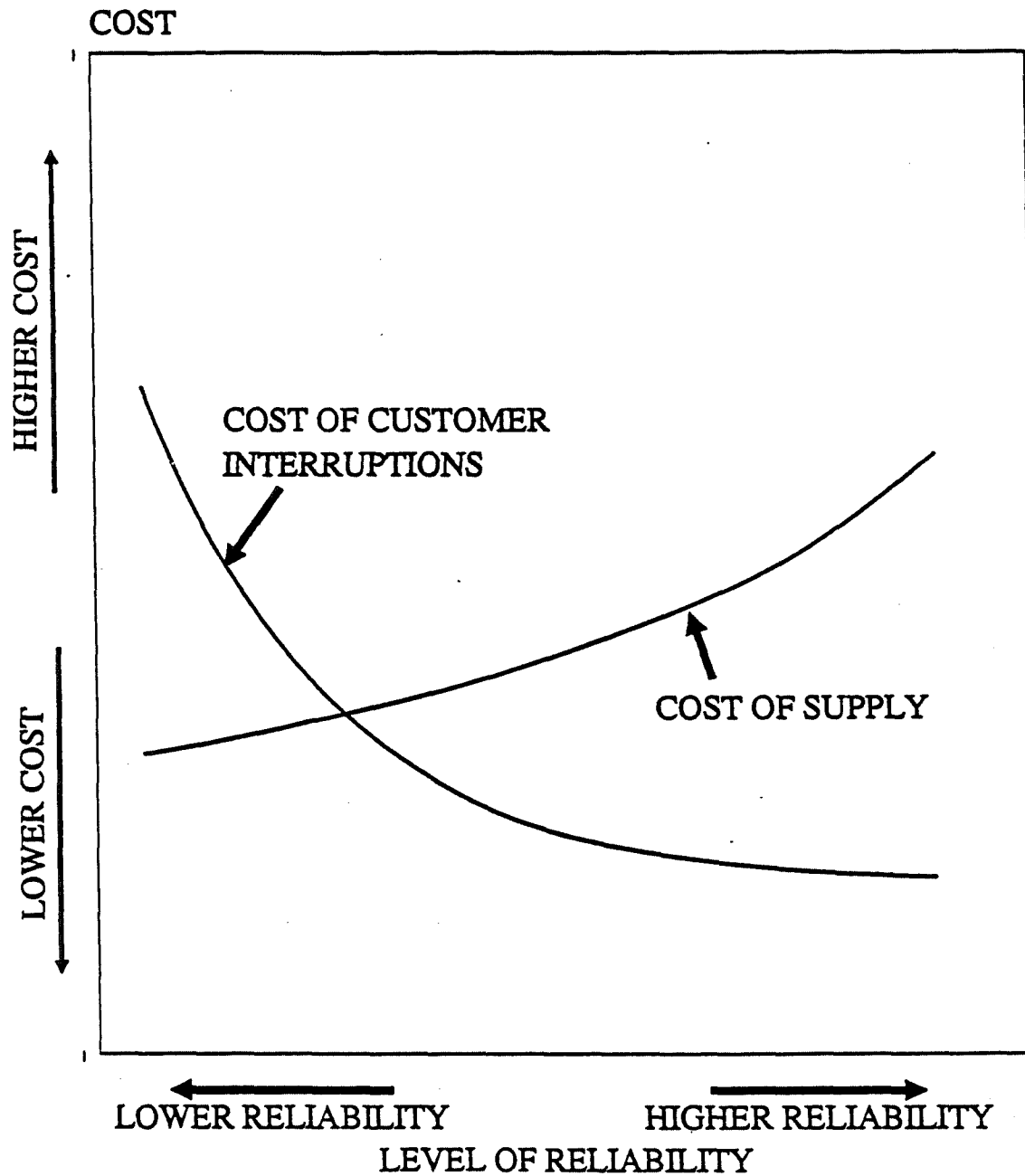
3.3 RELIABILITY AT WHAT COST?

Reliability carries two kinds of costs: the cost of electricity supply and the customer loss due to supply interruptions. Adding more supply facilities leads to higher customer costs for electricity service, (Figure 3-2 - Reliability Costs), but lower customer interruption costs. Reducing supply facilities leads to lower electricity service costs, but higher customer interruption costs.

Interruption costs are a function of the damages resulting from loss of electricity service. If a farmer experiences a prolonged service interruption in a summer month, for example, milk could go bad; in the winter, a service interruption could cause chicks to freeze.

In 1978, Hydro did major pioneering work to obtain cost estimates for outages affecting primary electricity users -- large farms, offices, retail trade, small industrial, large user (auto plant, steel maker), government and institutions, and residential.

FIGURE 3-2
RELIABILITY COSTS



Since then, the cost of outages for some customers has likely gone up, due to the increasing dependency on electricity for everything from office and retail computers systems to robotics.

To determine the reliability level that minimizes total customer cost (Figure 3-3 - Total Cost of Electricity), Hydro balances the total cost of electricity, including the costs of supply and customer interruption, against the level of reliability. Typically, there is a range of reliability levels Hydro can provide at the lowest cost to the customer (Figure 3-4). Hydro chooses to operate at the top end of this range, because it provides a high level of reliability at low customer cost. For example, earlier studies on generation system reliability (the System Expansion Program Reassessment (1979)) found that a five percent increase in installed generation, results in a 60 percent decrease in unsupplied energy, at a cost of increasing customer prices by about one percent.

3.4 RELIABILITY CRITERION - "No more than 25 minutes..."

The current reliability criterion for generation planning states:

"Sufficient generation reserve is planned such that after allowing for interconnecting assistance and emergency operating actions, the expected annual unsupplied energy, the product of frequency, duration and magnitude of customer interruptions, caused by a deficiency of generation is less than 25 system minutes."

A system minute is the quantity of energy that is not supplied if the entire system is interrupted for one minute during annual peak demand.

Customer impact depends on how often interruptions occur, how long they last, and how much load gets interrupted. A short interruption affecting a large portion of the province, for example, could result in more unsupplied system minutes than a longer interruption in a city, simply because the provincial outage affected many more users.

To avoid or minimize a supply interruption, Hydro can:

- operate all available generating units;
- cut non-firm sales;
- cut interruptible loads;
- maximize purchases from interconnected systems;
- reduce voltage;
- reduce operating reserve to zero;
- make public appeals to reduce consumption of electricity;
- activate rotating load cuts.

FIGURE 3-3
TOTAL COST OF ELECTRICITY

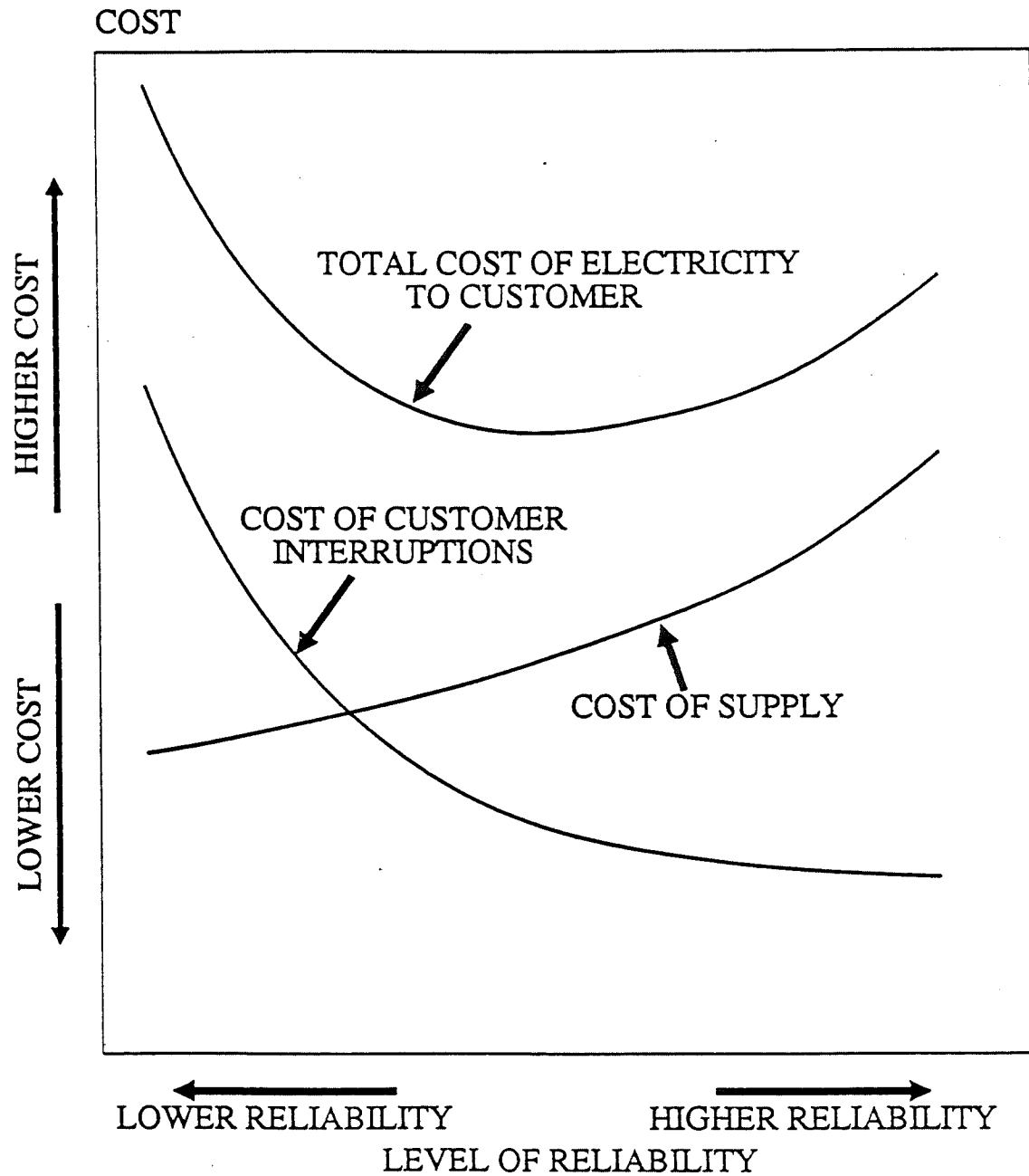
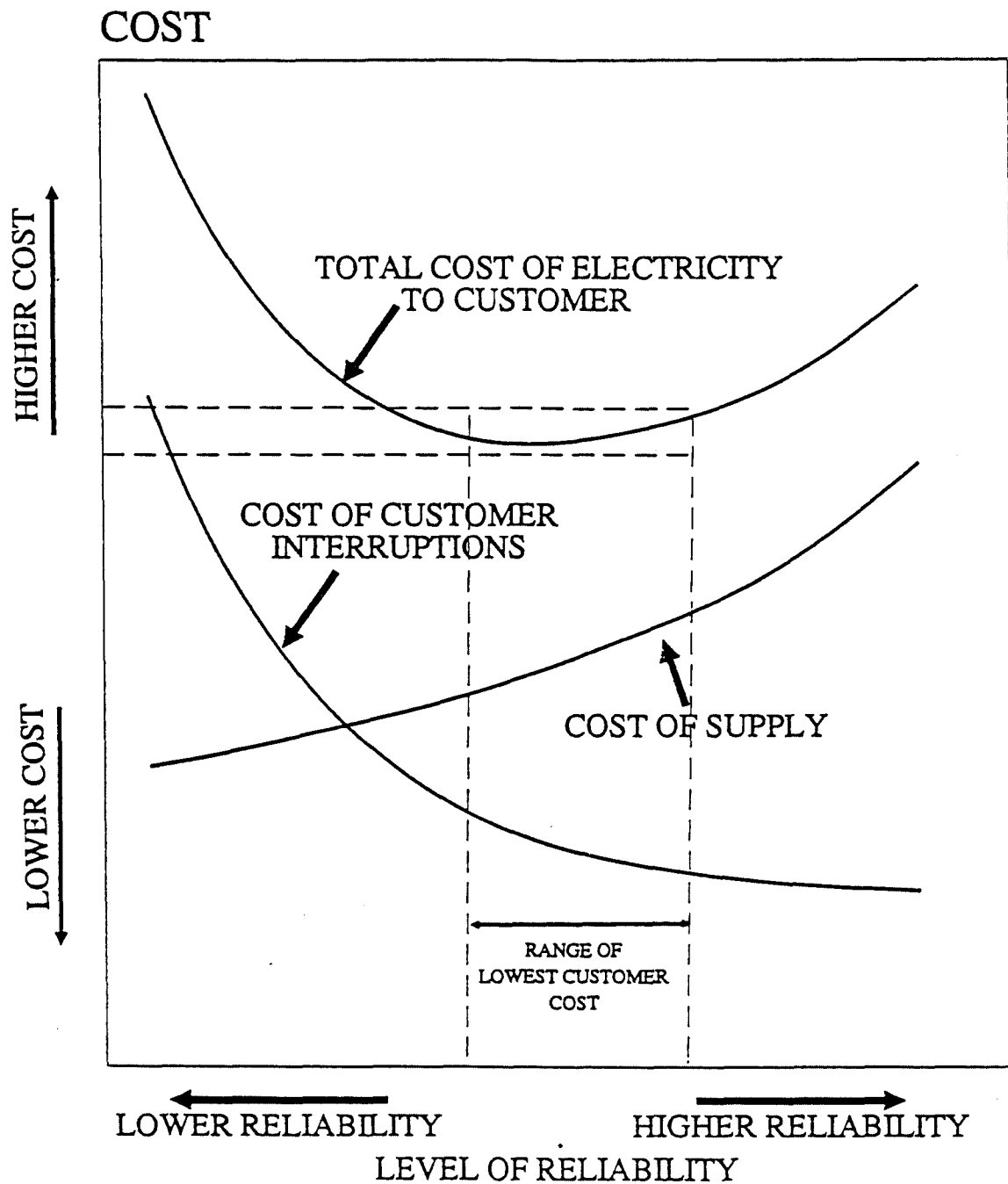


FIGURE 3-4
TOTAL CUSTOMER COST OF ELECTRICITY



The order of these steps depends on the nature of the shortage, location, duration and timing.

The last two actions, public appeals and rotating load cuts, result in unsupplied energy. Load cuts to interruptible customers are not tallied as unsupplied system minutes of energy, but are recorded.

In the last decade, some customers have experienced minimal interruptions, others have experienced extended interruptions. On a few occasions, such as in August, 1988, Hydro had to enact one or more measures to minimize supply interruptions. (For details see Section 3.5: Historical Generation Unreliability) However, the annual sum of unsupplied energy, resulting from generation deficiencies, has been below the 25 system-minute mark in each year.

3.5 HISTORICAL GENERATION UNRELIABILITY

The bulk electricity system unreliability data shown in Figure 3-5 includes both generation and transmission related events. The number of interruptible load cuts has increased in recent years; more than half of the interruptible load cuts in 1986-1988 were due to generation related events.

Unsupplied energy due to generation unreliability has averaged about 0.1 system-minutes per year over the last 10 years. This is well below the limit set in Hydro's standards.

3.5.1 Close Calls

Not indicated in Figure 3-5 is the how the available generation is needed and utilized year-round. Also not evident is the number of occasions when the system was on the brink of tallying significantly more minutes of unsupplied energy because of unplanned conditions. Figure 3-6a illustrates the generation available to meet Ontario's primary electricity demand in 1988. At several times, particularly in August, the generation system was just one contingency away, for example, turbine or generator problems, from being unable to meet demand. The actual reserve capacity for the last 6 years, after allowing for mothballed capacity, planned and forced outages is illustrated in Figure 3-6b. Figure 3-6c illustrates the actual reserve margin in percent for the past six years.

Figure 3-5

Bulk Electricity System Unreliability Data

Included in 25-minute criterion

<u>Voltage Reductions</u>	<u>Total No. of events</u>	<u>No. of Generation Related Events (included in Total)</u>	<u>Unsupplied Energy (System-minutes)</u>
1984	-	-	-
1985	1	0	1
1986	-	-	-
1987	-	-	-
1988	3	0	1

<u>Public Appeals</u>	<u>Total No. of Events</u>	<u>No. of Generation Related Events (included in Total)</u>	<u>Unsupplied Energy (System-minutes)</u>
1984	-	-	-
1985	1	1	1
1986	-	-	-
1987	1	0	3
1988	1	0	6

Not included in 25-minute criterion

<u>Capacity Interruptible Load Cuts</u>	<u>Total No. of Events</u>	<u>No. of Generation Related Events (included in total)</u>	<u>Unsupplied Energy (System-minutes)</u>
1984	2	1	4
1985	12	4	23
1986	6	3	35
1987	5	4	18
1988	14	8	50

FIGURE 3-6a
GENERATION AVAILABLE
TO MEET PRIMARY DEMAND
1988

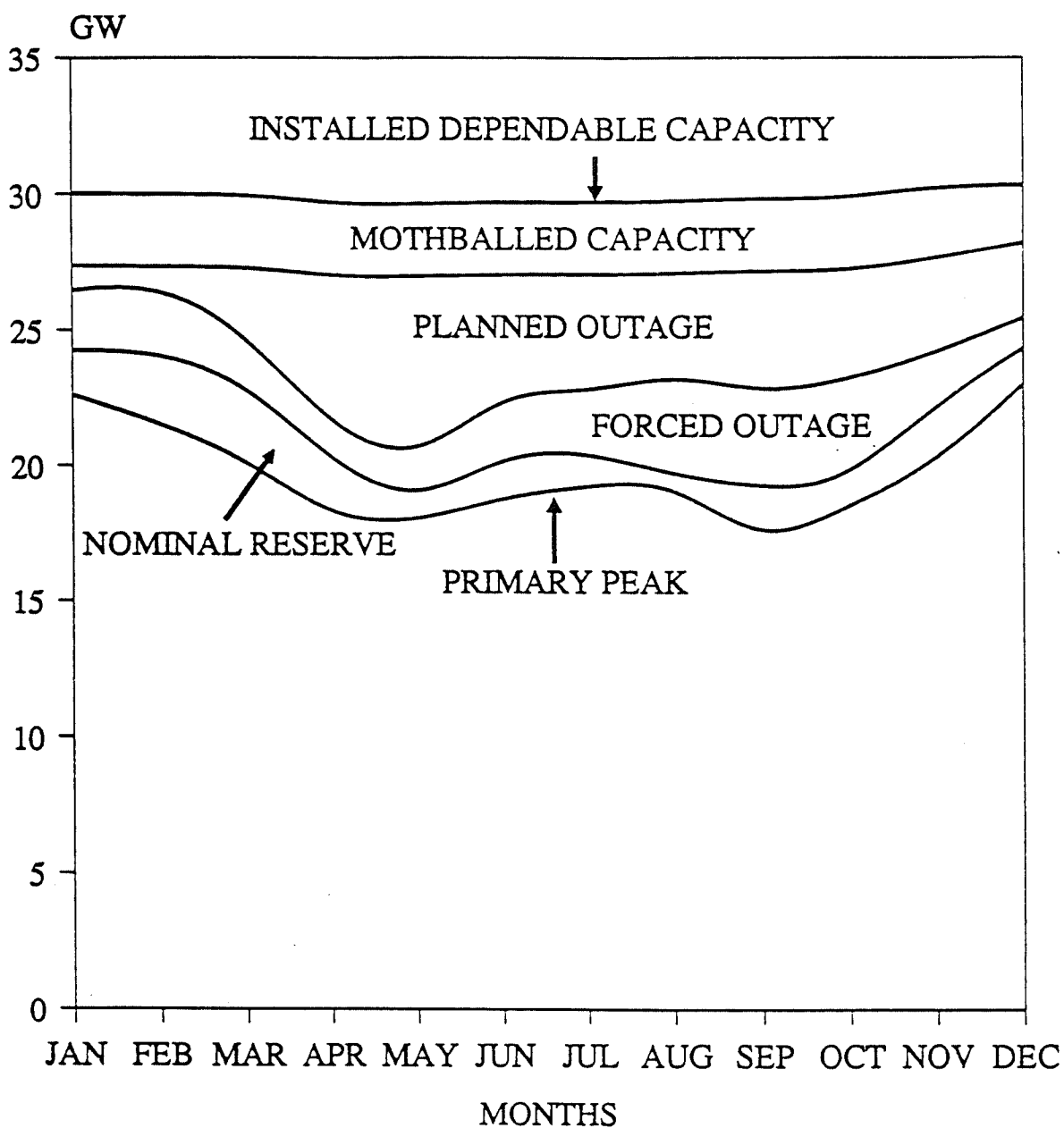


FIGURE 3-6b
GENERATION AVAILABLE
TO MEET PRIMARY DEMAND
1983 - 1988

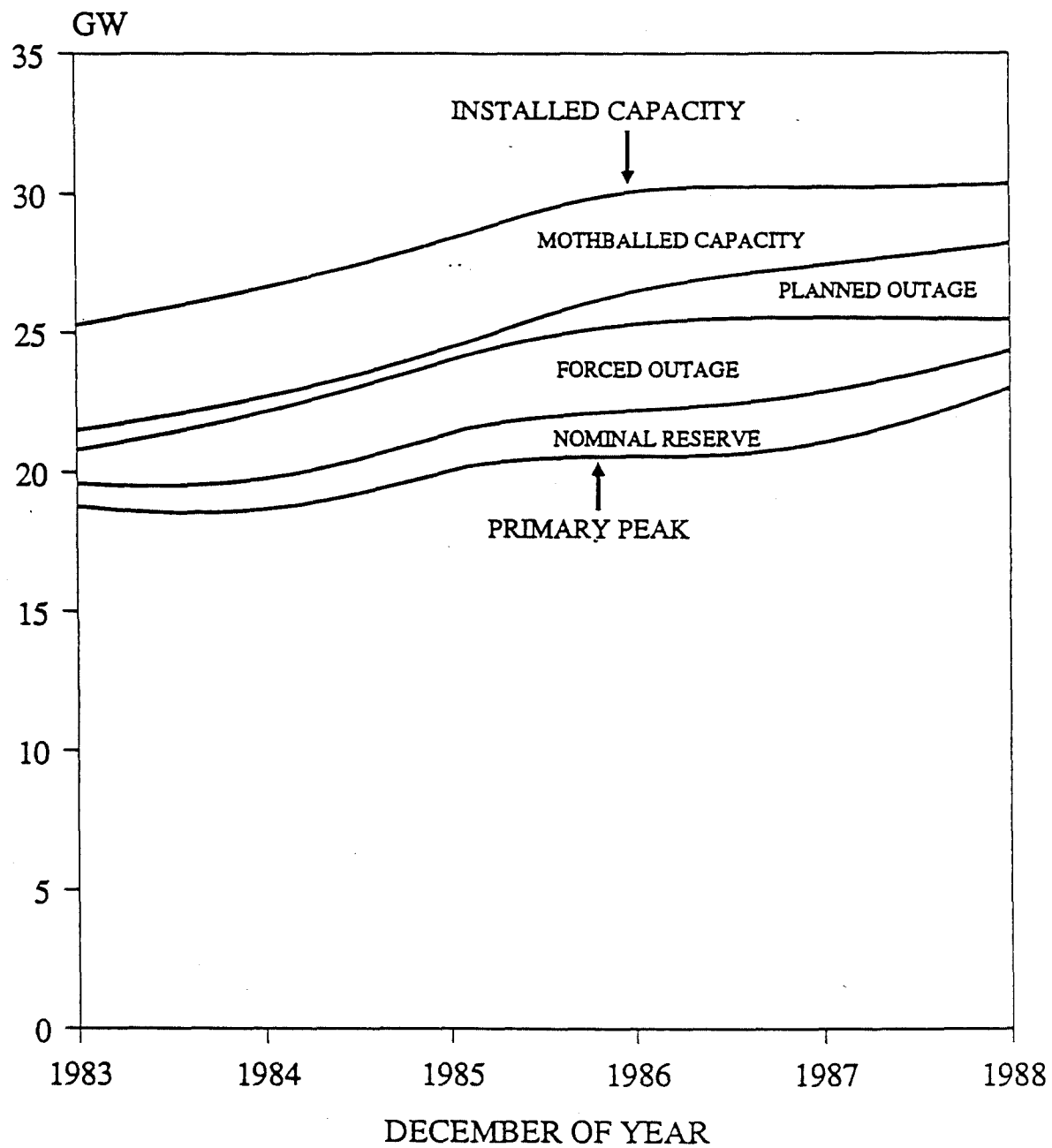
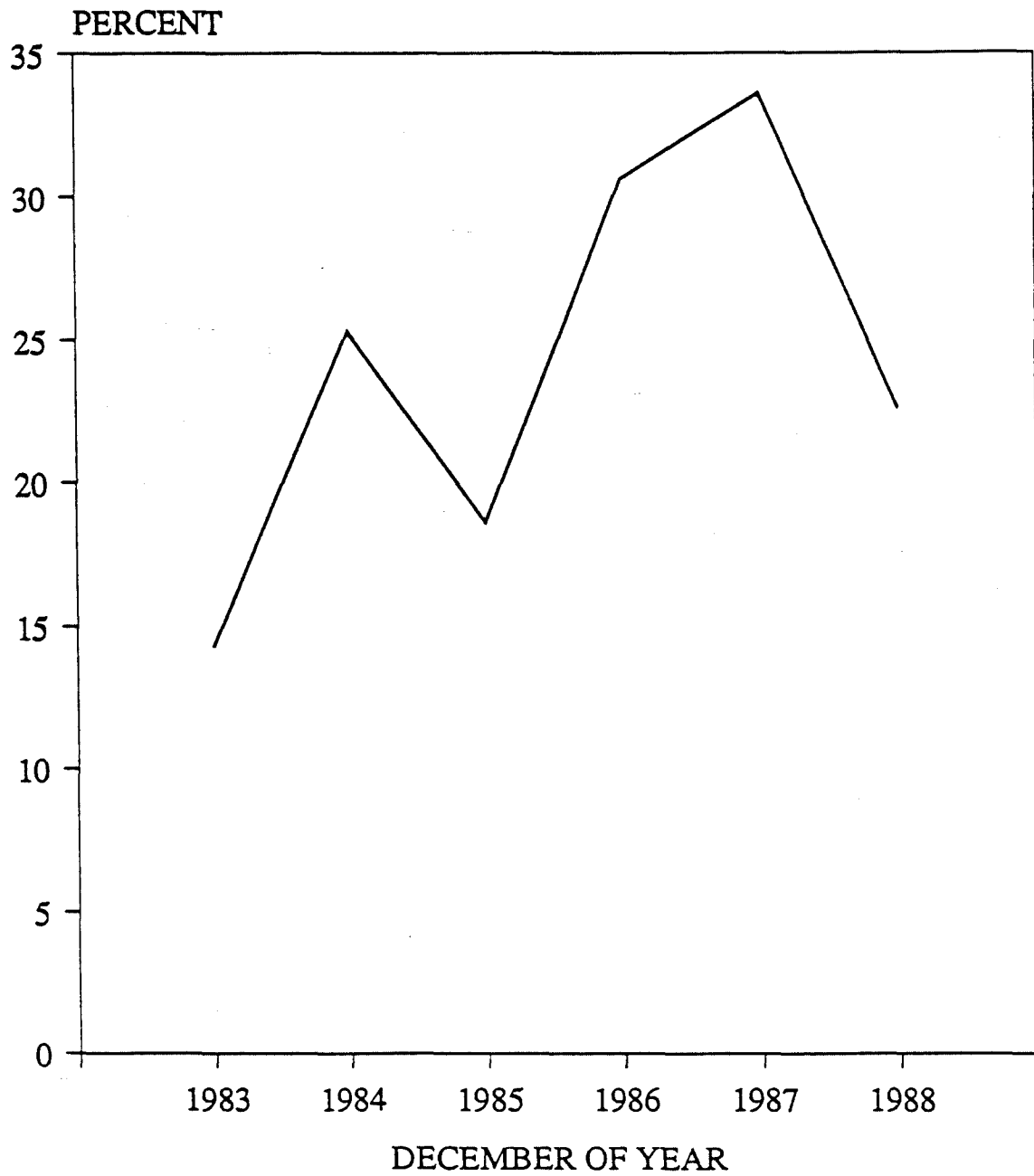


FIGURE 3-6c
HISTORICAL RESERVE MARGIN
(EXCLUDING MOTHBALLED CAPACITY)
1983 - 1988



3.6 MEASURING RELIABILITY

Generation reliability is estimated with a frequency and duration (F&D) analysis that compares generating capability from existing and new generating units with load and its specific characteristics. The generating capability of supply side resources and the level of customer demands are approximated by the supply and load models respectively in the F&D computations.

The supply model considers the impact of the following items:

1. Generating unit and non-utility generation reliability indices, i.e. forced outages, deratings, planned and maintenance outages;
2. Maturity of unit performances;
3. In-service date uncertainty for new units;
4. Lead time of new generating units;
5. Capacity assistance from neighbouring utilities equivalent to 700 MW of firm capacity.

The load model takes into account:

1. Variability of peak loads by day type, i.e. weekdays, weekends;
2. Daily load shapes;
3. Distribution of daily peak loads;
4. Effect of load shifting and demand management on daily load shapes;
5. Load forecast uncertainty.

Not considered in reliability calculations are:

1. "Common cause" events that would result in the shut down of several or all generating units at a station. See the following Section 3.6.1: Common cause events.
2. Catastrophic failures of generating units (failures due to normal wear and tear are considered in unit reliability indices);
3. Load forecast error beyond the range included in the uncertainty factor;
4. Strikes, shortage of major unit components;
5. Energy limitations of hydraulic generating units, e.g. low water levels or water use restrictions.

3.6.1 Common Cause Events

Certain events could cause several or all units at one generating station to be shut down unexpectedly. This would substantially reduce the amount of available generation and, because it is an unplanned outage, it could lead to increases in unsupplied energy, beyond those specified in the reliability criterion.

Some examples of common cause events are:

- Cooling water intake may be obstructed by fish, plants or other debris. As a result of insufficient cooling water, multiple generating units may have to be derated or even shut down.
- Generic design flaw may exist in new generating units, for example, the boiler hanger rods of Nanticoke units had to be replaced when they were put into service initially. Multiple units were taken out of service for this purpose in the mid-70s.
- Any planned or forced outage of vacuum building equipments will necessitate complete shutdown of all CANDU nuclear reactors linked to the common vacuum building. The vacuum building is one of many safety features designed to protect the public in case of accidents. One vacuum building is provided for a number of reactors; one for all eight units in Pickering NGS A & B, one each for Bruce A & B and Darlington NGSs, respectively.

3.7 MEETING THE RELIABILITY STANDARD

When Hydro set the 25 minute criterion in 1981, it established a method to quantify the amount of reserve margin needed to meet customer demand reliably. The calculation showed that this amount should be about 25 percent of planning firm load (PFL), depending on the data used in the reliability model. The latest estimate is 24 percent. This portion of generation is known as the "reserve margin".

Planning firm load, simply put, is total customer demand, minus that portion of capacity that is interruptible.

Since 1981, there have been some changes in system parameters such as load shape, demand management programs and outage factors of generating units. Hence, during the development of demand/supply plans, it was considered prudent to check whether the 24 percent target still provides sufficient generating reserve to meet the reliability standard. This was done by analyzing Cases 6 and 8.

These cases were selected from alternate demand/supply plans because they were representative of typical major supply plans using fossil and nuclear options. They were developed before the Manitoba Purchase option was finalized. Case 8 employs combustion turbines to satisfy near term capacity needs and nuclear stations for capacity and energy requirements in the long term. Case 6 is similar except that coal fired stations are used as instead of nuclear stations. Combustion turbines are included in both cases, when necessary, to bring the reserve margin to the desired target until base load generation is built.

The energy to be purchased from Manitoba will come from reliable hydraulic generating stations. Addition of the Manitoba purchase would not affect our reserve requirements; but in theory it should improve system reliability slightly.

The study data used in this reliability analysis are summarized here:

SUMMARY OF RELIABILITY STUDY DATA

<u>DATA</u>	<u>SOURCE OF INPUT/COMMENT</u>
Basic Load Forecast	December 1988 forecasts.
Demand Management, NUG, Load Shifting, Interruptible Loads	March 1988 forecasts
Load Forecast Uncertainty	It is assumed that the five load forecasts: lower, branch lower, median, branch upper and upper forecasts can vary by up to 12.6 percent in 8 years from the year when the forecasts are made.
Generating unit data	1988 Forecast of Reliability Indices for use in Corporate Planning Studies, Report 676 SP, March 1989. Due to data input limitations, only up to five yearly reliability indices can be used to model each of the DAFOR/DAUFOR, MOF and POF indices for each generating unit.
Nuclear Unit Retube Dates	February 6, 1989 proposed Schedule
Rehabilitation and Demothball Schedules	1989 Business Plan Assumptions/ Acid Gas Control Reference Plan, January 1989, Report 673SP
Retirement Dates	End of planned life of generating station
Combustion Turbine Unit Forced Outage Rates	North American Electric Reliability Council, Generation Availability Data System (NERC GADS), 1983-87 Statistics

3.7.1 Consequence of Inadequate Reserve

Figures 3-7a and 3-7b show what would happen to unsupplied energy and installed reserve margins, if no new capacity is added to Hydro's system after the completion of Darlington G.S. under median load forecast conditions. The level of unsupplied energy would begin to rise sharply as installed reserves begin to fall rapidly. By 2004, unsupplied energy reaches about 160 system minutes, more than six times the amount stipulated in our current reliability criterion. Contributions of economic demand management and non-utility generation were taken into account in this assessment.

Not considered in Figures 3-7a and 3-7b are two factors which would make reliability deteriorate more sharply than shown -- interruptible loads may switch to firm status when contract limits are reached; operating demands on hydraulic peaking stations during "off-peak" hours will reduce water availability, making peaking stations less able to meet peak demands.

3.7.2 Required Reserve

The generation reserve needed to meet the current 25 system-minute reliability criterion for Cases 6 and 8 under various load growth conditions are as tabulated in Figure 3-8 and shown in Figures 3-9a and 3-9b.

These results indicate that the required reserve, under all load forecast paths, ranges from 21 to 25% of planning firm load.

Based on the results in Figure 3-8, a target reserve level of 24% continues to be appropriate. This is also the reserve margin planned for other plans described in Chapter 4.0 - Formulation and Description of Plans.

FIGURE 3-7a
SYSTEM RELIABILITY
WITHOUT NEW CAPACITY ADDITION

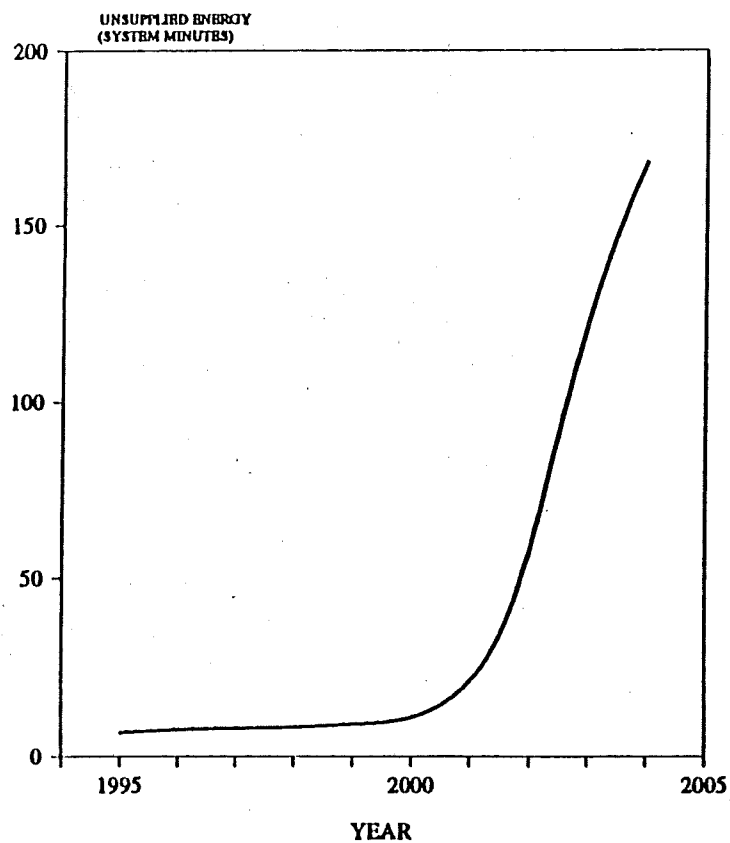


FIGURE 3-7b
SYSTEM RESERVE
WITHOUT NEW CAPACITY ADDITION

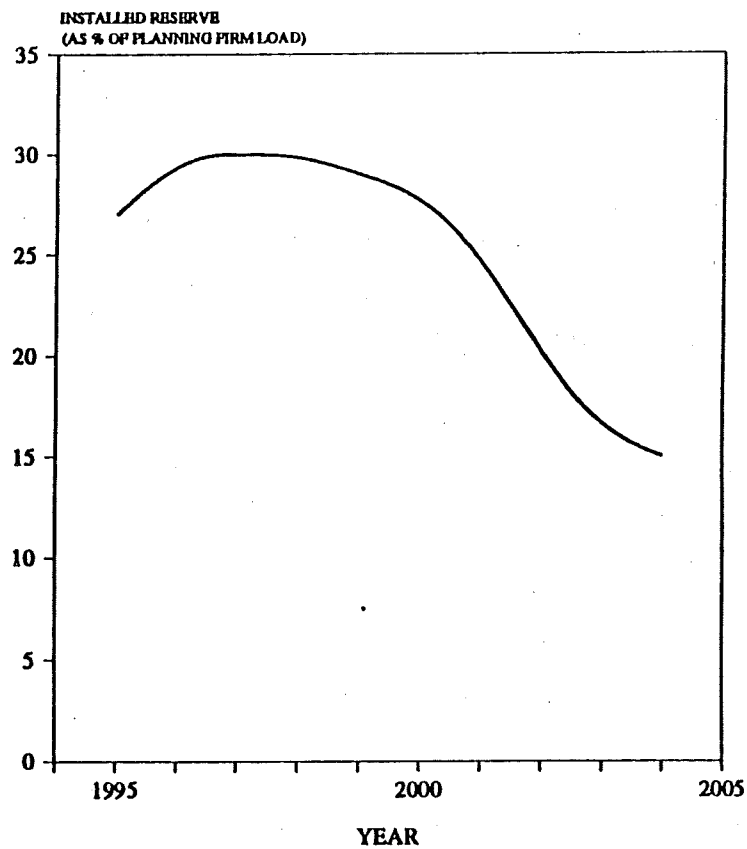


Figure 3-8

Required Reserve for Cases 6 and 8
Based on Frequency & Duration Computer Analysis

Case 6

<u>Load Growth</u>	<u>Reserve Margins (% of PFL)</u>
Upper	21.3 - 23.8
Branch Upper	22.6 - 25.0
Median	22.6 - 24.3
Branch Lower	22.8 - 24.6
Lower	23.9 - 25.3

Case 8

<u>Load Growth</u>	<u>Reserve Margins (% of PFL)</u>
Upper	21.5 - 22.9
Branch Upper	22.8 - 24.2
Median	22.3 - 23.9
Branch Lower	22.4 - 23.1
Lower	22.5 - 24.8

3.7.3 Key Generation System Reliability Variables

The reliability level of a generation system is dependent on two key variables: load characteristics and generation characteristics.

Load characteristics, including demand management, non-utility generation and interruptible loads, will be common for all alternative plans presented in Chapter 4.0 -- Formulation and Description of Plans.

Generation characteristics are a function of the performance of major generating units and the amount of reserve margin planned. As long as the reserve margins for any candidate demand/supply plans are maintained at levels similar to those for Cases 6 and 8, the reliability standard would be met. Specific supply options used

FIGURE 3-9a
CASE 6
REQUIRED RESERVE MARGIN
REQUIRED RESERVE
(AS % OF PLANNING FIRM LOAD)

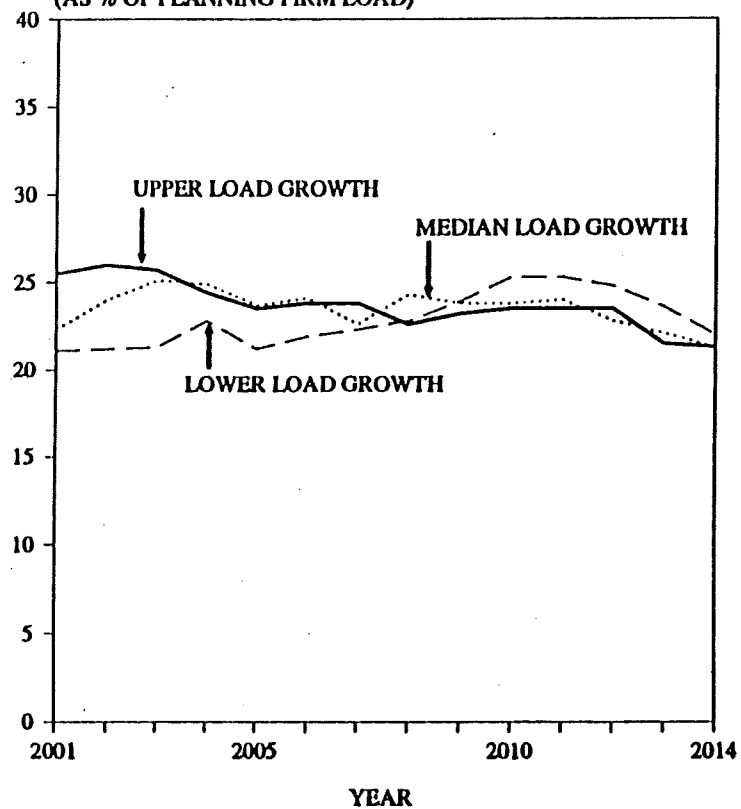
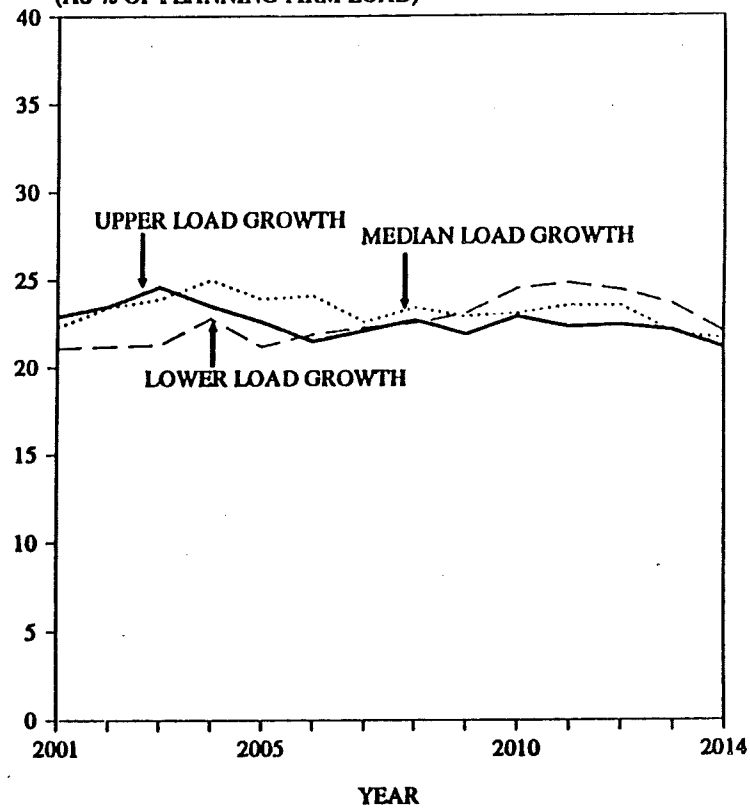


FIGURE 3-9b
CASE 8
REQUIRED RESERVE MARGIN
REQUIRED RESERVE
(AS % OF PLANNING FIRM LOAD)



in each alternate plan are not critical, because reliability indices for major supply options based on fossil or nuclear technology are not significantly different.

3.8 PLANNED RESERVE MARGINS

If the nominal reserve margin of 24 percent of Planning Firm Load is maintained, all five demand/supply plans can meet the 25 system-minutes of unsupplied energy criterion.

The planned reserve margin may vary from the 24% level. It will drop below 24% when short lead time capacity cannot be brought on-line soon enough to reach the 24% margin. When major generating units are built, their capacity can exceed the required reserve for load growth. As a result, the reserve margin can rise above 24% for a year or more.

Actual reserve levels have varied primarily because of load growth changes. Historic reserve margins are illustrated in Figure 3-10. (The reserve margin shown is expressed as a percentage of primary demand, as this is a measurable quantity, the planning firm load cannot be measured as easily.) Margins increase when load grows less than forecast, especially if new generation had been committed and could not be delayed economically.

Figures 3-11a and 3-11b illustrate the planned reserve levels for Cases 6 and 8 under median load growth. Reserve levels fluctuate in the near term due to major rehabilitation outages. It will rise above the 24% level in the early to mid-1990's as Darlington units come into service and as demand management, non-utility generation and hydraulic programs are implemented.

In years when this activity does not occur, for example 1993, the reserve margin for Case 8 climbs to just under 35 percent. In 1995, however, rehabilitation occurs and the margin drops to a level close to the reserve standard of 24 percent.

Around the year 2000, reserve margins will fall below 24 percent before they are restored.

Overall, reserve margins for Case 6 range from a high of 34 percent to a low of about 23 percent. For Case 8, it ranges from about 34 to 20 percent.

Figures 3-12 and 3-13 illustrate the planned reserves under upper and lower growth. These more clearly illustrate how reserves can vary: below the 24 percent target when there is insufficient time to respond to load growth increases; and above the target when load growth is slow and existing and committed resources exceed the

FIGURE 3-10
Historical Reserve Margin Levels

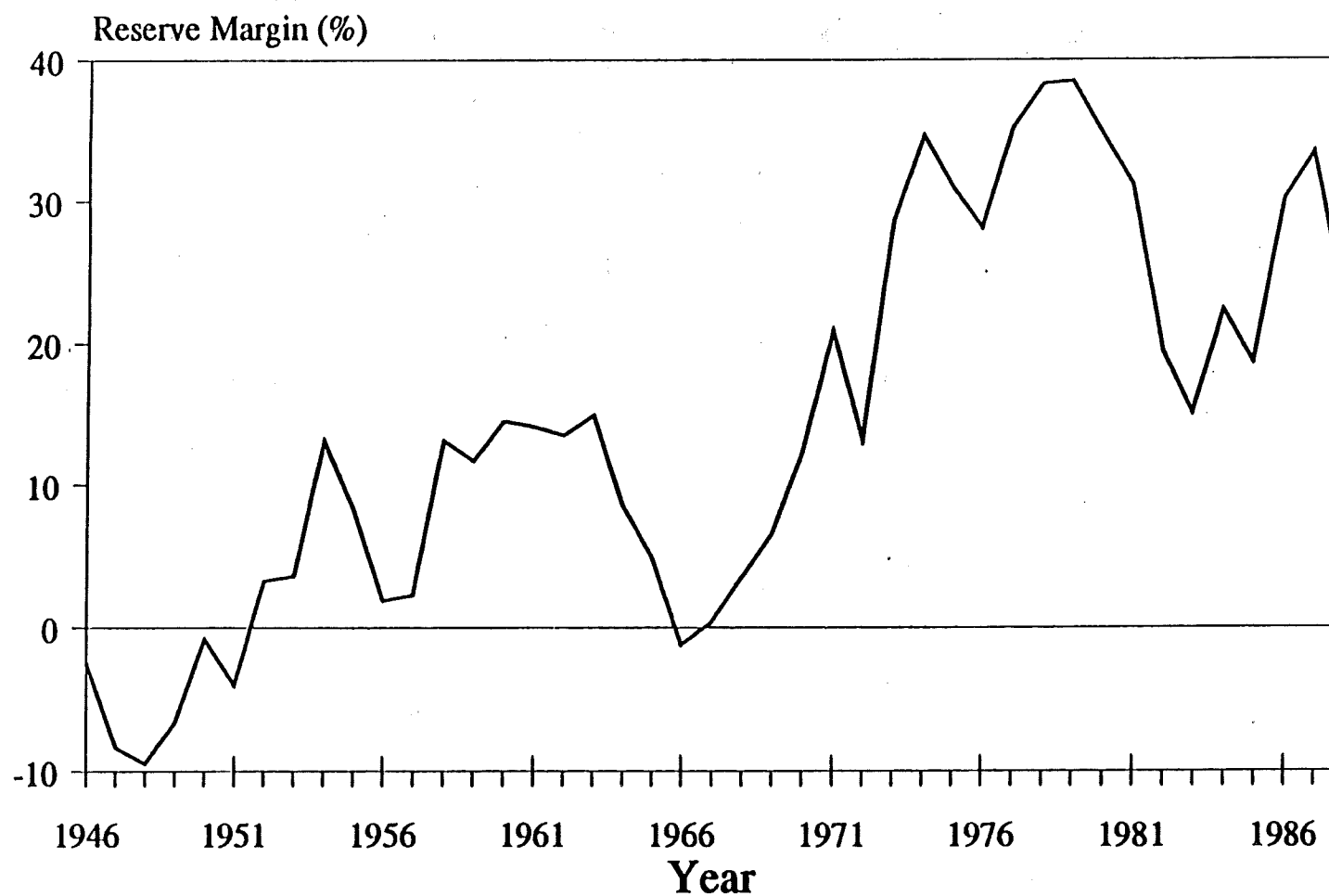


FIGURE 3-11a
1989 DEMAND SUPPLY PLAN RESERVE MARGINS
CASE 6
MEDIAN LOAD GROWTH

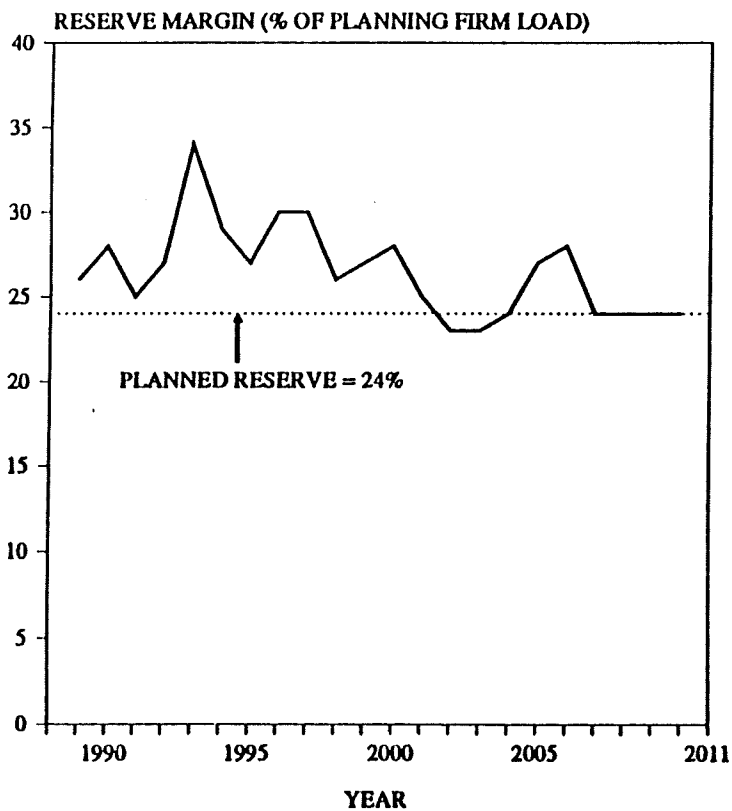
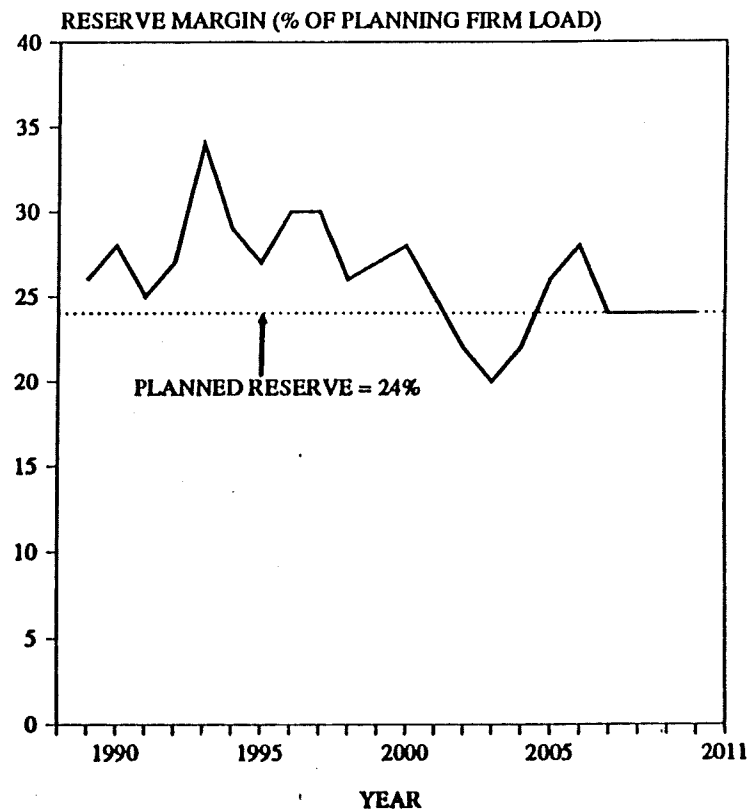


FIGURE 3-11b
1989 DEMAND SUPPLY PLAN RESERVE MARGINS
CASE 8
MEDIAN LOAD GROWTH



generation required to reliably supply electricity demand.

3.8.1 Comparing reserve levels with other utilities

Different utilities choose their reserve margins based on the nature of their systems, their experience, economic considerations and the reliability analysis tools considered appropriate for respective systems.

Hydro, as previously noted, expresses reserves as a percentage of planning firm load. Some other utilities measure reserves levels by "capacity margin" -- required reserve capacity expressed as a percentage of installed generation. Figure 3-14 provides the required reserve margins both as a % of PFL and % installed capacity respectively. As the installed generation is usually higher than planning firm load, the capacity margin expressed in terms of installed generation capacity is lower than reserve margin based on planning firm load.

Power systems with similar supply and demand characteristics will demonstrate similar need for reserve capacity, as indicated by the reserve margins shown in Figure 3-15 for various utilities with systems similar to Ontario Hydro.

Hydraulic generating units are usually more reliable than thermal electric generating units. Therefore, systems that are predominantly hydraulic, such as Hydro Quebec and Manitoba Hydro would require lower reserve margins.

FIGURE 3-12a
1989 DEMAND SUPPLY PLAN RESERVE MARGINS
CASE 6
UPPER LOAD GROWTH

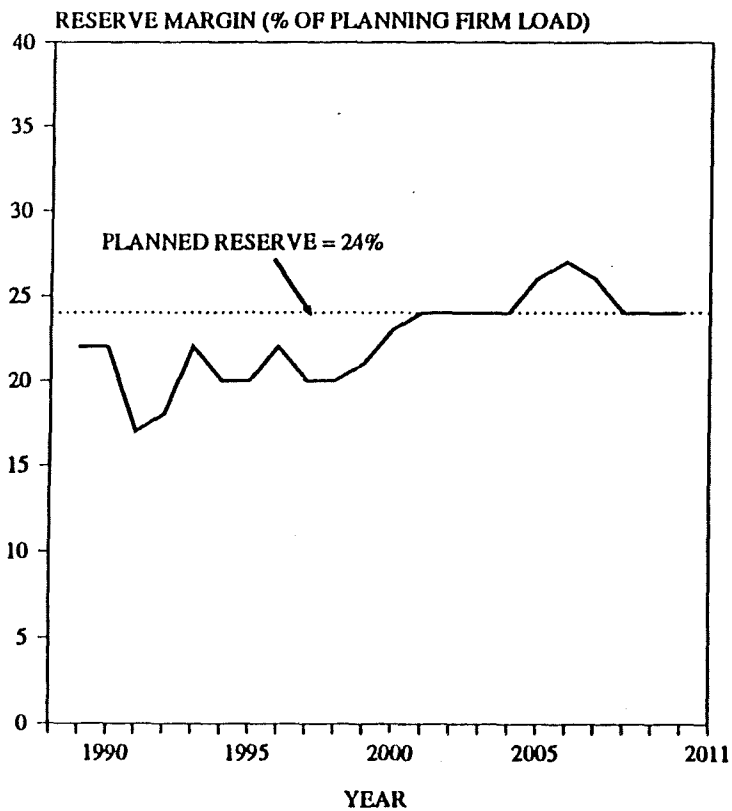


FIGURE 3-12b
1989 DEMAND SUPPLY PLAN RESERVE MARGINS
CASE 8
UPPER LOAD GROWTH

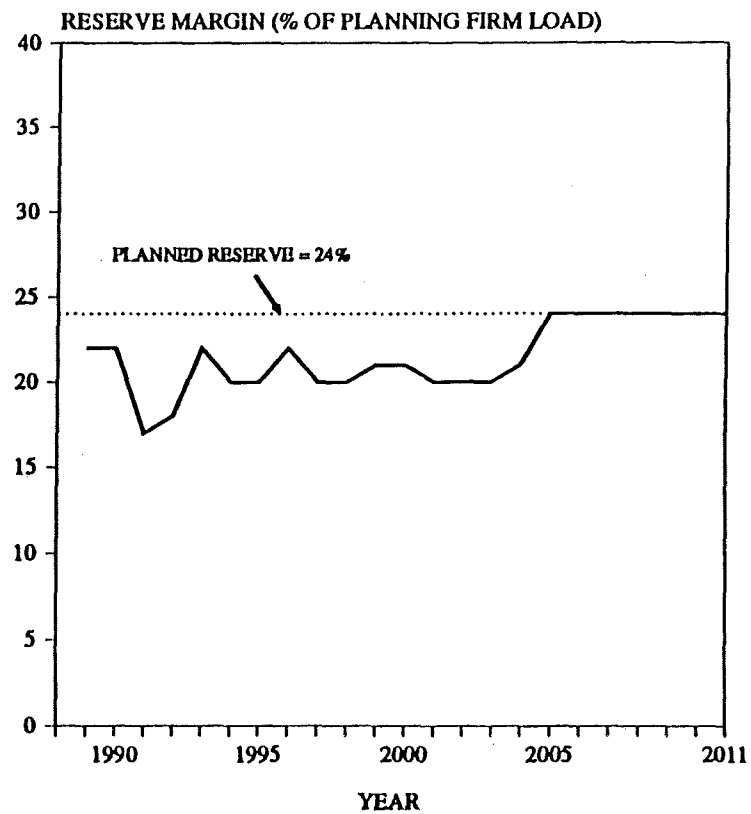


FIGURE 3-13a
1989 DEMAND SUPPLY PLAN RESERVE MARGINS
CASE 6
LOWER LOAD GROWTH

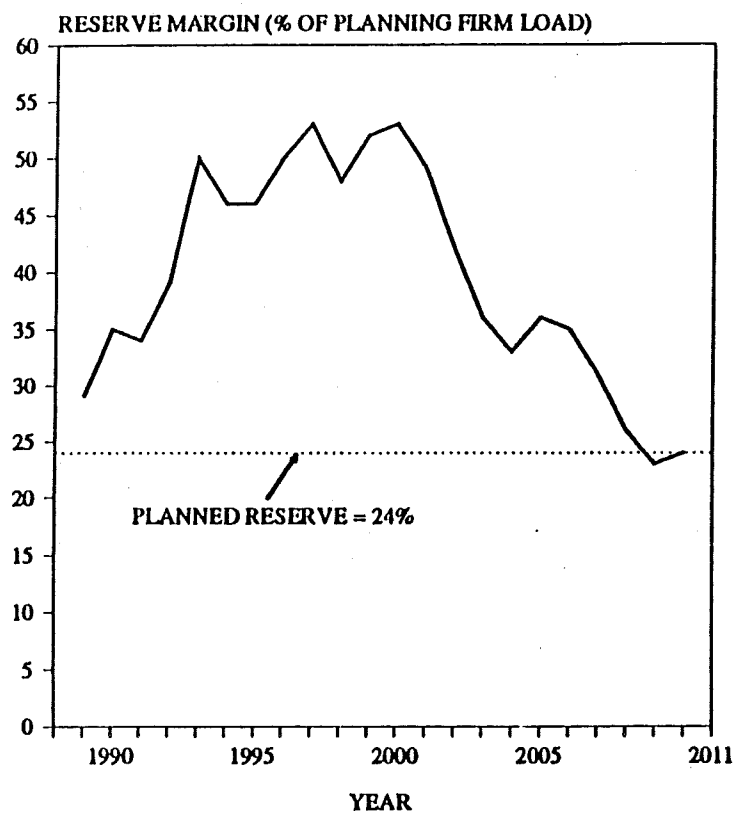


FIGURE 3-13b
1989 DEMAND SUPPLY PLAN RESERVE MARGINS
CASE 8
LOWER LOAD GROWTH

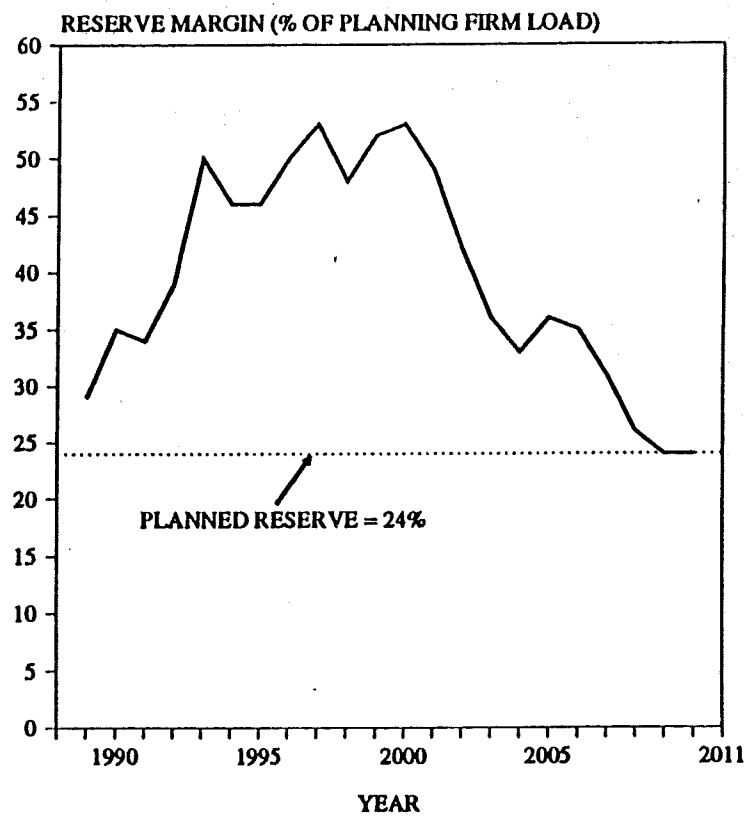


Figure 3-14

Required Reserve for Cases 6 and 8
Based on Frequency & Duration Computer Analysis

Case 6

<u>Load Forecast</u>	<u>Reserve margins (% of PFL)</u>	<u>Capacity margins (% of Installed Capacity)</u>
Upper	21.3 - 23.8	17.6 - 19.6
Branch Upper	22.6 - 25.0	18.0 - 19.5
Median	22.6 - 24.3	17.9 - 19.0
Branch Lower	22.8 - 24.6	17.7 - 19.0
Lower	23.9 - 25.3	18.5 - 19.5

Case 8

<u>Load Forecast</u>	<u>Reserve margins (% of PFL)</u>	<u>Capacity margins (% of Installed Capacity)</u>
Upper	21.5 - 22.9	17.3 - 17.8
Branch Upper	22.8 - 24.2	18.1 - 19.6
Median	22.3 - 23.9	18.0 - 19.5
Branch Lower	22.4 - 23.1	17.5 - 18.0
Lower	22.5 - 24.8	17.1 - 19.1

Figure 3-15

Reserve Margins Adopted by Various

North American Utilities

<u>Utility Name</u>	<u>Reserve Margin (% of Peak Load)*</u>
Ontario Hydro	24
Public Service Electric & Gas of New Jersey	22
New York Power Pool	22
Philadelphia Electric	22
Delmarva Power & Light, Delaware	22
Northeast Utilities, Hartford, Conn.	23-24
Michigan Electric Coordinated Systems	23
Commonwealth Edison	15-20
New Brunswick & Nova Scotia Power	20
Hydro Quebec	10
Manitoba Hydro	12

*Definition varies from utility to utility; Ontario Hydro specifies reserve margin as percentage of planning firm load.

3.9 REVIEW

Reserve margin provides the flexibility to handle equipment failures, load forecast errors or lower than expected demand management penetration or contribution from non-utility generation.

Ontario Hydro has a strong reliability record; albeit there were more interruptible load cuts and public appeals for reduced power consumption in recent years. In order to maintain good performance in the future, adequate reserve margins must be planned for future system expansion.

The long-term reserve margin (24% of planning firm load) used in the development of plans for the 1989 Demand/Supply Plan Study allows the system, as modified under each alternative demand/supply plan, to maintain the present reliability criterion (25 system minutes) in the long term.

While Hydro has selected a reserve target that is in the high end of the range required to meet the reliability criterion, over the long term the incremental cost of meeting that target is not significantly higher than it would be if Hydro selected a level lower in the range.

Also, providing slightly higher reserve does not lead to large increases in electricity rates charged to our customers. Provision of this extra reserve by non-capital intensive combustion turbine units (CTU) is more economic than more capital intensive coal-fuelled units, an alternative considered by the SEPR study.

Hydro's reserve levels are similar to those adopted by other similar utilities in North America.

In short, reserve margins are a form of insurance -- they carry a cost, but it is significantly below the costs that would be incurred if electricity service was unreliable.

4. FORMULATION AND DESCRIPTION OF PLANS

- 4.0 INTRODUCTION**
- 4.1 PLAN FORMULATION OVERVIEW**
- 4.2 STRUCTURE OF FOLLOWING SECTIONS**
- 4.3 BASIC FORECASTS**
- 4.4 THE EXISTING SYSTEM**
- 4.5 REQUIREMENT FOR DEMAND/SUPPLY OPTIONS**
- 4.6 COSTING CONCEPTS AND AVOIDED COST**
- 4.7 DEMAND MANAGEMENT PLAN**
- 4.8 NON-UTILITY GENERATION PLAN**
- 4.9 PRIMARY AND FIRM LOAD FORECASTS**
- 4.10 REHABILITATION PLAN**
- 4.11 REQUIREMENT FOR NEW SUPPLY**
- 4.12 THE HYDRAULIC PLAN**
- 4.13 REQUIREMENT FOR MAJOR SUPPLY**
- 4.14 MAJOR SUPPLY OPTIONS**
- 4.15 MAJOR SUPPLY PLANS**
- 4.16 AVOIDED COST DETERMINATION**
- 4.17 DEMAND/SUPPLY PLANS**
- 4.18 ACTION PLANS**
- 4.19 APPROVALS**
- 4.20 REVIEW**

APPENDIX

4.0 INTRODUCTION

The 1989 Demand/Supply Plan Report is one of the documents issued under the title "Providing The Balance Of Power: Ontario Hydro's Plan To Serve Customers' Energy Needs". It contains a relatively comprehensive discussion of the background to, and elements of, Hydro's Proposed Demand/Supply Plan to meet future needs. It also discusses some of the alternatives which were considered.

The Plan Report does not report exhaustively on all demand/supply cases which were examined since the end of 1988, when the demand/supply plan formulation and analysis process began in earnest. Rather, it presents the results of the "final" round of analysis which began in the fall of 1989 and was completed just prior to the public release of the Proposed and Candidate Plans.

Section 4.1 of this Analysis Report is provided as an overview of some of the many demand/supply cases which were considered during the earlier stages of the plan formulation and analysis process.

Chapter 15 of the Plan Report describes how cases were developed and tested the against five electricity demand paths (Upper, Branch Upper, Median, Branch Lower, and Lower forecasts). The Plan Report does not, however, present details on either the Branch Upper or Branch Lower forecasts; nor does it indicate the response of the five major supply cases to those branch forecasts. These items are covered in this chapter. The majority of this chapter (Sections 4.3 to 4.19) discusses how the need for major supply options under Branch Upper or Branch Lower forecast conditions was determined. It also indicates how the cases presented in the Plan Report would respond to these electricity demand paths.

The Plan Report contains a relatively detailed discussion of both the need for major new supply options and the resulting cases under Upper, Median, and Lower load forecasts. The vast majority of this material will not be repeated here. However, in some instances it was deemed useful to clarify or provide additional details on some of the assumptions and factors considered during the formulation of these demand/supply cases.

The opportunity is also taken to identify instances where data used during the formulation of demand/supply cases do not exactly match those reported in the Plan Report. These differences are shown to have no significant overall effect on the comparison and evaluation of cases.

4.1 PLAN FORMULATION OVERVIEW

As part of Hydro's on-going planning process there are frequent reviews and revisions of the load forecast, Demand Management and Non-utility Generation Plans, and projections of future economic conditions. Similarly, the suitability of existing and new generating technologies is constantly reassessed in light of Hydro's and others' experience with the technology, changing environmental requirements, societal preferences, and the costs, reliability, and safety of the option. Throughout the demand/supply planning process, this "changing landscape" was explicitly taken into account by frequently updating the information upon which the analysis was based, and by making corresponding adjustments to the demand/supply cases. The cycle of updating cases, analyzing them, reviewing the analysis and then adjusting cases was, and remains a continuous, iterative process.

The five major supply cases described in the Plan Report represent the most recent iterations in this process. The following few paragraphs summarize demand/supply cases which were developed, analyzed, and refined during preceding iterations of the demand/supply planning process.

FIRST PHASE

The preliminary phase of demand/supply case formulation and analysis began in the Fall of 1988 and continued until the Spring of 1989. Much of this time was spent gathering data and improving computer simulation models used to analyze cases. Toward the latter stages of this period, as data became more refined, it became practical to begin to formulate and analyze demand/supply cases. These preliminary cases were created for two purposes.

Most importantly, they were created so that the various analysis tools and techniques could be exercised on "sample problems" to ensure that they worked effectively and efficiently to provide the required analytical results.

Secondly, the cases were created in such a way as to represent a broad range of potential major supply plans. By analyzing these using the preliminary data then available, it was possible to begin to identify those broad categories of plans which warranted further investigation.

A wide variety of cases was formulated and subjected to preliminary analysis at this time. Some of these included only nuclear additions after 2002; and some employed only CTUs to meet all future load growth. There were cases in which one or more major fossil stations (CSC-Coal or IGCC) were always added before any nuclear additions; and others were just the opposite. A number of cases were formulated in which new nuclear generation was always added very late in the planning period to study the effect of minimizing initial capital expenditures. Still other cases were designed to dramatically reduce CO2 emissions by installing more nuclear than might otherwise be required.

It was soon recognized that major supply cases which included only CTU generation were unlikely to be economic and that those which relied exclusively on new nuclear plant could not maintain system reserves at an adequate level under Upper load forecast conditions. Hence, primary consideration was given to major supply cases which featured a mixture of new fossil peaking resources (CTUs and/or CTU/CC and/or CTU/IGCC) and new baseload generation comprised of nuclear, CSC-Coal plant and/or IGCC plant.

When this analysis was performed, data on the Demand Management and Non-utility Generation Plans, the program for new hydraulic development, and the retubing and retirement schedules were not yet finalized. The probable unit sizes for new fossil stations were still being investigated and the purchase of 1000 MW from Manitoba, which now figures in all plans presented in the Plan Report, was not yet incorporated. As well, the costs associated with radial transmission and with obtaining the required approvals prior to the commitment of new generation were not fully captured at this point. Hence, although the results of this preliminary analysis were useful for indicating which general features of cases should be investigated further, the results cannot be compared directly to those presented in the Plan Report.

Because of their preliminary nature, none of the cases developed and analyzed in this first phase of the process were formally assigned case designation numbers (as in "Case 15" of the Proposed Demand/Supply Plan).

SECOND PHASE

Before the second major phase of demand/supply case formulation and analysis was begun, the assumptions about the retirement of aging existing plant were finalized and incorporated into the models. The retirement schedule used is the same as that reported in the Plan Report. By this point, various details regarding fossil unit characteristics and costs had been compiled and submitted for review by an independent consultant as part of the Thermal Cost Review. Computer model data

files were modified as needed to incorporate that information. New cases were formulated which reflected these changes as well as the insights gained during the first round of analysis.

Demand/Supply cases were developed which included mixtures of nuclear, IGCC, and CSC-Coal baseload facilities, and CTU peaking plant, either as stand-alone CTUs, or the first phase of CTU/CC or CTU/IGCC. The goal of most of the analysis performed during this phase was to determine the effect of varying the relative amounts (quantity and timing) of new peaking and baseload plant under the five load forecast paths.

Early in May, 1989 cases developed to that point and found to warrant further investigation were assigned "case numbers". Case numbers 4,5,6,7,8,and 9 were assigned arbitrarily to the then existing cases. Case numbers 1 through 3 were saved for future use, as were the numbers following 9 (in fact, case numbers 1, 2, and 3 never were used). The cases which were identified and analyzed had the following general characteristics:

<u>CASE NUMBER</u>	<u>DESCRIPTION</u>
4	A mix of new nuclear baseload and CTU for peaking, with no new baseload plant prior to 2007.
5	A mix of new nuclear plus a postulated purchase of 1000 MW of power from Manitoba for baseload, with new CTUs added for peaking as needed. The dates upon which new nuclear is to be added were chosen in an attempt to minimize overall demand/supply case cost, consistent with the need to respect leadtimes required to place new major facilities into service.
6	A case with IGCCs serving all new baseload with CTUs added for peaking.

CASE NUMBER

DESCRIPTION

7

A predominantly nuclear case with the first new nuclear plant added as early as 2000. All new baseload additions are nuclear, and CTUs are added for peaking.

8

A case falling between Case 4 and Case 7, with new nuclear baseload added on a schedule which attempts to minimize overall demand/supply case costs. As well as analyzing this case under the "nominal" set of assumptions used for studying the other cases in this list, its behaviour under various changes to those assumptions was examined. These included three scenarios: imposition of more stringent acid gas control regulations; escalation of fossil fuel prices more than expected; significant delays in obtaining approvals for nuclear generation. Examination of the response to these scenarios helped to better define the degree of flexibility which cases could exhibit.

9

A case similar to Case 8, but with a 4x800 MW CSC-Coal fired station reducing the number of peaking CTUs needed after 2007.

Analysis of the cases listed above began in the Spring of 1989 and continued through to the middle of the Summer.

THIRD PHASE

In mid-August, a third round of data modification, case revision, and re-analysis began. This opportunity was taken to incorporate into the computer model used for case simulation and analysis, revisions to the forecast of capacity interruptible load, the non-utility generation forecast, and the future hydraulic generation program. The

revised levels of load reduction and new generation, which were incorporated at that time, were eventually carried through to the final analysis and are discussed in following sections of this chapter.

The cases which were analyzed at this point were given case numbers 12, 14, 15, 16, and 18 to distinguish them from those created in previous rounds of analysis. The cases were as follows:

<u>CASE NUMBER</u>	<u>DESCRIPTION</u>
12	This case was similar to Case 8 (see above) but with additional new nuclear units to reduce acid gas and CO2 emissions.
14	A case similar to Case 18, described below, but with the first major new baseload facility being a 4x800 MW CSC-Coal plant rather than a new nuclear station.
15(rev 1)	Similar to Case 5, but reflecting changes necessitated by the revised hydraulic, NUG, and CIL forecasts. The then current terms of the 1000 MW purchase from Manitoba were also incorporated into this case.
16	A case similar to Case 6, but incorporating 4x800 MW CSC-Coal plants for baseload operation rather than IGCCs.
18(rev 1)	A case similar to Case 8, but reflecting updated modelling data. The timing of new nuclear baseload additions reflects two objectives: minimizing overall demand/supply case cost, and reducing acid gas and CO2 emissions.

Case numbers 10, 11, 13, 17, and 19 were not used.

FOURTH PHASE

By the early fall of 1989, the terms of the Manitoba Purchase had become much more clear and it appeared likely that an agreement to purchase would be reached. This necessitated another iteration of case revision and re-analysis. All but one of the cases formulated and analyzed in this final phase incorporated the 1000 MW Manitoba Purchase described in the Plan Report. As it turned out, this was to be the final round of analysis before publication of the Proposed Plan.

The analysis performed at this stage explicitly considered the cost impacts of the illustrative sites described in the Plan Report. In particular, the costs of transmission required to incorporate new facilities located at defined illustrative sites, and the estimated costs of obtaining the necessary approvals for those sites, were modelled.

The cases considered during this final iteration of formulation and analysis are listed below. Note, again, that case designation numbers were not assigned on a sequential basis.

<u>CASE NUMBER</u>	<u>DESCRIPTION</u>
18(rev 2)	This is the same as Case 18(rev 1) but with explicit consideration of radial transmission and approval costs for defined illustrative sites. This case did not include the Manitoba Purchase.
15(rev 2)	This is the Case 15 described in the Plan Report. It is essentially identical to Case 15(rev 1), but with new Manitoba Purchase terms and with the costs associated with radial transmission and illustrative site approvals incorporated.
20	Similar to Case 15(rev 2), but with the first new nuclear station replaced by a 4x660 MW unphased IGCC facility.

CASE NUMBER

DESCRIPTION

- | | |
|----|--|
| 21 | An all fossil case providing new IGCC plant for baseload and CTU for peaking. Similar to Case 6, but analyzed with revised data and incorporating the Manitoba Purchase. |
| 22 | This is the "Higher Nuclear" case described in Chapter 15 of the Plan Report. It is similar to Case 12. |
| 23 | This case is presented in Chapter 15 of the Plan Report. It is the case in which most new major supply requirements are provided by new nuclear generation in order to reduce CO2 emissions. |
| 24 | <p>Two versions of this case were created. The first was similar to Case 15, but with the first new nuclear station replaced by a 4x800 MW CSC-Coal fired facility. This was Case 14 with the new Manitoba Purchase terms and with explicit consideration of the illustrative siting effects on costs.</p> <p>The second version of this case was similar to Case 15, but with the second new nuclear plant replaced by a 4x800 MW CSC-Coal station. This is the "Higher Fossil" Candidate Major Supply Plan (Plan 24) referred to in the Plan Report.</p> |
| 26 | In this case, discussed in Chapter 15 of the Plan Report, all new major supply requirements are provided by new 4x800 MW CSC-Coal generation. It is similar to Case 16. |

Each of these cases was created by bringing to bear the considerable judgement and experience gained by analyzing literally hundreds of cases in the preceding phases of the analysis. This same judgement and experience was used to help determine which of the many major supply cases should be presented in the Plan Report, and which of those should be advanced as the Proposed Plan and acceptable Alternative Plans.

Of those examined in the final phase of analysis and listed immediately above, Cases 18, 20, 21, and the first version of Case 24 were not carried through to the Plan Report.

Case 18 was eliminated when it became apparent that a purchase agreement with Manitoba Hydro for 1000 MW of capacity would, in fact, be signed.

To date, the world's utilities have had relatively little experience with the IGCC option. Hydro's judgement is that this promising but new technology is not sufficiently mature to be relied upon heavily to serve near term baseload requirements. Hence, Cases 20 and 21 were not carried through to the Plan Report. Note, however, that the appearance of phased CTU/IGCC facilities (in which the conversion of CTUs to a fully fledged IGCC station is delayed) in the Proposed and Alternative Plans is indicative of Hydro's expectation that the technology will be proven as experience is gained by various other utilities.

In the earlier version of Case 24, a 4x800 MW CSC-Coal plant was provided as the first major baseload facility, followed by new nuclear stations, as required, to meet all other baseload needs. Hydro's judgement was that such a case would not adequately comply with the intent of the Demand/Supply Planning Strategy (specifically, consideration number 5.8: "Ontario Hydro will seek to maintain CANDU nuclear so that it is available for future development"). The second version of Case 24, in which a 4x800 MW CSC-Coal fired station is built after the first new nuclear station, was judged to be an acceptable alternative, and was carried through to the Plan Report.

4.2 STRUCTURE OF FOLLOWING SECTIONS

The chapters in the "Plan Report" were arranged to describe the various elements of the planning process in a sequence which shows their logical linkages. In general terms, that report shows how the requirement for additional demand/supply options was determined, how feasible options to meet that requirement were identified, and

how plans to put these options into place in a timely manner were developed and analyzed.

The structure of the remainder of this chapter mirrors the Plan Report. For each chapter of the Plan Report, the reader will find a correspondingly numbered subsection of this chapter which supplements the information present in the Plan Report. For example, subsection 4.3 of this chapter of the Analysis Report provides details of the basic forecast which were not presented in Chapter 3 of the Plan Report.

The primary purpose of the remainder of this chapter of the Analysis Report is to present the details of the Branch Upper and Branch Lower load forecast paths and describe how the five major supply cases presented in the Plan Report respond to those branch forecasts.

4.3 BASIC FORECASTS

Chapter Three of the Plan Report stresses the importance of considering load forecast uncertainty when developing flexible plans to meet future electricity needs. For the Proposed and Alternative Demand/Supply Plans, this was done explicitly by developing planning cases which were capable of responding to future load growth which falls within the "bandwidth forecast".

As indicated in the Plan Report text, the bandwidth forecast for basic electrical energy needs covers 80% of the expected future outcomes for load growth. There is a 10% probability that the basic energy demand will be higher than the upper bound of the bandwidth forecast and a 10% probability that it could be less than the lower bound of the forecast range.

Five basic load forecast paths which fall within this bandwidth forecast were developed. The "Median" forecast is the most likely electricity demand in each year in the study period. The "Upper" forecast is the upper bound of the bandwidth forecast, and the "Lower" path is the lower bound of electricity demand. The Upper, Median, and Lower basic forecasts are presented in detail in Chapter 3 of the Plan Report. In addition to these three forecasts, a "Branch Upper" forecast and a "Branch Lower" forecast were developed. The Branch Upper forecast was developed to model a case in which load growth proceeds along the Median path until 1995, when demand accelerates and tends toward the Upper forecast. Similarly, the Branch

Lower forecast proceeds along the Median path until 1995, when demand is assumed to slow and tend toward the Lower forecast.

Each of the major supply cases presented in the Plan Report was tested under the five load forecast paths to ensure that the cases had adequate ability to respond to changes in electricity demand. The Upper and Lower forecast paths exercise the ability of the demand/supply cases to respond to a demand for electricity which is consistently different from that expected (Median forecast). This tests the suitability of the short term actions in the case. This also, in a sense, tests the "stamina" of the cases - their ability to respond to a prolonged onslaught of load growth which is faster or slower than expected.

The Branch Upper and Branch Lower forecasts help highlight the cases' agility:- their responsiveness to an unexpected, rapid change in demand in the mid 1990s.

Any of the demand/supply cases studied could result in an undercommitment or overcommitment of resources if demand grows faster or slower than expected after a major supply facility is committed. All cases were tested using the Branch Upper load forecast path to determine their ability to avoid or minimize long term impacts of undercommitting resources in the mid- to late- 1990s, when the Branch forecast diverges from the Median forecast. Similarly, the Branch Lower forecast path was used to test the ability of the cases to avoid or minimize the effects of overcommitments of resources.

Figure 3-10 of the Plan Report presents the detailed Basic Energy forecast for the Upper, Median, and Lower forecast cases. Figure 4.3-1 is a table which presents those three forecasts as well as the Branch Upper and Branch Lower Basic Energy forecasts used in case analyses. Figure 4.3-2 compares these five forecasts. Note that the Branch forecasts are identical to the Median forecast until after 1995 - the year in which the forecasts were assumed to diverge.

The 20-minute January Basic Peak Power forecasts which were used when formulating demand/supply cases under the five load forecast conditions are tabulated in Figure 4.3-3 of this report. This Figure corresponds to Figure 3-12 of the Plan Report. Figure 4.3-4 presents these five forecasts graphically and is analogous to Figure 3-13 of the Plan Report.

The annual average basic energy growth rates in percentage and absolute (TWh per year) terms are presented for all five load forecast paths in Figures 4.3-5 and 4.3-6, respectively. These figures correspond to Plan Report Figures 3-14 and 3-15.

The Basic forecasts presented in Figures 4.3-2 and 4.3-4 form the starting point in the determination of the need for new demand/supply options, and in the subsequent formulation and analysis of demand/supply cases.

**Figure 4.3-1: BASIC LOAD FORECAST BANDWIDTH
ANNUAL ENERGY (TWh)**

Year	Lower	Branch Lower	Median	Branch Upper	Upper
1989	132	137	137	137	142
1990	133	140	140	140	147
1991	135	145	145	145	154
1992	137	151	151	151	162
1993	138	155	155	155	169
1994	139	159	159	159	176
1995	141	163	163	163	180
1996	141	163	165	167	185
1997	143	165	169	174	192
1998	146	167	174	180	198
1999	149	170	178	186	205
2000	153	172	184	194	212
2001	159	178	192	204	221
2002	163	181	196	210	227
2003	166	184	201	216	231
2004	167	185	202	219	234
2005	168	186	205	222	236
2006	171	188	208	226	240
2007	174	191	211	231	242
2008	178	193	214	234	245
2009	181	196	217	237	247
2010	185	199	220	241	250
2011	188	201	224	245	252
2012	191	204	227	249	255
2013	194	207	230	252	257
2014	197	209	234	256	260

FIGURE 4.3-2
BASIC LOAD FORECAST BANDWIDTH
ANNUAL ENERGY (TWh)

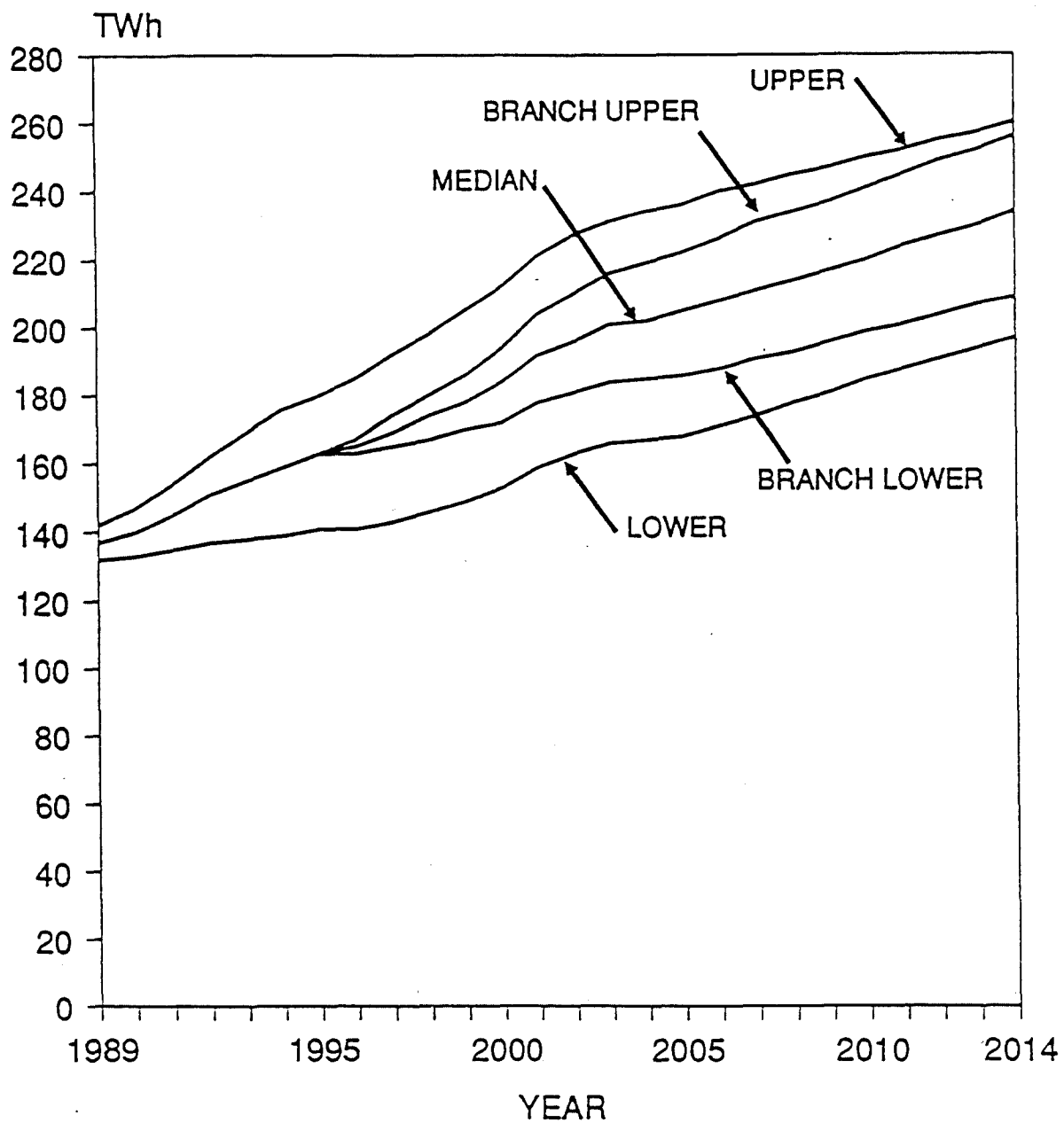


Figure 4.3-3: BASIC LOAD FORECAST BANDWIDTH
20-MINUTE JANUARY PEAK POWER (GW)

Year	Lower	Branch Lower	Median	Branch Upper	Upper
1989	22.7	23.2	23.2	23.2	24.0
1990	22.5	23.8	23.8	23.8	24.9
1991	22.8	24.5	24.5	24.5	26.0
1992	23.2	25.5	25.5	25.5	27.4
1993	23.5	26.3	26.3	26.3	28.7
1994	23.7	26.9	26.9	26.9	29.8
1995	23.9	27.5	27.5	27.5	30.8
1996	24.2	28.0	28.1	28.3	31.6
1997	24.2	28.1	28.7	29.3	32.6
1998	24.7	28.4	29.4	30.4	33.6
1999	25.1	28.8	30.2	31.5	34.8
2000	25.7	29.3	31.1	32.7	36.0
2001	26.6	30.1	32.3	34.2	37.4
2002	27.8	30.8	33.3	35.5	38.6
2003	28.2	31.4	34.1	36.5	39.5
2004	28.7	31.6	34.5	37.2	40.1
2005	28.6	31.8	34.9	37.8	40.6
2006	29.0	32.1	35.4	38.5	41.1
2007	29.6	32.5	35.9	39.2	41.6
2008	30.1	32.9	36.4	39.9	42.1
2009	30.7	33.4	37.0	40.4	42.5
2010	31.2	33.9	37.5	41.0	42.9
2011	31.9	34.3	38.1	41.7	43.3
2012	32.4	34.8	38.6	42.3	43.8
2013	33.0	35.2	39.2	43.0	44.2
2014	33.5	35.6	39.8	43.6	44.7

FIGURE 4.3-4
BASIC LOAD FORECAST BANDWIDTH
20-MINUTE JANUARY PEAK POWER (GW)

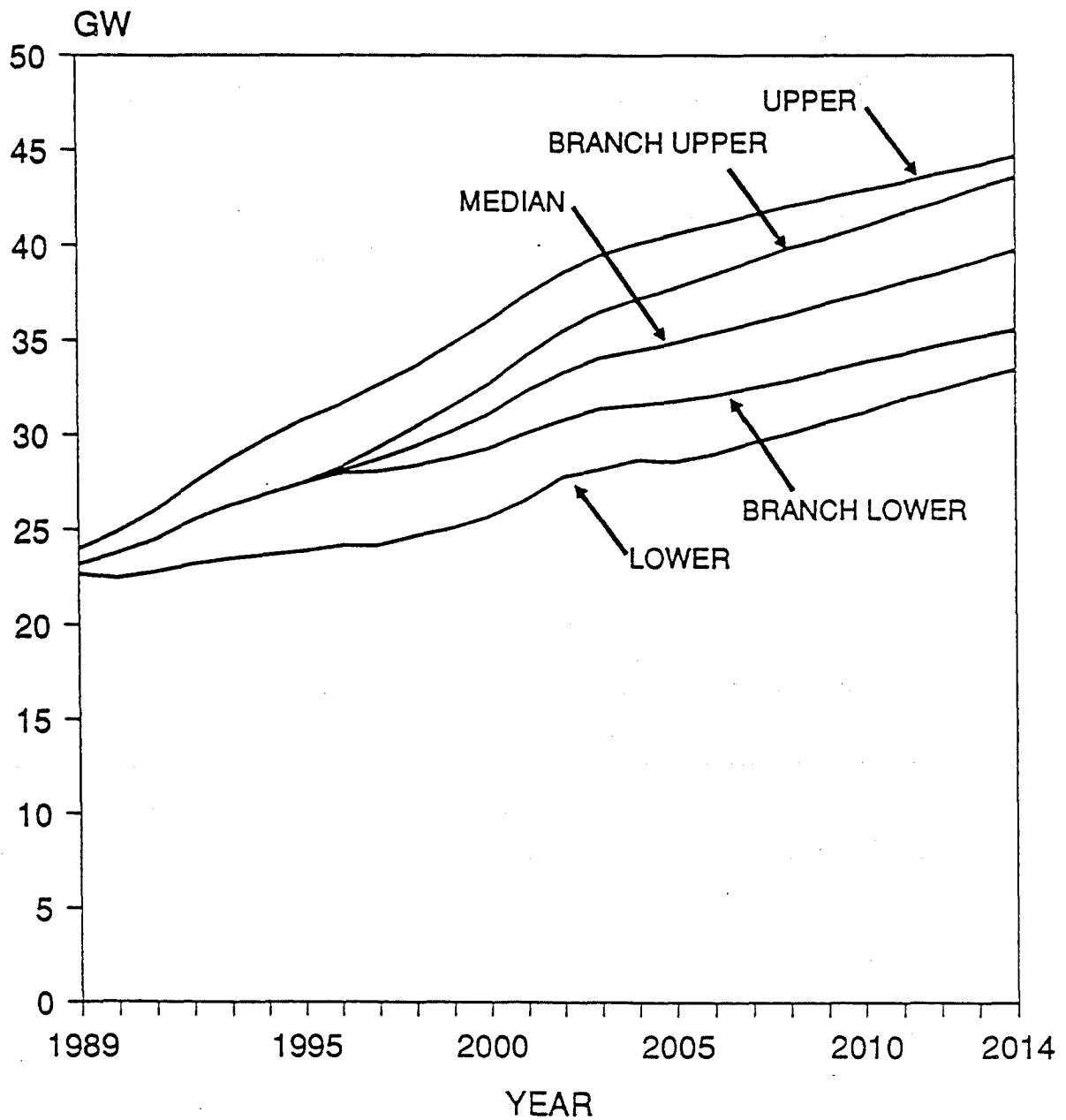


FIGURE 4.3-5
BASIC LOAD FORECAST
AVERAGE ANNUAL GROWTH RATES FOR ENERGY (%)

PERIOD	LOWER	BRANCH LOWER	MEDIAN	BRANCH UPPER	UPPER
1987-1995	1.33	3.18	3.18	3.18	4.53
1987-2000	1.47	2.40	2.93	3.36	4.05
1987-2010	1.66	1.98	2.44	2.84	3.00
1987-2014	1.66	1.88	2.30	2.65	2.71

FIGURE 4.3-6
BASIC LOAD FORECAST
AVERAGE ANNUAL ABSOLUTE GROWTH FOR ENERGY (TWh/YEAR)

PERIOD	LOWER	BRANCH LOWER	MEDIAN	BRANCH UPPER	UPPER
1987-2000	2.0	3.5	4.4	5.2	6.6
2000-2014	3.2	2.6	3.6	4.4	3.4
1987-2014	2.6	3.1	4.0	4.8	4.9

4.4 THE EXISTING SYSTEM

Prior to developing demand/supply cases, the capabilities and characteristics of all existing generating system facilities were determined. Generating units expected to retire within the 25 year planning period were identified and an estimate was made of how the existing system's capabilities were likely to change. The projected load meeting capability of the existing system and the generating unit retirement schedule upon which this was based were assumed to be the same for all five load forecast paths.

Chapter 4 of the Plan Report presents the existing system's projected load and energy meeting capability and describes how this was determined. That chapter also discusses the retirement of existing system resources.

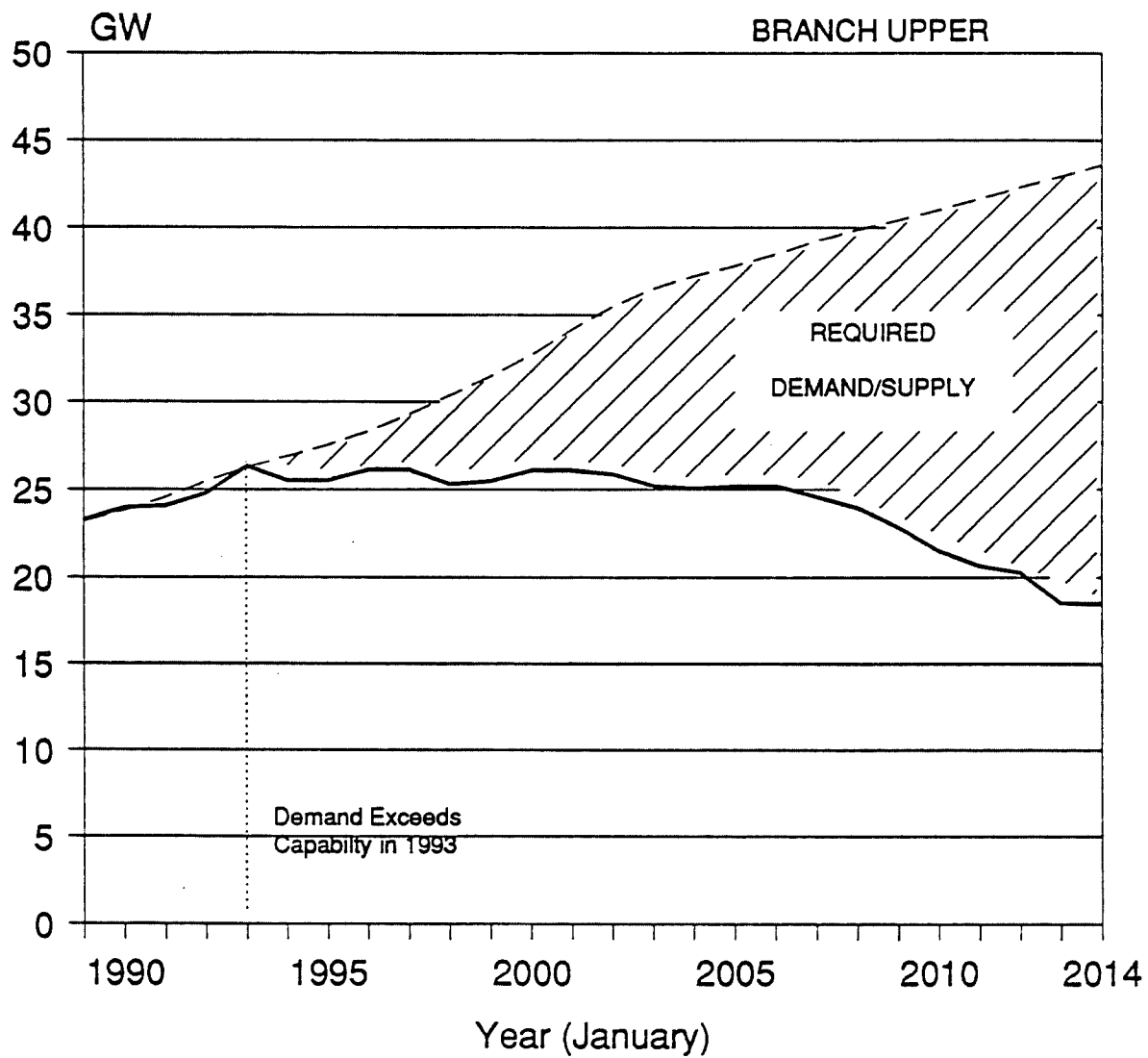
4.5 REQUIREMENT FOR DEMAND/SUPPLY OPTIONS

The requirement for new demand/supply options in any given year is the difference between the forecast need for electrical service and the ability of the system to serve those needs reliably. Put another way, it is the difference between the forecast basic demand in a given year and the projected load meeting capability of the existing system. Hydro's Demand/Supply Plans attempt to provide a suitable mix of demand reducing and electricity supply options to meet needs across the five load paths of the bandwidth forecast.

Figures 5-1 through 5-3 of the Plan Report show the Basic load forecast, the load meeting capability of the existing system (with allowance for retirements), and the requirement for new demand/supply options for the Upper, Median, and Lower load paths for the period to 2014. Analogous to these figures are Figure 4.5-1 for the Branch Upper forecast and Figure 4.5-2 for the Branch Lower. The year in which demand exceeds capability is 1993 for both the Branch Upper forecast and the Branch Lower forecast. This is the same year in which demand exceeds capability for the Median load forecast, which is consistent with the fact that the Median, Branch Upper, and Branch Lower forecasts are identical until after 1995.

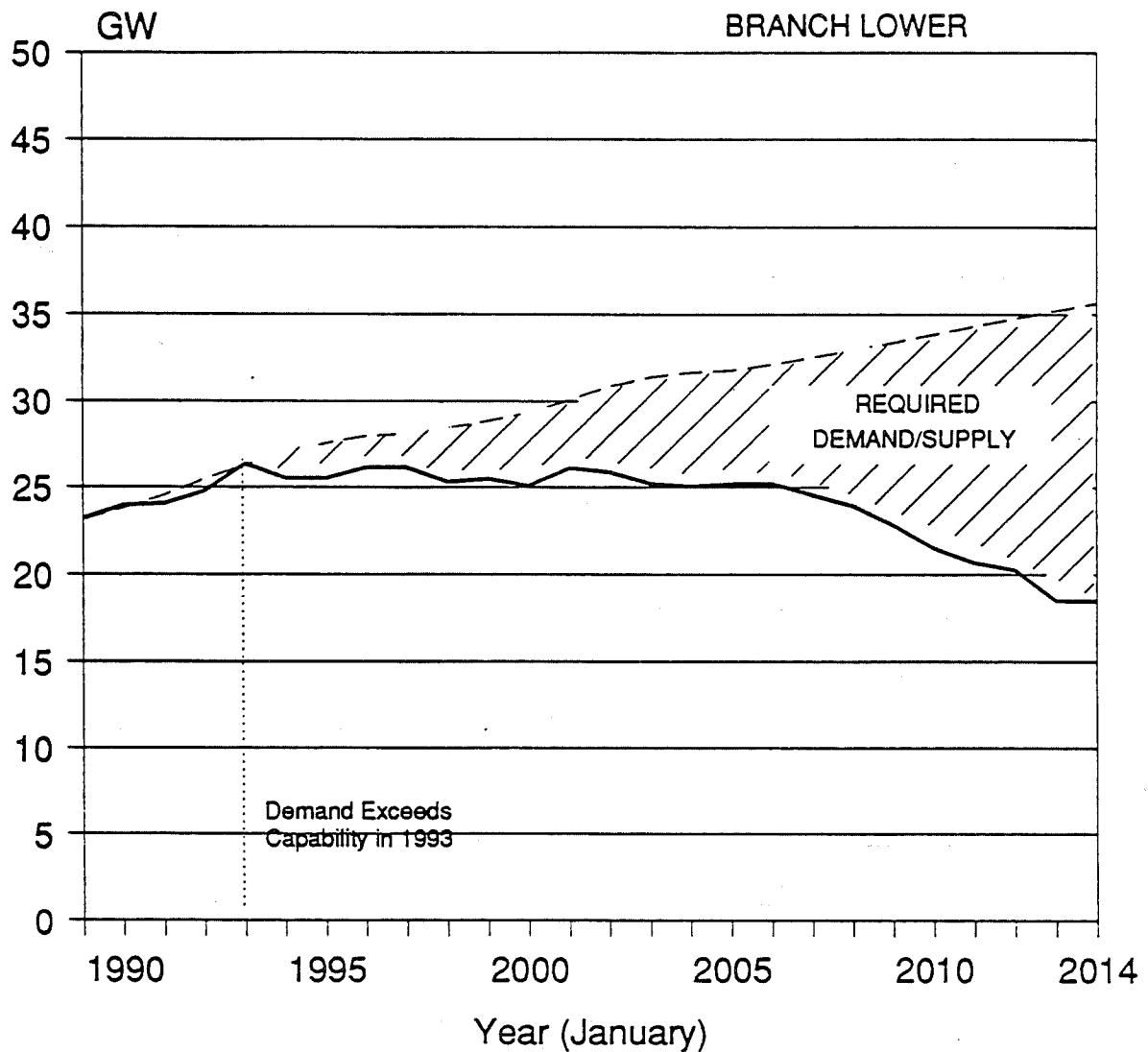
Figure 4.5-3 presents a graph of required demand/supply in terms of load meeting capability for all five load forecasts. This curve is analogous to Figure 5-5 of the Plan Report. Figure 4.5-4 is a table of required demand/supply load meeting capability for selected years, and is analogous to Figure 5-4 of the Plan Report.

FIGURE 4.5-1
REQUIRED DEMAND/SUPPLY
20-MINUTE PEAK POWER DEMAND



expressed in terms of LMC

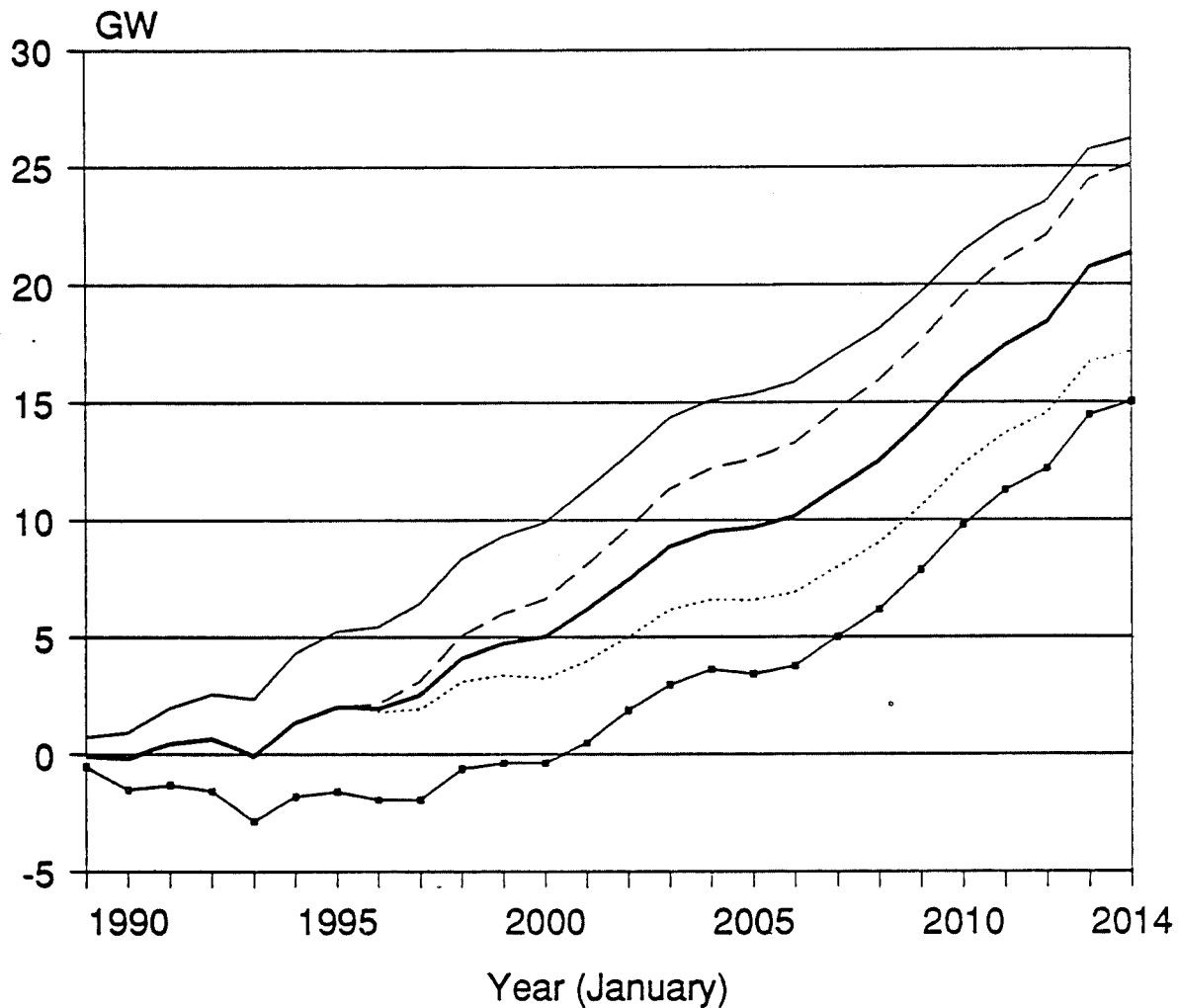
FIGURE 4.5-2 REQUIRED DEMAND/SUPPLY 20-MINUTE PEAK POWER DEMAND



Branch Lower Basic Load Forecast	Existing System Load Meeting Capability
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expressed in terms of LMC

FIGURE 4.5-3
REQUIRED DEMAND/SUPPLY
20-MINUTE PEAK POWER DEMAND



expressed in terms of LMC

FIGURE 4.5-4

Requirements* for New Demand/Supply Options (GW)

January of Year	Lower Forecast	Branch Lower Forecast	Median Forecast	Branch Upper Forecast	Upper Forecast
1990	0	0	0	0	0.9
1995	0	2.0	2.0	2.0	5.2
2000	0	3.2	5.0	6.6	9.9
2005	3.4	6.6	9.7	12.6	15.4
2010	9.8	12.4	16.0	19.6	21.4
2014	15.0	17.2	21.3	25.1	26.2

* Load-meeting capability.

Figures 4.5-5 and 4.5-6 present the Branch Upper and Branch Lower energy forecasts respectively, along with the reference energy meeting capability of the existing system (with retirements as appropriate). Similar curves for the Upper, Median, and Lower forecasts are shown in the Plan Report, Figures 5-6 through 5-8. As in the Median forecast, the required demand/supply in both branch forecasts exceeds the reference energy meeting capability of the existing system in 1993.

Figure 4.5-7 shows the need for new demand/supply options, in terms of energy demand, for all five load forecasts, and is analogous to Figure 5-10 of the Plan Report. Figure 4.5-8 shows the requirement for future energy reductions and/or new supply for a number of selected years, and is analogous to Figure 5-9 of the Plan Report.

4.6 COSTING CONCEPTS AND AVOIDED COSTS

This subject matter is covered in detail in Chapter 6 of the Plan Report and in Chapter 8 of this Analysis Report, and will not be discussed further here.

4.7 DEMAND MANAGEMENT PLAN

The Demand Management Plan contains initiatives for load reduction through electrical efficiency improvements, load shifting through time-of-use rates and direct load control, and peak clipping through capacity interruptible load contracts. To permit timely plan formulation, the relative contributions of each of these facets of demand management were estimated late in 1988. At that time, it was recognized that the degree of attainable demand management would be a function of load growth. The potential contribution of demand management to reductions in load would likely be greater in situations where basic load growth was relatively high.

The forecasts of attainable energy efficiency improvements and load shifting which were developed late in 1988 were carried through to the final round of demand/supply case formulation and analysis. The forecast of capacity interruptible load used when formulating and analyzing demand/supply cases was revised most recently in August of 1989. Figures 4.7-1 through 4.7-5 depict the levels of Demand Management assumed to be attainable for each of the five load forecasts when the final round of case formulation and analysis was undertaken. Figure 4.7-6 presents the same data on a year-by-year basis and is similar to Figure 7-22 in the Plan Report.

FIGURE 4.5-5
REQUIRED DEMAND/SUPPLY
ANNUAL ENERGY DEMAND

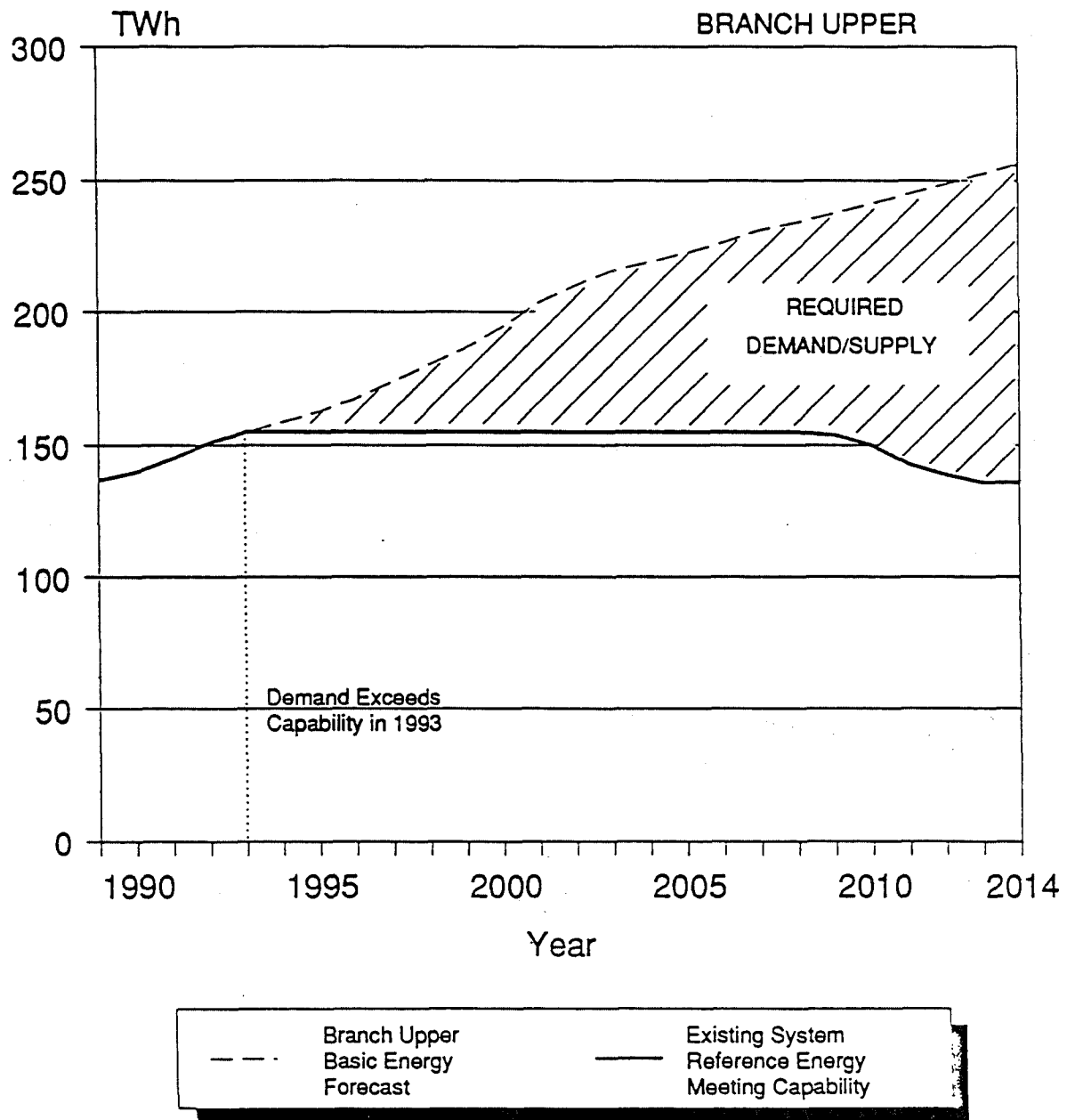


FIGURE 4.5-6
REQUIRED DEMAND/SUPPLY
ANNUAL ENERGY DEMAND

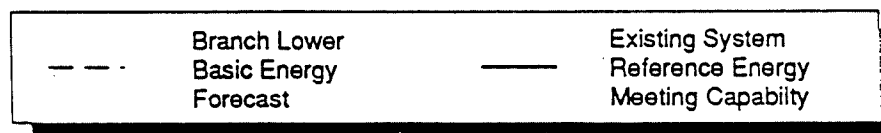
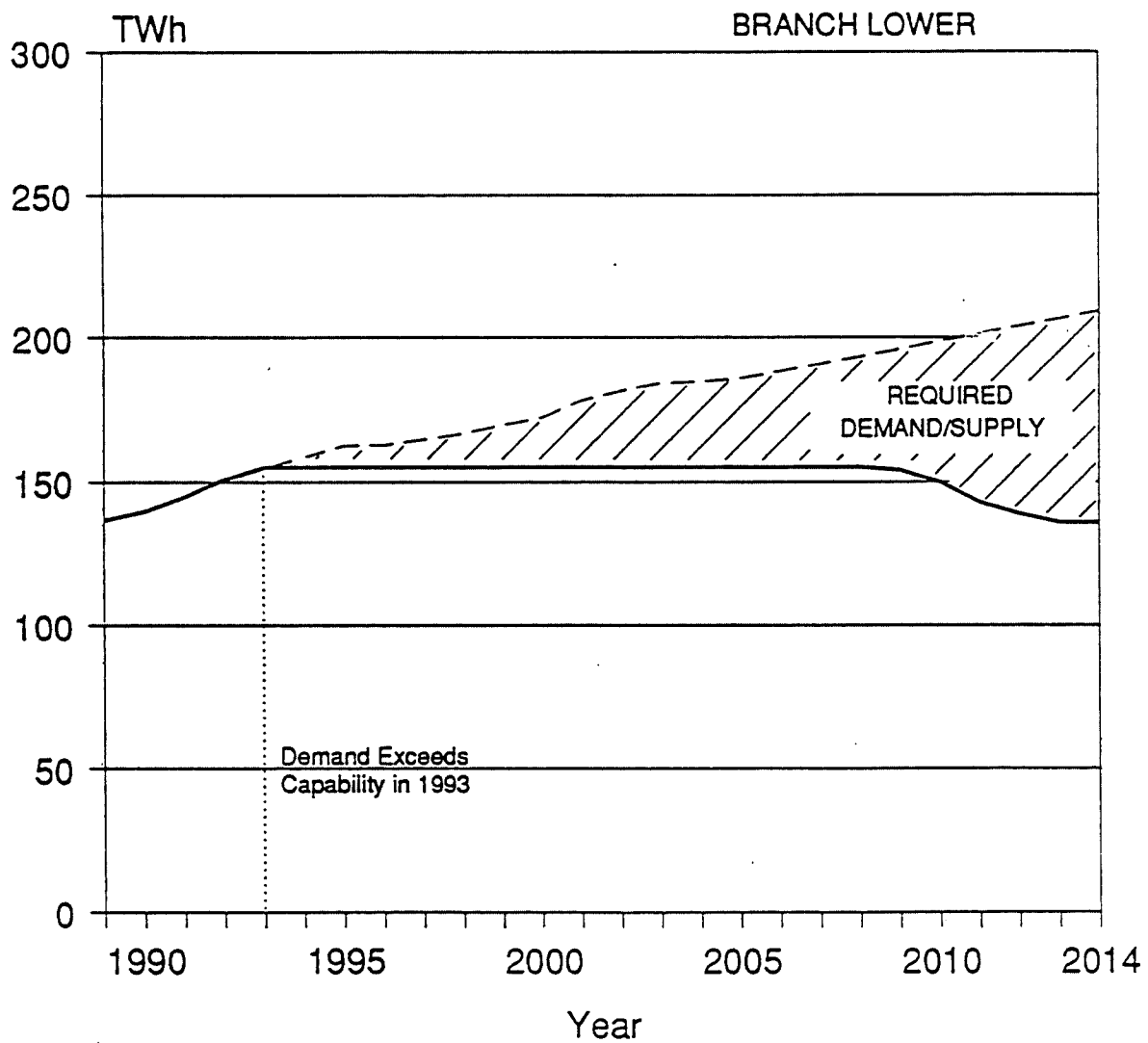


FIGURE 4.5-7
REQUIRED DEMAND/SUPPLY
ANNUAL ENERGY DEMAND

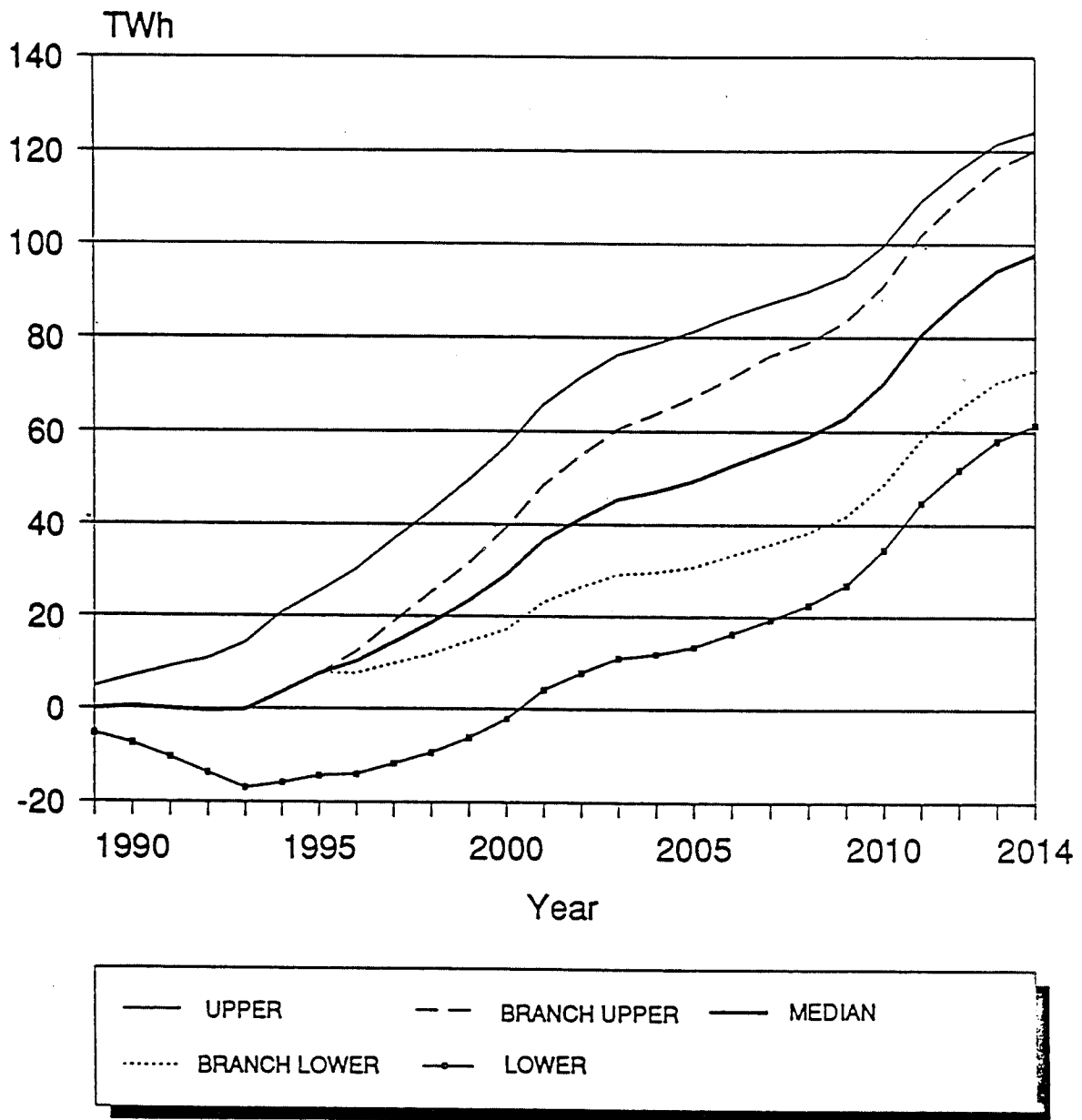


FIGURE 4.5-8
Future Energy Requirements (TWh)

January of Year	Lower Forecast	Branch Lower Forecast	Median Forecast	Branch Upper Forecast	Upper Forecast
1990	0	0	0	0	7
1995	0	8	8	8	25
2000	0	17	29	39	57
2005	13	31	50	67	81
2010	35	49	70	91	100
2014	61	73	98	120	124

FIGURE 4.7-1
DEMAND MANAGEMENT DATA
USED FOR ANALYSIS
LOWER LOAD FORECAST

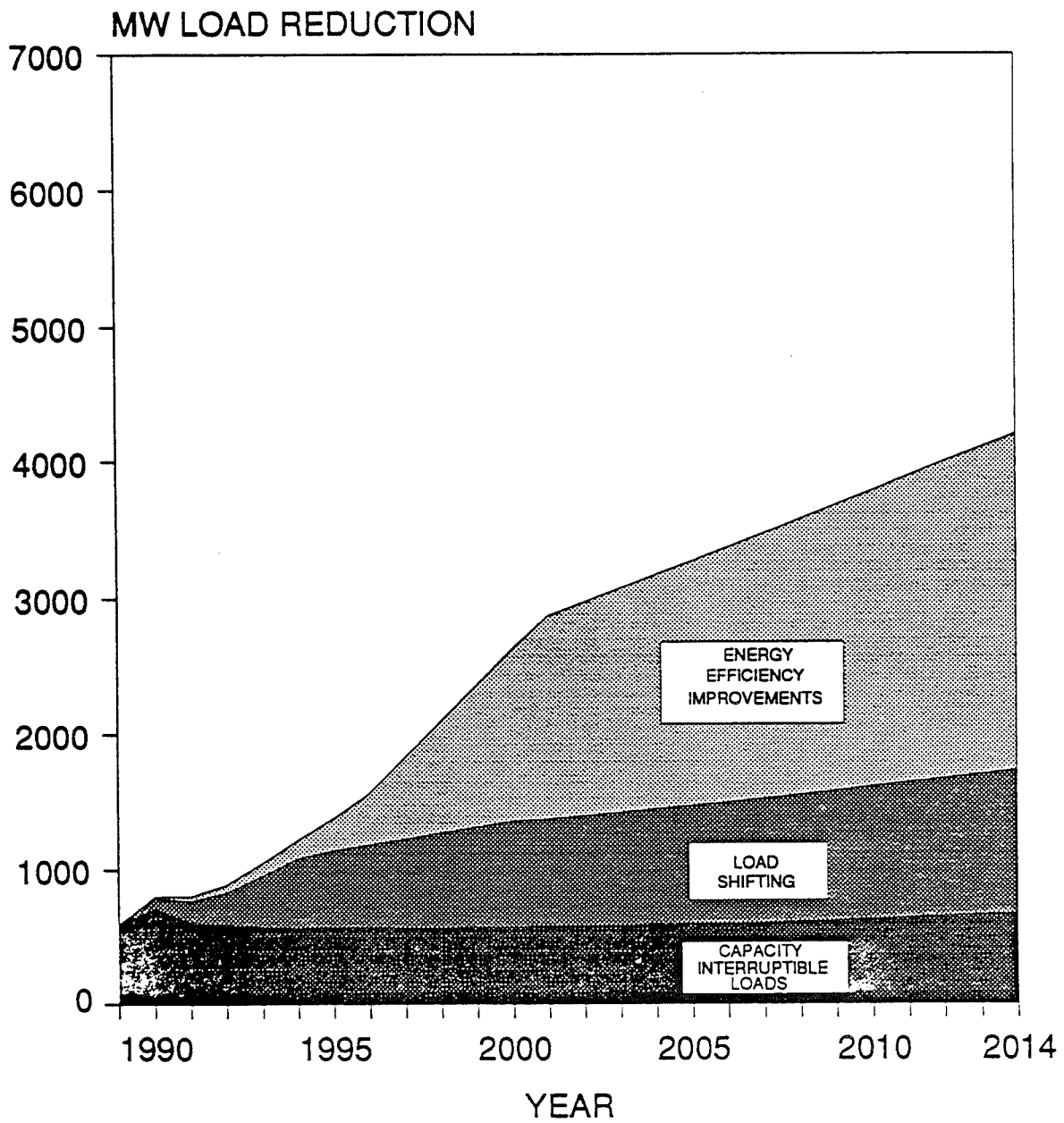


FIGURE 4.7-2
DEMAND MANAGEMENT DATA
USED FOR ANALYSIS
BRANCH LOWER LOAD FORECAST

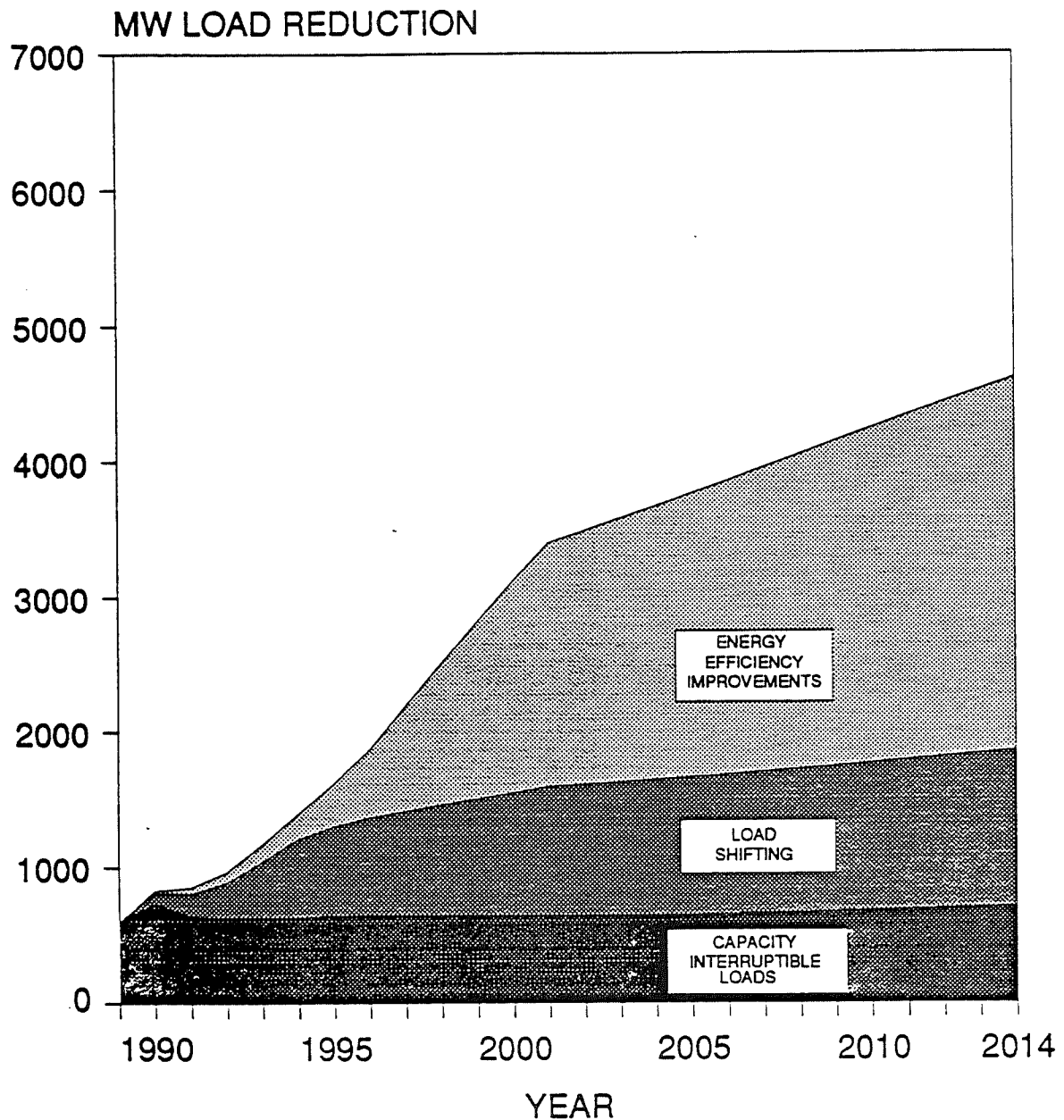


FIGURE 4.7-3
DEMAND MANAGEMENT DATA
USED FOR ANALYSIS
MEDIAN LOAD FORECAST

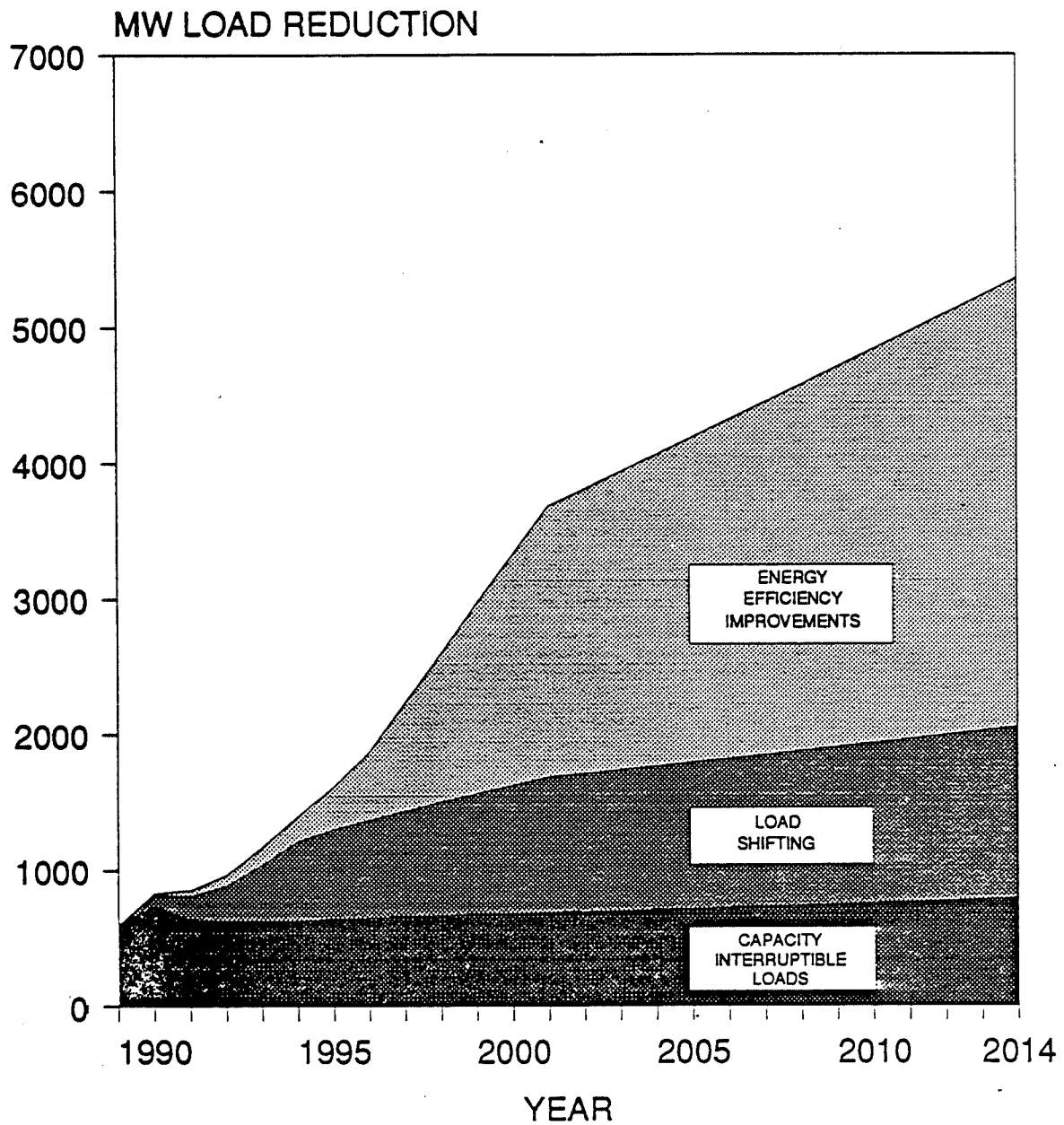


FIGURE 4.7-4
DEMAND MANAGEMENT DATA
USED FOR ANALYSIS
BRANCH UPPER LOAD FORECAST

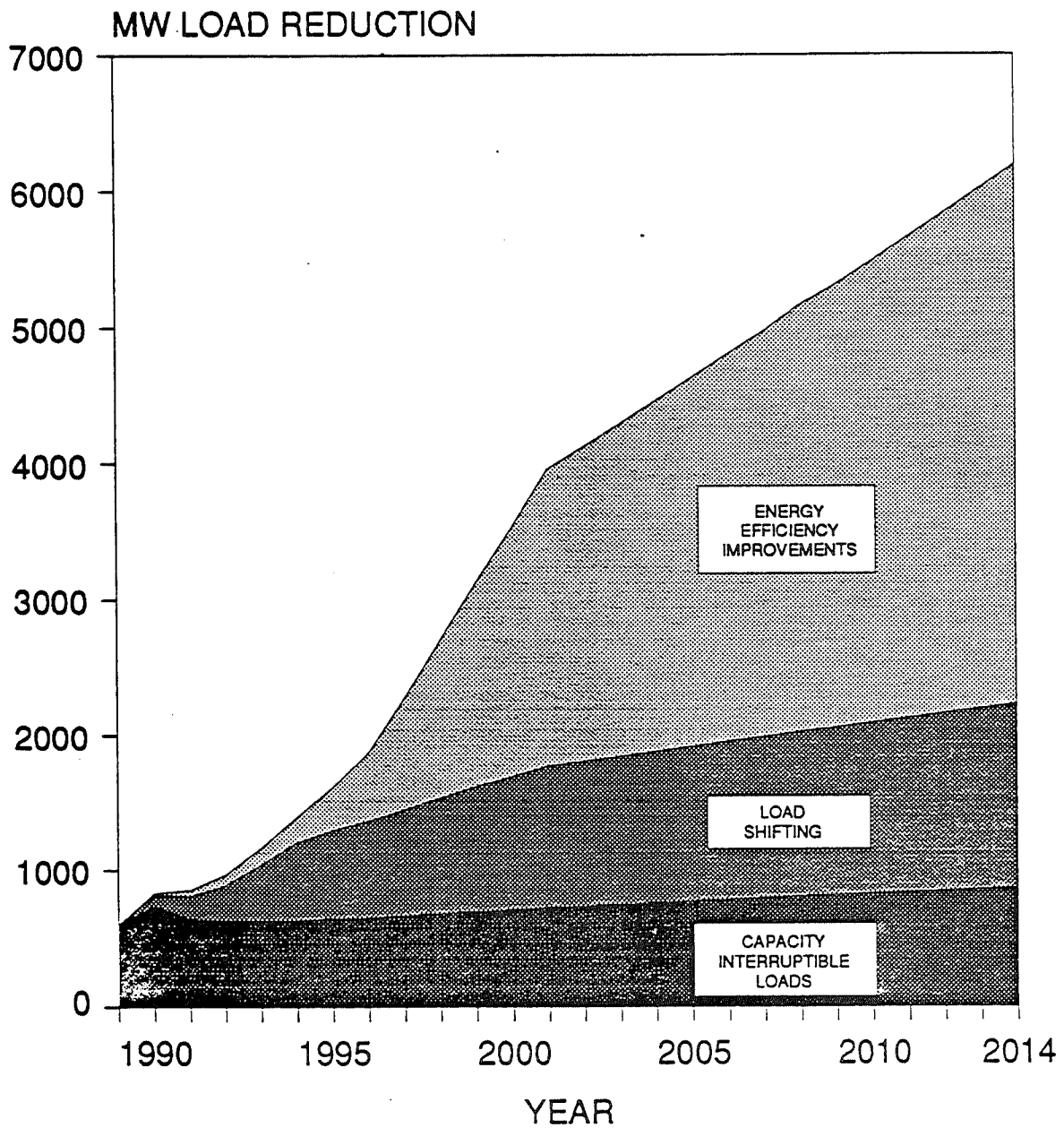


FIGURE 4.7-5
DEMAND MANAGEMENT DATA
USED FOR ANALYSIS
UPPER LOAD FORECAST

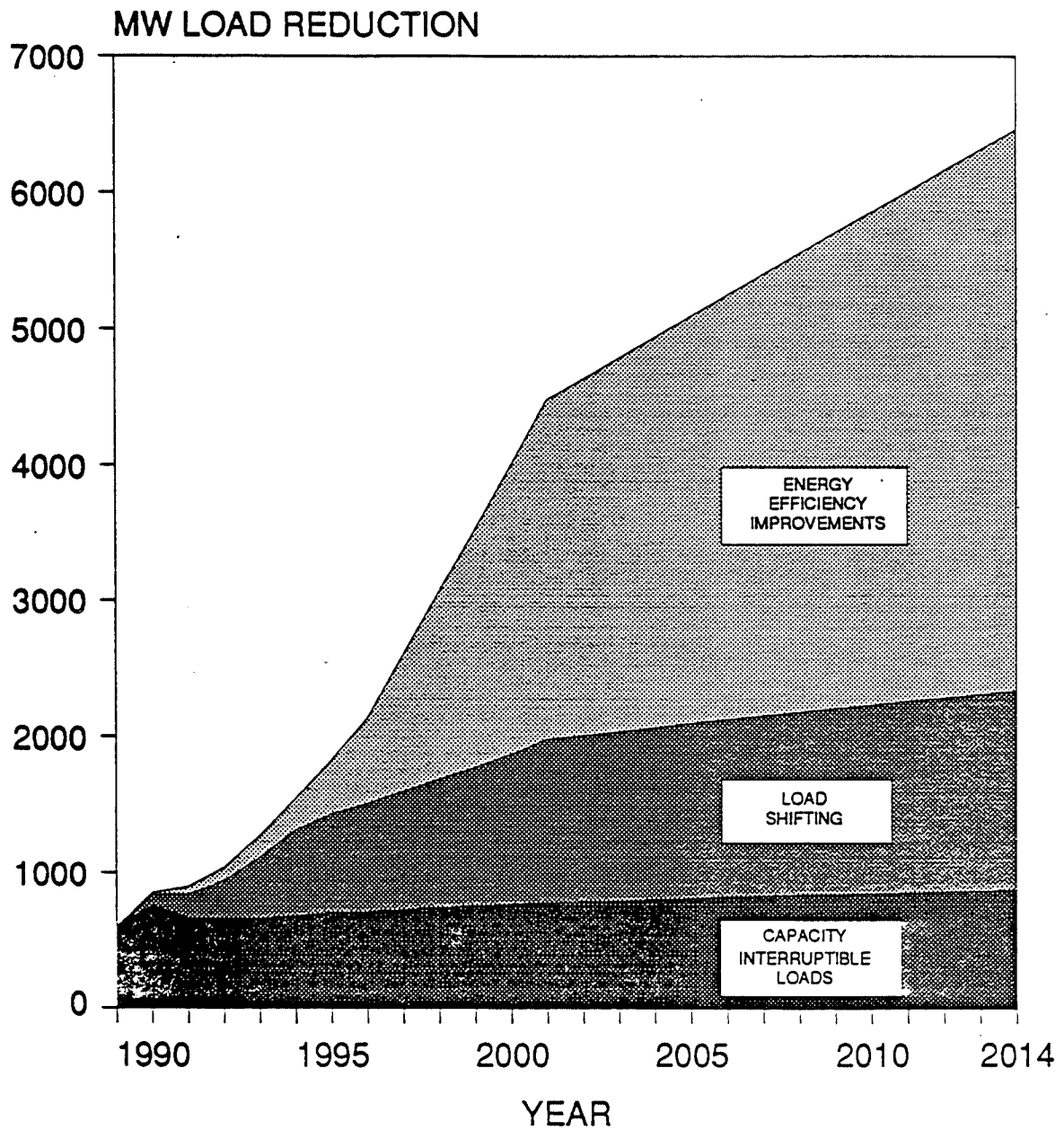


FIGURE 4.7-6
DEMAND MANAGEMENT DATA USED IN PLAN FORMULATION
(CUMULATIVE VALUES AS OF JANUARY OF THE YEAR)

YEAR	LOWER LOAD FORECAST				BRANCH LOWER LOAD FORECAST				MEDIAN LOAD FORECAST				BRANCH UPPER LOAD FORECAST				UPPER LOAD FORECAST			
	EEI (MW)	LS (MW)	CIL (MW)	TOTAL (MW)	EEI (MW)	LS (MW)	CIL (MW)	TOTAL (MW)	EEI (MW)	LS (MW)	CIL (MW)	TOTAL (MW)	EEI (MW)	LS (MW)	CIL (MW)	TOTAL (MW)	EEI (MW)	LS (MW)	CIL (MW)	TOTAL (MW)
1989	0	0	594	594	0	0	594	594	0	0	594	594	0	0	594	594	0	0	594	594
1990	14	77	709	800	14	80	735	829	14	80	735	829	14	80	735	829	14	83	758	855
1991	34	159	606	799	45	169	639	853	45	169	639	853	45	169	639	853	56	177	665	898
1992	59	244	585	888	78	263	626	967	78	263	626	967	78	263	626	967	98	279	662	1039
1993	95	384	570	1049	126	421	621	1168	126	421	621	1168	126	421	621	1168	158	452	664	1274
1994	137	517	566	1220	183	580	630	1393	183	580	630	1393	183	580	630	1393	229	634	684	1547
1995	236	575	570	1381	314	655	643	1612	314	655	643	1612	314	655	643	1612	393	726	708	1827
1996	375	619	568	1562	500	715	650	1865	500	715	650	1865	500	715	650	1865	625	793	716	2134
1997	600	662	566	1828	779	763	647	2189	800	775	656	2231	822	785	664	2271	1000	869	730	2599
1998	825	707	566	2098	1051	812	646	2509	1100	835	664	2599	1154	857	680	2691	1375	945	745	3065
1999	1050	748	568	2366	1315	857	646	2818	1400	892	671	2963	1495	926	695	3116	1750	1017	760	3527
2000	1275	789	569	2633	1574	899	645	3118	1700	946	677	3323	1831	989	706	3526	2125	1100	770	3995
2001	1500	800	574	2874	1809	950	641	3400	2000	1000	685	3685	2185	1050	721	3956	2500	1200	780	4480
2002	1575	820	578	2973	1882	965	642	3489	2100	1020	690	3810	2315	1074	732	4121	2625	1220	787	4632
2003	1650	840	582	3072	1956	980	644	3580	2200	1040	697	3937	2447	1098	744	4289	2750	1240	797	4787
2004	1725	860	586	3171	2028	995	646	3669	2300	1060	704	4064	2580	1122	756	4458	2875	1260	806	4941
2005	1800	880	589	3269	2102	1010	649	3761	2400	1080	712	4192	2714	1146	769	4629	3000	1280	817	5097
2006	1875	900	594	3369	2177	1025	652	3854	2500	1100	719	4319	2850	1170	782	4802	3125	1300	826	5251
2007	1950	920	600	3470	2253	1040	658	3951	2600	1120	727	4447	2980	1194	792	4966	3250	1320	834	5404
2008	2025	940	608	3573	2328	1055	664	4047	2700	1140	735	4575	3134	1218	806	5158	3375	1340	841	5556
2009	2100	960	617	3677	2403	1070	670	4143	2800	1160	744	4704	3252	1242	813	5307	3500	1360	847	5707
2010	2175	980	627	3782	2476	1085	677	4238	2900	1180	752	4832	3390	1266	823	5479	3625	1380	852	5857
2011	2250	1000	638	3888	2548	1100	686	4334	3000	1200	761	4961	3532	1290	833	5655	3750	1400	858	6008
2012	2325	1020	647	3992	2619	1115	693	4427	3100	1220	771	5091	3674	1314	843	5831	3875	1420	864	6159
2013	2400	1040	656	4096	2688	1130	700	4518	3200	1240	780	5220	3819	1338	854	6011	4000	1440	871	6311
2014	2475	1060	666	4201	2755	1145	707	4607	3300	1260	790	5350	3965	1362	864	6191	4125	1460	877	6462

The Demand Management forecasts presented in Figure 4.7-6 (in terms of peak power reduction) for Upper, Median, and Lower load paths are slightly lower than those reported in the Plan Report. This is because the Demand Management program is reviewed constantly and, if appropriate, modified to reflect changing expectations about attainable load reduction targets. The Demand Management Plan appearing in the Plan Report is the latest available Demand Management forecast (as of the Plan issue date). As stated in the Plan Report, these targets are not regarded by Ontario Hydro as ceilings:- if it is possible to exceed them, Hydro will do so.

Figure 4.7-7 compares the Demand Management Plan for the Median load forecast case as specified in the Plan Report with demand management projections used during the demand/supply case formulation process. Figures 4.7-8 and 4.7-9 provide a similar comparison for data pertaining to the Upper and Lower load forecast paths.

The Energy Efficiency Improvement forecasts used for demand/supply case formulation under Median and Upper load forecasts conditions differ from those reported in the Plan Report by less than 3 MW in any year, taken on a cumulative basis. For all practical purposes, these forecasts are in total agreement. Under Lower load forecast conditions, the EEI forecast used for demand/supply case formulation was less than that reported in the Plan Report by amounts growing to about 100 MW by 2001. Note, however, that by the time major supply options were determined to be needed in the Proposed Plan Lower forecast case (2009), the disagreement between the case formulation and the Plan Report EEI forecasts was nil. Therefore, the "need date" for new major supply options in the Proposed Demand/Supply Plan would not have changed even if demand/supply case formulation had proceeded based on the more recent EEI forecast.

In fact, case formulation was based on a forecast of EEI after 2009 which was slightly **more** optimistic than the forecast presented in the Plan Report. Theoretically, incorporation of the new, Plan Report EEI forecast into the Lower load forecast cases might result in post-2009 capacity additions being slightly advanced compared to the Proposed Plan. In practice, though, this would not occur. By the end of the study period, the difference between the forecasts is at most 63 MW, or only about 2.5 percent of the currently planned EEI contribution.

Differences between the forecast of load shifting presented in the Plan Report and the forecast used for demand/supply case formulation are no more than about 3 MW. Note that Figure 7-22 of the Plan Report contains a typographical error. The load reduction expected from load shifting in 1994 for the Upper load forecast case should have read 634 MW, not 735 MW.

The most notable differences between the Upper, Median, and Lower demand management forecasts which were used for demand/supply case formulation and

FIGURE 4.7-7
COMPARISON OF DEMAND MANAGEMENT DATA USED IN
PLAN ANALYSIS AND SHOWN IN THE PLAN REPORT
(VALUES AS OF JANUARY OF THE YEAR)

MEDIAN LOAD FORECAST

YEAR	EEI			LS			CIL			TOTAL		
	PLAN REPORT	ANALYSIS	DIFFER- ENCE	PLAN REPORT	ANALYSIS	DIFFER- ENCE	PLAN REPORT	ANALYSIS	DIFFER- ENCE	PLAN REPORT	ANALYSIS	DIFFER- ENCE
1990	14	14	0	81	80	-1	735	735	0	830	829	-1
1991	45	45	0	171	169	-2	632	639	7	848	853	5
1992	78	78	0	266	263	-3	625	626	1	969	967	-2
1993	126	126	0	423	421	-2	621	621	0	1170	1168	-2
1994	183	183	0	582	580	-2	623	630	7	1388	1393	5
1995	314	314	0	656	655	-1	632	643	11	1602	1612	10
1996	500	500	0	717	715	-2	641	650	9	1858	1865	7
1997	800	800	0	776	775	-1	652	656	4	2228	2231	3
1998	1100	1100	0	836	835	-1	664	664	0	2600	2599	-1
1999	1400	1400	0	893	892	-1	676	671	-5	2969	2963	-6
2000	1700	1700	0	946	946	0	688	677	-11	3334	3323	-11
2001	2000	2000	0	1000	1000	0	702	685	-17	3702	3685	-17
2002	2100	2100	0	1020	1020	0	712	690	-22	3832	3810	-22
2003	2200	2200	0	1040	1040	0	724	697	-27	3964	3937	-27
2004	2300	2300	0	1060	1060	0	737	704	-33	4097	4064	-33
2005	2400	2400	0	1080	1080	0	749	712	-37	4229	4192	-37
2006	2500	2500	0	1100	1100	0	762	719	-43	4362	4319	-43
2007	2600	2600	0	1120	1120	0	775	727	-48	4495	4447	-48
2008	2700	2700	0	1140	1140	0	788	735	-53	4628	4575	-53
2009	2800	2800	0	1160	1160	0	802	744	-58	4762	4704	-58
2010	2899	2900	1	1180	1180	0	816	752	-64	4895	4832	-63
2011	3000	3000	0	1200	1200	0	830	761	-69	5030	4961	-69
2012	3101	3100	-1	1220	1220	0	844	771	-73	5165	5091	-74
2013	3200	3200	0	1240	1240	0	859	780	-79	5299	5220	-79
2014	3298	3300	2	1260	1260	0	874	790	-84	5432	5350	-82

FIGURE 4.7-8
COMPARISON OF DEMAND MANAGEMENT DATA USED IN
PLAN ANALYSIS AND SHOWN IN THE PLAN REPORT
(VALUES AS OF JANUARY OF THE YEAR)

UPPER LOAD FORECAST

YEAR	EEI			LS			CIL			TOTAL		
	PLAN REPORT	ANALYSIS	DIFFER- ENCE	PLAN REPORT	ANALYSIS	DIFFER- ENCE	PLAN REPORT	ANALYSIS	DIFFER- ENCE	PLAN REPORT	ANALYSIS	DIFFER- ENCE
1990	14	14	0	84	83	-1	758	758	0	856	855	-1
1991	56	56	0	180	177	-3	658	665	7	894	898	4
1992	98	98	0	282	279	-3	660	662	2	1040	1039	-1
1993	158	158	0	455	452	-3	660	664	4	1273	1274	1
1994	229	229	0	634	634	0	672	684	12	1535	1547	12
1995	393	393	0	728	726	-2	696	708	12	1817	1827	10
1996	625	625	0	795	793	-2	705	716	11	2125	2134	9
1997	1000	1000	0	870	869	-1	724	730	6	2594	2599	5
1998	1375	1375	0	946	945	-1	744	745	1	3065	3065	0
1999	1749	1750	1	1017	1017	0	765	760	-5	3531	3527	-4
2000	2125	2125	0	1100	1100	0	782	770	-12	4007	3995	-12
2001	2500	2500	0	1200	1200	0	798	780	-18	4498	4480	-18
2002	2624	2625	1	1220	1220	0	811	787	-24	4655	4632	-23
2003	2750	2750	0	1240	1240	0	826	797	-29	4816	4787	-29
2004	2875	2875	0	1260	1260	0	841	806	-35	4976	4941	-35
2005	3000	3000	0	1280	1280	0	857	817	-40	5137	5097	-40
2006	3125	3125	0	1300	1300	0	871	826	-45	5296	5251	-45
2007	3250	3250	0	1320	1320	0	884	834	-50	5454	5404	-50
2008	3375	3375	0	1340	1340	0	896	841	-55	5611	5556	-55
2009	3500	3500	0	1360	1360	0	907	847	-60	5767	5707	-60
2010	3625	3625	0	1380	1380	0	917	852	-65	5922	5857	-65
2011	3750	3750	0	1400	1400	0	928	858	-70	6078	6008	-70
2012	3875	3875	0	1420	1420	0	940	864	-76	6235	6159	-76
2013	4000	4000	0	1440	1440	0	951	871	-80	6391	6311	-80
2014	4123	4125	2	1460	1460	0	963	877	-86	6546	6462	-84

FIGURE 4.7.4
COMPARISON OF DEMAND MANAGEMENT DATA USED IN
PLAN ANALYSIS AND SHOWN IN THE PLAN REPORT
(VALUES AS OF JANUARY OF THE YEAR)

LOWER LOAD FORECAST												
YEAR	EEI			LS			CIL			TOTAL		
	PLAN REPORT	ANALYSIS	DIFFER- ENCE	PLAN REPORT	ANALYSIS	DIFFER- ENCE	PLAN REPORT	ANALYSIS	DIFFER- ENCE	PLAN REPORT	ANALYSIS	DIFFER- ENCE
1990	14	14	0	78	77	-1	709	709	0	801	800	-1
1991	36	34	-2	161	159	-2	590	606	7	796	799	3
1992	62	59	-3	246	244	-2	593	595	2	891	898	7
1993	101	95	-6	387	384	-3	566	570	4	1054	1049	-5
1994	146	137	-9	519	517	-2	554	566	12	1219	1220	1
1995	251	236	-15	576	575	-1	558	570	12	1385	1381	-4
1996	400	375	-25	620	619	-1	561	568	7	1561	1562	1
1997	646	600	-46	683	682	-1	566	566	0	1869	1828	-41
1998	890	825	-65	707	707	0	573	566	-7	2160	2098	-62
1999	1120	1050	-70	748	748	0	580	568	-12	2440	2365	-75
2000	1360	1275	-85	790	789	-1	587	569	-18	2737	2633	-104
2001	1600	1500	-100	800	800	0	599	574	-25	2999	2874	-125
2002	1683	1575	-108	820	820	0	607	578	-29	3090	2973	-117
2003	1725	1650	-75	840	840	0	616	582	-34	3161	3072	-89
2004	1788	1725	-63	860	860	0	625	586	-39	3273	3171	-102
2005	1850	1800	-50	880	880	0	633	589	-44	3363	3269	-94
2006	1913	1875	-38	900	900	0	643	594	-49	3456	3369	-87
2007	1974	1950	-24	920	920	0	655	600	-55	3549	3470	-79
2008	2038	2025	-13	940	940	0	668	608	-60	3646	3573	-73
2009	2100	2100	0	960	960	0	682	617	-65	3742	3677	-65
2010	2163	2175	12	980	980	0	697	627	-70	3840	3782	-58
2011	2225	2250	25	1000	1000	0	713	638	-75	3938	3886	-52
2012	2288	2325	37	1020	1020	0	727	647	-80	4035	3992	-43
2013	2350	2400	50	1041	1040	-1	742	656	-86	4133	4086	-47
2014	2412	2475	63	1060	1060	0	756	666	-90	4228	4201	-27

those presented in the Plan Report occur for capacity interruptible loads. Even so, these differences are relatively small. They are less than 3% of the current CIL forecast until the early 2000s. They grow throughout the remainder of the planning period, reaching a maximum of about 90 MW by 2014 (ie. Plan Report values exceed those used during demand/supply case formulation by up to about 90 MW).

Even for the Lower load forecast path, the basic demand between now and 2014 is forecast to grow by as much as 10.8 GW. The total of all of the differences between the two demand management forecasts identified above is small when compared to this forecast load growth. Moreover, the difference between the old and new demand management projections also represents a very small percentage of the load forecast bandwidth for which plans are designed:- a bandwidth which itself covers only about 80% of the load growth uncertainty judged to be possible. For these reasons, differences in Demand Management projections of the magnitude reported above would have no discernable influence on the validity of the cases.

4.8 NON-UTILITY GENERATION PLAN

Chapter 8 of the Plan Report discusses the difference between load-displacement non-utility generation and purchase non-utility generation. It also presents Figures 8-6 and 8-7, which tabulate the levels of each type of non-utility generation which are currently planned under Median load forecast conditions.

In order to facilitate timely demand/supply case formulation and analysis, it was necessary early in 1989 to obtain preliminary estimates of achievable levels of demand displacement and purchase non-utility generation. Early phases of the analysis were undertaken using these preliminary estimates.

As discussed in Section 4.2 above, the non-utility generation estimates used in the analysis were revised in August 1989. Cases formulated and analyzed after that time were all based on the non-utility generation forecasts shown in Figures 4.8-1 and 4.8-2 below. These figures present non-utility generation contributions in terms of both peak power and energy. The energy contributions from non-utility generation shown in these figures were calculated assuming an average annual capacity factor of 80%, as stated in the Plan Report text. Figure 4.8-3 shows the cumulative net induced demand displacement (in terms of MW peak power reduction) as a function of time. This figure is analogous to the bottom half of Figure 8-8 of the Plan Report. Figure 4.8-4, analogous to the top half of Figure 8-8 of the Plan Report, displays the net purchase non-utility generation contribution over time.

FIGURE 4.8-1
CUMULATIVE NET INDUCED DEMAND DISPLACEMENT NON-UTILITY GENERATION
DATA USED FOR ANALYSIS
(VALUES AS OF JANUARY OF THE YEAR)

YEAR	LOWER		BRANCH- LOWER		MEDIAN		BRANCH UPPER		UPPER	
	LOAD REDUCTION (MW)	ENERGY (TWh)	LOAD REDUCTION (MW)	ENERGY (TWh)	LOAD REDUCTION (MW)	ENERGY (TWh)	LOAD REDUCTION (MW)	ENERGY (TWh)	LOAD REDUCTION (MW)	ENERGY (TWh)
1990	23	0.16	23	0.16	23	0.16	23	0.16	23	0.16
1991	90	0.63	90	0.63	90	0.63	90	0.63	90	0.63
1992	144	1.01	144	1.01	144	1.01	144	1.01	144	1.01
1993	210	1.47	210	1.47	210	1.47	210	1.47	210	1.47
1994	275	1.91	275	1.93	275	1.93	275	1.93	276	1.93
1995	288	2.02	300	2.10	300	2.10	300	2.10	307	2.15
1996	288	2.02	325	2.28	325	2.28	325	2.28	342	2.40
1997	288	2.02	340	2.38	340	2.38	340	2.38	362	2.54
1998	288	2.02	354	2.48	354	2.48	354	2.48	369	2.59
1999	288	2.02	364	2.55	364	2.55	364	2.55	362	2.54
2000	288	2.02	368	2.58	368	2.58	368	2.58	355	2.49
2001	288	2.02	340	2.38	368	2.58	348	2.44	348	2.44
2002	288	2.02	320	2.24	361	2.53	341	2.39	341	2.39
2003	288	2.02	300	2.10	354	2.48	334	2.34	334	2.34
2004	281	1.97	281	1.97	347	2.43	327	2.29	327	2.29
2005	274	1.92	274	1.92	339	2.38	320	2.24	320	2.24
2006	267	1.87	267	1.87	332	2.33	313	2.19	313	2.19
2007	260	1.82	260	1.82	325	2.28	306	2.15	306	2.15
2008	253	1.77	253	1.77	318	2.23	299	2.10	299	2.10
2009	246	1.72	246	1.72	311	2.18	292	2.05	292	2.05
2010	239	1.68	239	1.68	303	2.12	285	2.00	285	2.00
2011	232	1.63	232	1.63	296	2.07	278	1.95	278	1.95
2012	225	1.58	225	1.58	289	2.03	271	1.90	271	1.90
2013	218	1.53	218	1.53	282	1.98	264	1.85	264	1.85
2014	211	1.48	211	1.48	275	1.93	257	1.76	257	1.76

NOTE: A capacity factor of 80% is assumed to calculate annual energy.

FIGURE 4.8-2
CUMULATIVE NET PURCHASE NON-UTILITY GENERATION
DATA USED FOR ANALYSIS
(VALUES AS OF JANUARY OF THE YEAR)

YEAR	LOWER		BRANCH LOWER		MEDIAN		BRANCH UPPER		UPPER	
	CAPACITY (MW)	ENERGY (TWh)	CAPACITY (MW)	ENERGY (TWh)	CAPACITY (MW)	ENERGY (TWh)	CAPACITY (MW)	ENERGY (TWh)	CAPACITY (MW)	ENERGY (TWh)
1989	26	0.18	26	0.18	26	0.18	26	0.18	26	0.18
1990	54	0.38	54	0.38	54	0.38	54	0.38	54	0.38
1991	81	0.57	81	0.57	81	0.57	81	0.57	81	0.57
1992	252	1.77	252	1.77	252	1.77	252	1.77	252	1.77
1993	338	2.37	338	2.37	338	2.37	338	2.37	338	2.37
1994	424	2.97	424	2.97	424	2.97	424	2.97	424	2.97
1995	461	3.23	497	3.48	497	3.48	497	3.48	535	3.75
1996	461	3.23	570	3.99	570	3.99	570	3.99	688	4.82
1997	461	3.23	642	4.50	642	4.50	642	4.50	846	5.93
1998	461	3.23	717	5.02	717	5.02	717	5.02	975	6.83
1999	461	3.23	797	5.59	797	5.59	797	5.59	1036	7.26
2000	461	3.23	883	6.19	883	6.19	883	6.19	1097	7.69
2001	461	3.23	883	6.19	974	6.83	993	6.96	1157	8.11
2002	461	3.23	883	6.19	1035	7.25	1113	7.80	1218	8.54
2003	461	3.23	883	6.19	1096	7.68	1223	8.57	1279	8.96
2004	521	3.65	883	6.19	1156	8.10	1313	9.20	1339	9.38
2005	581	4.07	883	6.19	1216	8.52	1399	9.80	1399	9.80
2006	641	4.49	883	6.19	1276	8.94	1459	10.22	1459	10.22
2007	701	4.91	883	6.19	1336	9.36	1519	10.65	1519	10.65
2008	760	5.33	883	6.19	1395	9.78	1578	11.06	1578	11.06
2009	819	5.74	883	6.19	1454	10.19	1637	11.47	1637	11.47
2010	850	5.96	914	6.41	1485	10.41	1668	11.69	1668	11.69
2011	881	6.17	945	6.62	1516	10.62	1699	11.91	1699	11.91
2012	912	6.39	976	6.84	1547	10.84	1730	12.12	1730	12.12
2013	943	6.61	1007	7.06	1578	11.06	1761	12.34	1761	12.34
2014	974	6.83	1038	7.27	1609	11.28	1792	12.56	1792	12.56

NOTE: A capacity factor of 80% is assumed to calculate annual energy.

FIGURE 4.8-3
NUG DATA USED FOR ANALYSIS
NET INDUCED DEMAND DISPLACEMENT

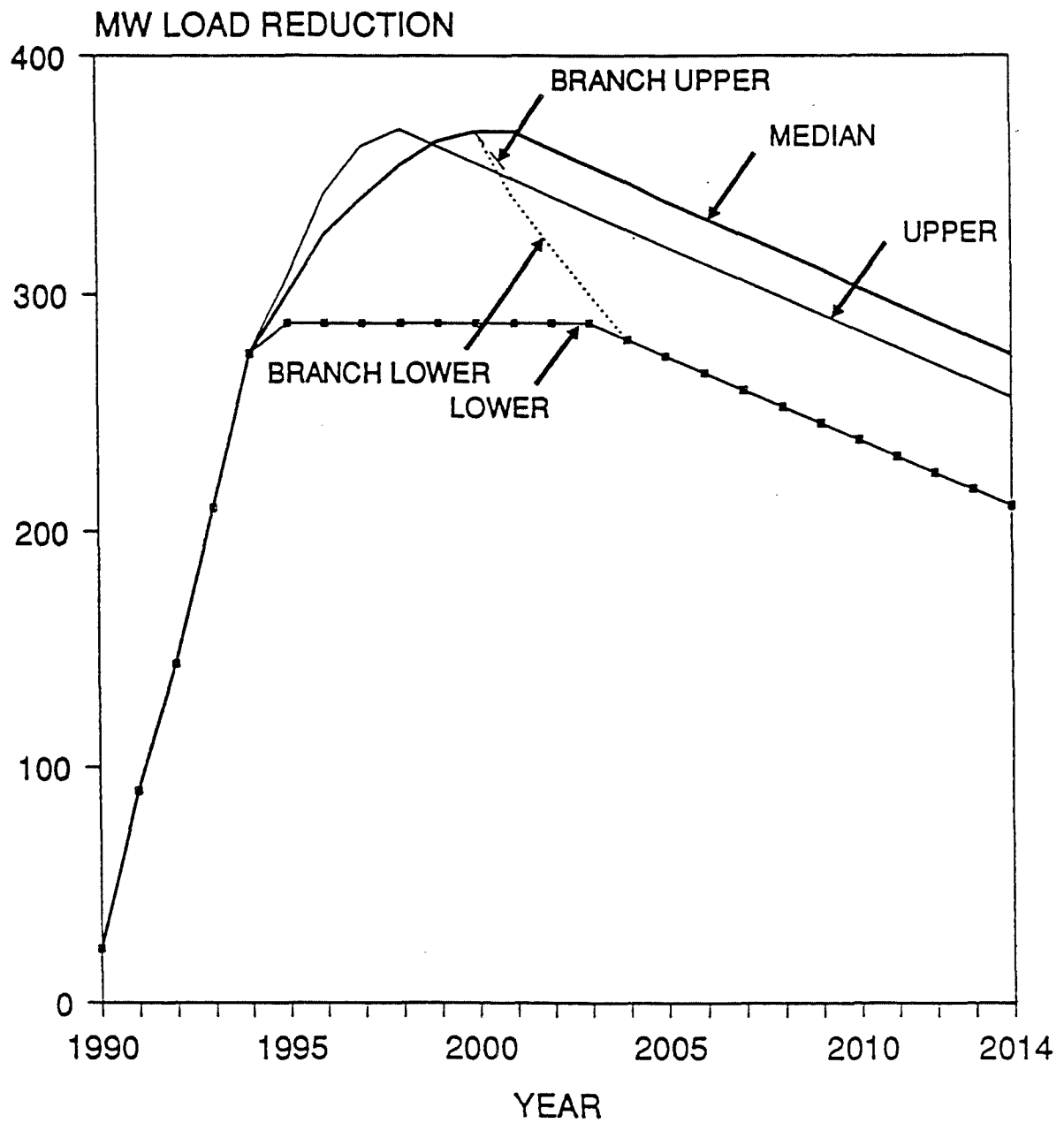
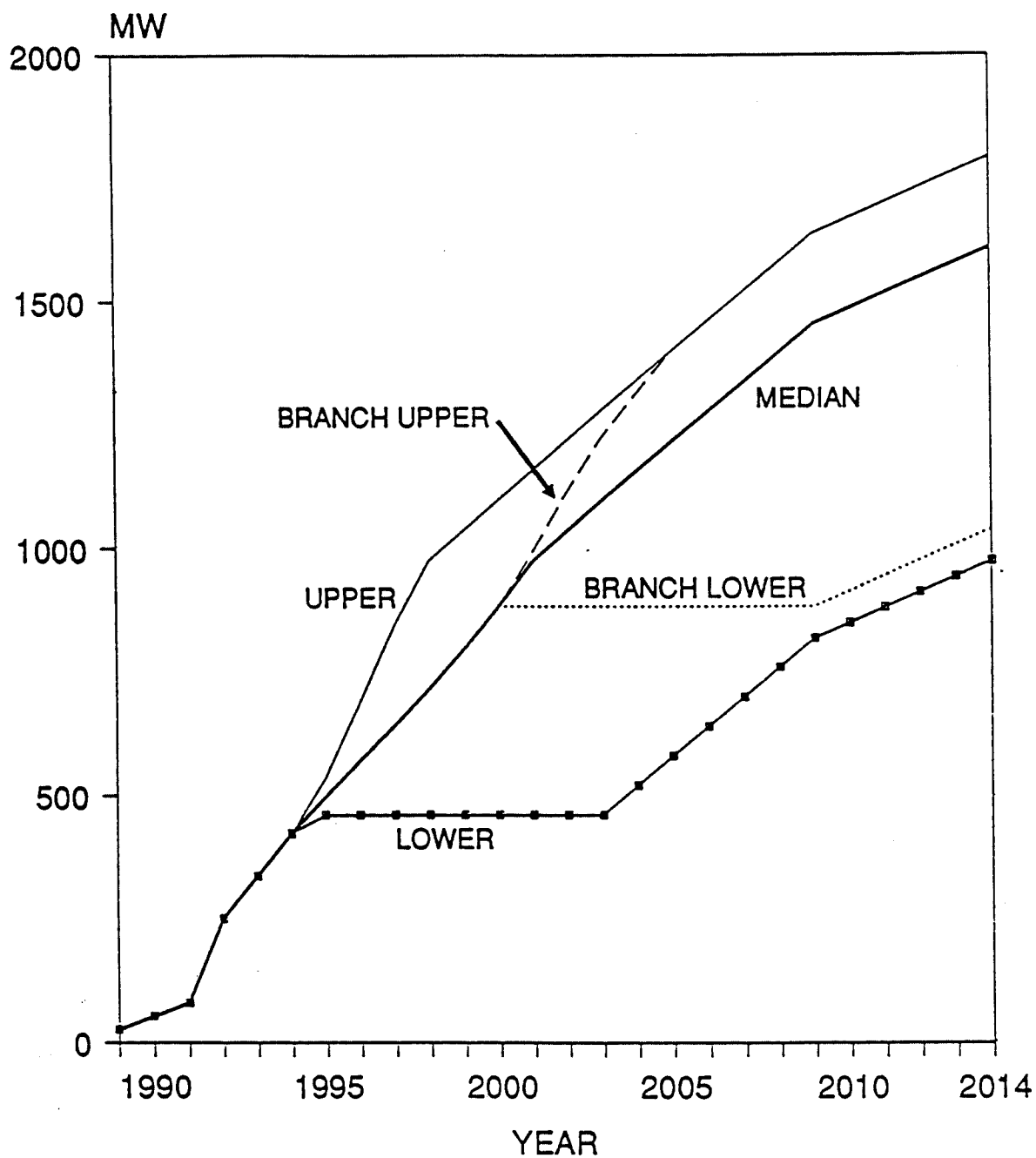


FIGURE 4.8-4
CUMULATIVE NET PURCHASE NUG CAPACITY
USED IN ANALYSIS



The current Non-utility Generation Plan (as listed in Figure 8-6 and 8-7 of the Plan Report) differs from that developed in the summer of 1989 and used for the final round of demand/supply case formulation and analysis. Figure 4.8-5 compares the two projections. The differences between the two projections for any given year are small compared to the width of the bandwidth forecast in that year. Any differences are not large enough to significantly affect the relative merits of the demand/supply cases.

4.9 PRIMARY AND FIRM LOAD FORECASTS

Figure 9-3 of the Plan Report presents the year-by-year forecast of the 20-minute January primary peak power demand for the Upper, Median, and Lower load paths. This primary forecast was based on the basic load forecast of December 1988, from which the power contributions of the Demand Management and Non-utility Generation Plans (as of September 1989) were subtracted. As noted previously the Demand Management and NUG contributions analyzed were based on forecasts available earlier in 1989, and are not in exact agreement with those current in the Fall of 1989. Hence, the Primary load forecast which was used in analysis is not exactly the same as that presented in the Plan Report.

Figure 4.9-1 provides the year-by-year values of the 20-minute January peak power demand used in the analysis under the five load forecast conditions. These values are not greatly different than those reported in Figure 9-3 of the Plan Report. The greatest difference is about 0.2 GW for the Lower and Median load forecast cases and 0.3 GW for the Upper. The average difference between forecasts is much less than this. Differences in primary load forecasts of this magnitude are not significant, particularly in light of the range of load growth uncertainty embodied in the bandwidth forecast.

Figure 4.9-2 presents the five primary load forecasts used during demand/supply case formulation and analyses.

Figure 4.9-3 tabulates the 20-minute January peak firm load forecast used in the final round of demand/supply case analysis for each of the five load forecast conditions. This Figure is analogous to Figure 9-8 of the Plan Report. Each of the five firm load forecasts was obtained by subtracting the Capacity Interruptible Load forecasts discussed in Section 4.7 from the primary forecasts of Figure 4.9-2. The five firm load forecasts are shown in Figure 4.9-4.

FIGURE 4.8-5

COMPARISON OF NON-UTILITY GENERATION DATA USED
IN THE MAIN PLAN REPORT AND IN PLAN FORMULATION

MEDIAN LOAD FORECAST

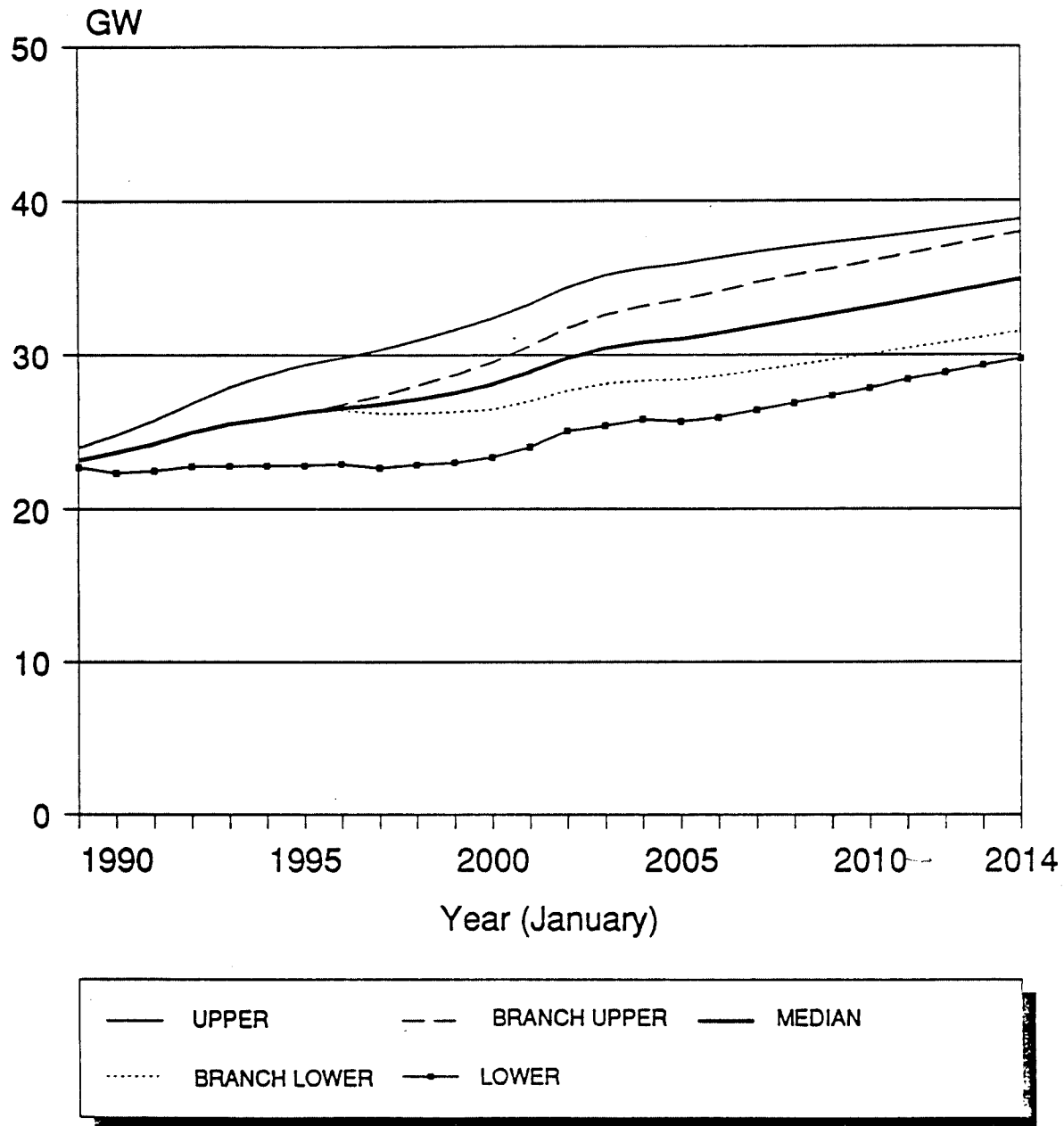
YEAR	CUMULATIVE DEMAND DISPLACEMENT NUG (January of Year)			CUMULATIVE PURCHASE NUG (January of Year)		
	PLAN REPORT	PLAN FORMULATION	DIFFERENCE	PLAN REPORT	PLAN FORMULATION	DIFFERENCE
1989	0	0	0	0	0	0
1990	59	23	-36	28	26	-2
1991	102	90	-12	55	54	-1
1992	176	144	-32	226	81	-145
1993	243	210	-33	312	252	-60
1994	310	275	-35	398	338	-60
1995	334	300	-34	471	424	-47
1996	359	325	-34	544	497	-47
1997	373	340	-33	616	570	-46
1998	384	354	-30	691	642	-49
1999	391	364	-27	771	717	-54
2000	392	368	-24	857	797	-60
2001	403	368	-35	932	883	-49
2002	407	361	-46	981	974	-7
2003	411	354	-57	1030	1035	5
2004	414	347	-67	1078	1096	18
2005	418	339	-79	1126	1156	30
2006	422	332	-90	1174	1216	42
2007	426	325	-101	1222	1276	54
2008	429	318	-111	1269	1336	67
2009	433	311	-122	1316	1395	79
2010	437	303	-134	1360	1454	94
2011	441	296	-145	1403	1485	82
2012	445	289	-156	1439	1516	77
2013	448	282	-166	1470	1547	77
2014	452	275	-177	1497	1578	81

**Figure 4.9-1: PRIMARY LOAD FORECAST USED FOR ANALYSIS -
JANUARY 20 MINUTE PEAK POWER
DEMAND (GW)**

Year	Lower	Branch Lower	Median	Branch Upper	Upper
1989	22.7	23.2	23.2 *	23.2	24.0
1990	22.3	23.7	23.7	23.7	24.8
1991	22.5	24.2	24.2	24.2	25.7
1992	22.8	25.0	25.0	25.0	26.8
1993	22.8	25.5	25.5	25.5	27.9
1994	22.8	25.8	25.8	25.8	28.7
1995	22.8	26.3	26.3	26.3	29.3
1996	22.9	26.4	26.6	26.8	29.8
1997	22.7	26.2	26.8	27.3	30.3
1998	22.9	26.2	27.1	28.0	31.0
1999	23.0	26.3	27.5	28.7	31.6
2000	23.4	26.5	28.1	29.5	32.4
2001	24.0	27.0	28.9	30.6	33.3
2002	25.1	27.7	29.8	31.8	34.4
2003	25.4	28.1	30.5	32.6	35.2
2004	25.8	28.3	30.8	33.2	35.7
2005	25.7	28.4	31.1	33.6	36.0
2006	25.9	28.6	31.4	34.2	36.3
2007	26.4	29.0	31.9	34.8	36.7
2008	26.9	29.3	32.3	35.2	37.0
2009	27.4	29.7	32.7	35.6	37.3
2010	27.8	30.1	33.1	36.1	37.6
2011	28.4	30.4	33.6	36.6	37.9
2012	28.8	30.8	34.0	37.0	38.2
2013	29.3	31.2	34.5	37.5	38.5
2014	29.8	31.5	35.0	38.0	38.8

* January 1989 Actual Primary Load was 23.1 GW.

FIGURE 4.9-2
PRIMARY LOAD FORECAST USED FOR ANALYSIS
20-MINUTE JANUARY PEAK POWER DEMAND



**FIGURE 4.9-3: FIRM LOAD FORECAST USED FOR ANALYSIS -
JANUARY 20-MINUTE PEAK POWER
DEMAND (GW)**

Year	Lower	Branch Lower	Median	Branch Upper	Upper
1989	22.1	22.6	22.6	22.6	23.4
1990	21.6	23.0	23.0	23.0	24.0
1991	21.9	23.6	23.6	23.6	25.1
1992	22.2	24.4	24.4	24.4	26.2
1993	22.2	24.9	24.9	24.9	27.2
1994	22.2	25.2	25.2	25.2	28.0
1995	22.3	25.6	25.6	25.6	28.6
1996	22.3	25.8	25.9	26.1	29.1
1997	22.1	25.5	26.1	26.7	29.6
1998	22.3	25.6	26.5	27.3	30.2
1999	22.5	25.7	26.9	28.0	30.9
2000	22.8	25.8	27.4	28.8	31.6
2001	23.4	26.3	28.2	29.9	32.5
2002	24.5	27.0	29.1	31.0	33.6
2003	24.8	27.5	29.8	31.9	34.4
2004	25.2	27.7	30.1	32.5	34.9
2005	25.1	27.7	30.3	32.9	35.1
2006	25.3	28.0	30.7	33.4	35.5
2007	25.8	28.3	31.1	34.0	35.9
2008	26.3	28.6	31.6	34.4	36.2
2009	26.7	29.0	32.0	34.8	36.5
2010	27.2	29.4	32.4	35.3	36.7
2011	27.8	29.7	32.8	35.7	37.0
2012	28.2	30.1	33.3	36.2	37.3
2013	28.6	30.5	33.7	36.7	37.6
2014	29.1	30.8	34.2	37.1	38.0

FIGURE 4.9-4
FIRM LOAD FORECAST USED FOR ANALYSIS
20-MINUTE JANUARY PEAK POWER DEMAND

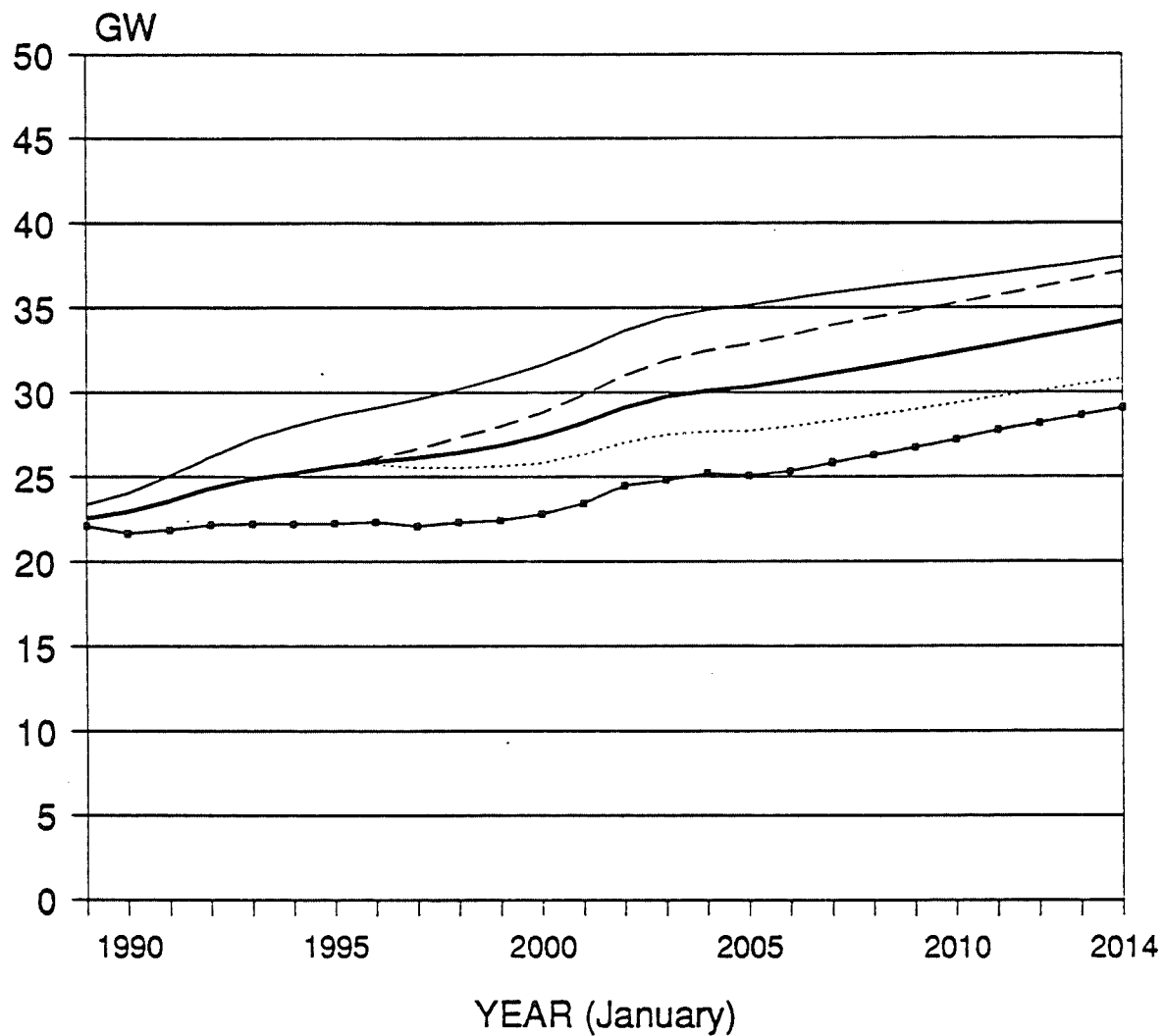


Figure 4.9-5 is a table of average year-over-year growth rates for the basic, primary, and firm forecasts used in the analysis. This figure is analogous to Figure 9-6 of the Plan Report.

4.10 REHABILITATION PLAN

As stated in the Plan Report, the Rehabilitation Plan used during the plan formulation process was common to all demand/supply cases and common to all five load forecasts. The Plan Report presents most of the details of the Rehabilitation Plan which are relevant to demand/supply case formulation. However, since nuclear unit retubing can have a relatively large impact on the total available generating capacity in any given year, it is documented more fully in this section.

The table in Figure 4.10-1 presents the retubing schedule which was used in demand/supply case formulation. This schedule was common to all demand/supply cases and all load forecast paths. Figure 4.10-2 is another representation of this retubing schedule which shows assumed unit outage start times and durations more clearly. Also shown in this figure is the number of megawatts assumed to be unavailable during the January peak due to retubing activity. The effect of this retubing activity has been included in the projected system Load Meeting Capability shown in Figures 4.5-1 and 4.5-2 in this Analysis Report and in Figures 4-14, 4-18, and 5-1 through 5-3 of the Plan Report.

4.11 REQUIREMENT FOR NEW SUPPLY

Plan Report Figures 11-1 through 11-3 present curves showing the derivation of the requirement for new supply under the Upper, Median, and Lower forecast conditions, using corporate forecasts current in September, 1989. Figures 4.11-1 through 4.11-5 below redevelop these curves for all five load forecast paths, using data employed in the fourth phase of demand/supply case formulation and analysis.

From these five curves, the requirement for new supply capacity was determined. This has been plotted for all five load forecast paths in Figure 4.11-6. This Figure is analogous to Figure 11-6 of the Plan Report. Despite the differences between the Demand Management and Non-utility Generation forecasts presented here and in the Plan Report, the calculated requirement for new supply shown in Figure 4.11-6 is in close agreement with that shown in Figure 11-6 of the Plan Report.

FIGURE 4.9-5: AVERAGE YEAR-OVER-YEAR PEAK DEMAND GROWTH RATES
 (FROM DATA USED FOR ANALYSIS)

	<u>Lower Load Forecast</u>			<u>Branch Lower Load Forecast</u>			<u>Median Load Forecast</u>			<u>Branch Upper Load Forecast</u>			<u>Upper Load Forecast</u>		
	Firm	Primary	Basic	Firm	Primary	Basic	Firm	Primary	Basic	Firm	Primary	Basic	Firm	Primary	Basic
1988-1995	0.3%	0.1%	0.8%	2.3%	2.2%	2.8%	2.3%	2.2%	2.8%	2.3%	2.2%	2.8%	3.9%	3.8%	4.5%
1988-2000	0.3%	0.3%	1.1%	1.4%	1.3%	2.2%	1.9%	1.8%	2.7%	2.3%	2.2%	3.1%	3.1%	3.0%	4.0%
1988-2010	1.0%	0.9%	1.5%	1.3%	1.3%	1.9%	1.8%	1.7%	2.3%	2.2%	2.2%	2.7%	2.4%	2.3%	3.0%
1988-2014	1.1%	1.1%	1.5%	1.3%	1.3%	1.8%	1.7%	1.7%	2.2%	2.0%	2.0%	2.6%	2.1%	2.1%	2.7%

**FIGURE 4.10-1: MAJOR PLANNED FUEL CHANNEL
OUTAGES - NUCLEAR STATIONS (1989-2014)**

<u>Unit Name</u>	<u>Unit Capacity</u>	<u>Outage Type *</u>	<u>Outage Start</u>	<u>Outage Duration</u> (months)
Pickering 3	515	LSFCR	June 1989	23
Bruce 3	769	SLAR	February 1990	6
Bruce 4	769	SLAR	July 1990	10
Pickering 4	515	LSFCR	March 1991	19
Bruce 2	769	MAINT	May 1991	3
Pickering 5	516	SLAR	June 1991	5
Bruce 1	769	SLAR	August 1991	10
Pickering 6	516	SLAR	June 1992	5
Bruce 2	769	LSFCR	April 1993	31
Bruce 1	769	LSFCR	March 1997	27
Bruce 3	769	REFAB	July 1998	5
Bruce 3	769	LSFCR	July 2002	24
Pickering 5	516	LSFCR	April 2006	21
Bruce 4	769	LSFCR	July 2007	24
Pickering 6	516	LSFCR	January 2008	21
Bruce 5	860	LSFCR	July 2009	24
Pickering 7	516	LSFCR	October 2009	21
Pickering 8	516	LSFCR	July 2011	21
Bruce 6	860	LSFCR	July 2011	24
Bruce 7	860	LSFCR	July 2013	24

* LSFCR denotes "Large Scale Fuel Channel Replacement"
 SLAR denotes "Spacer Location and Relocation"
 REFAB denotes "Repositioning End-Fitting and Bearings"
 MAINT denotes "Major Maintenance"

FIGURE 4.10-2: MAJOR PLANNED/FUEL CHANNEL OUTAGES
AT NUCLEAR STATIONS (1989-2014)

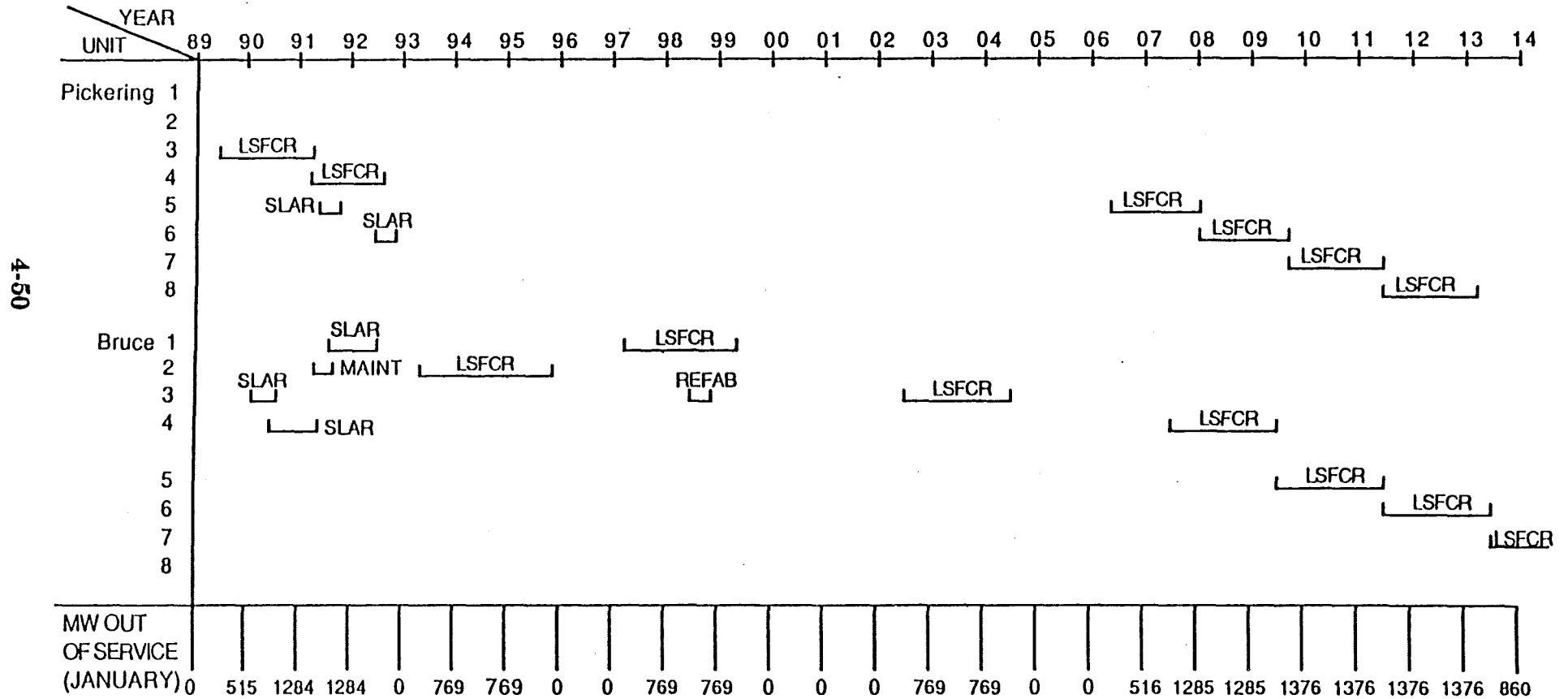


FIGURE 4.11-1
REQUIRED SUPPLY - LMC - PEAK POWER DEMAND
(DATA USED IN ANALYSIS)

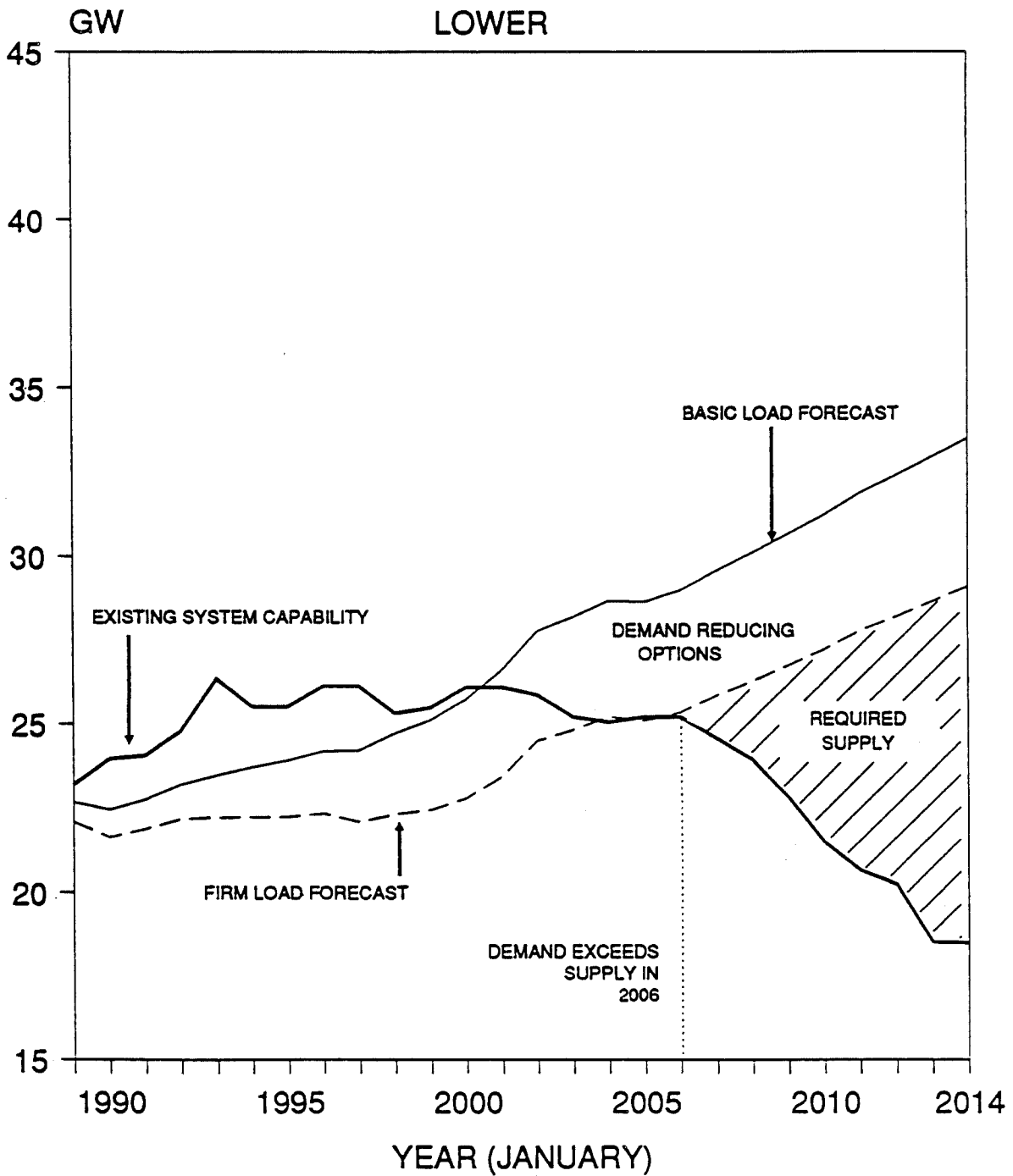


FIGURE 4.11-2

REQUIRED SUPPLY - LMC - PEAK POWER DEMAND
(DATA USED IN ANALYSIS)

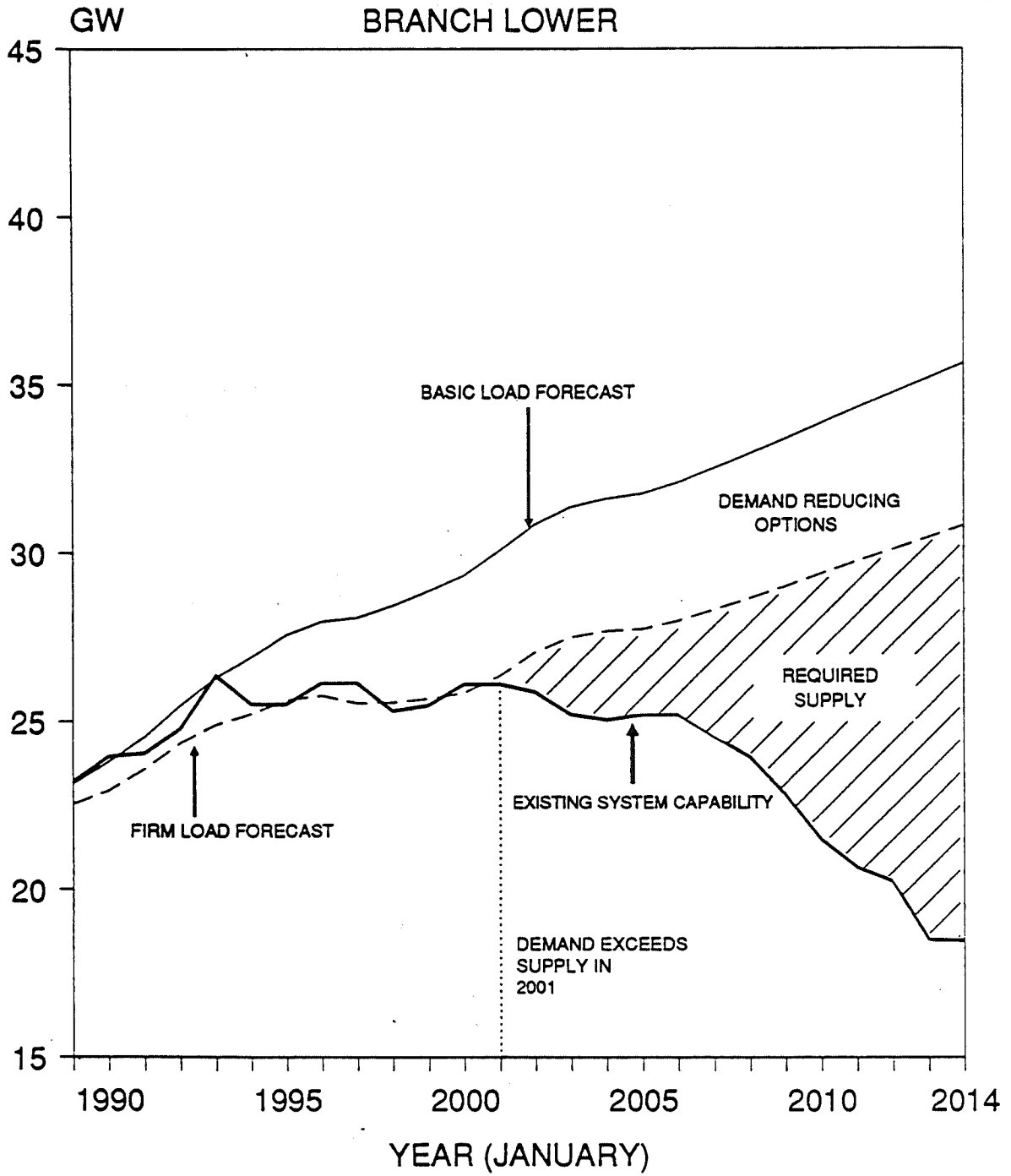


FIGURE 4.11-3
REQUIRED SUPPLY - LMC - PEAK POWER DEMAND
(DATA USED IN ANALYSIS)

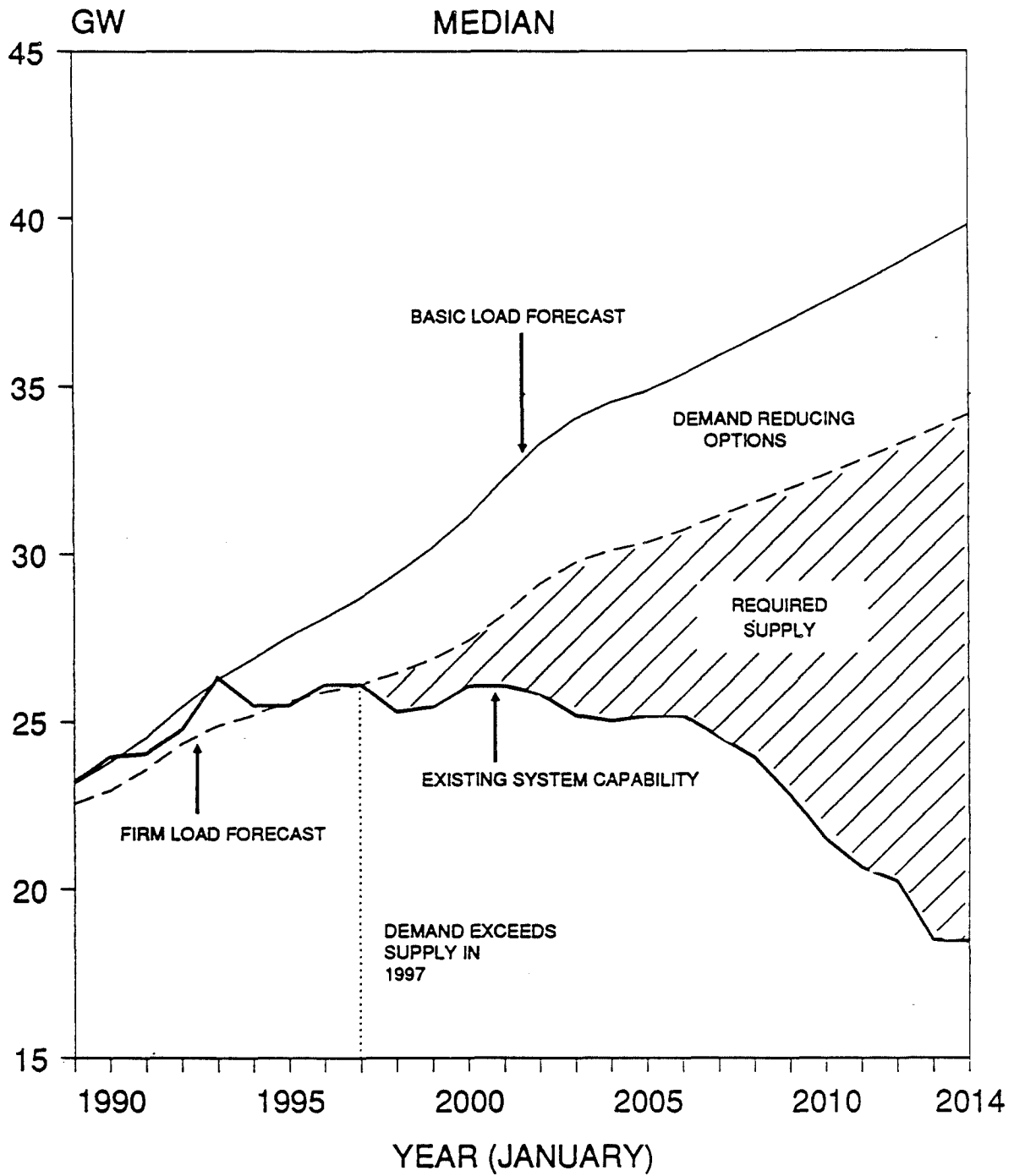


FIGURE 4.11-4

REQUIRED SUPPLY - LMC - PEAK POWER DEMAND
(DATA USED IN ANALYSIS)

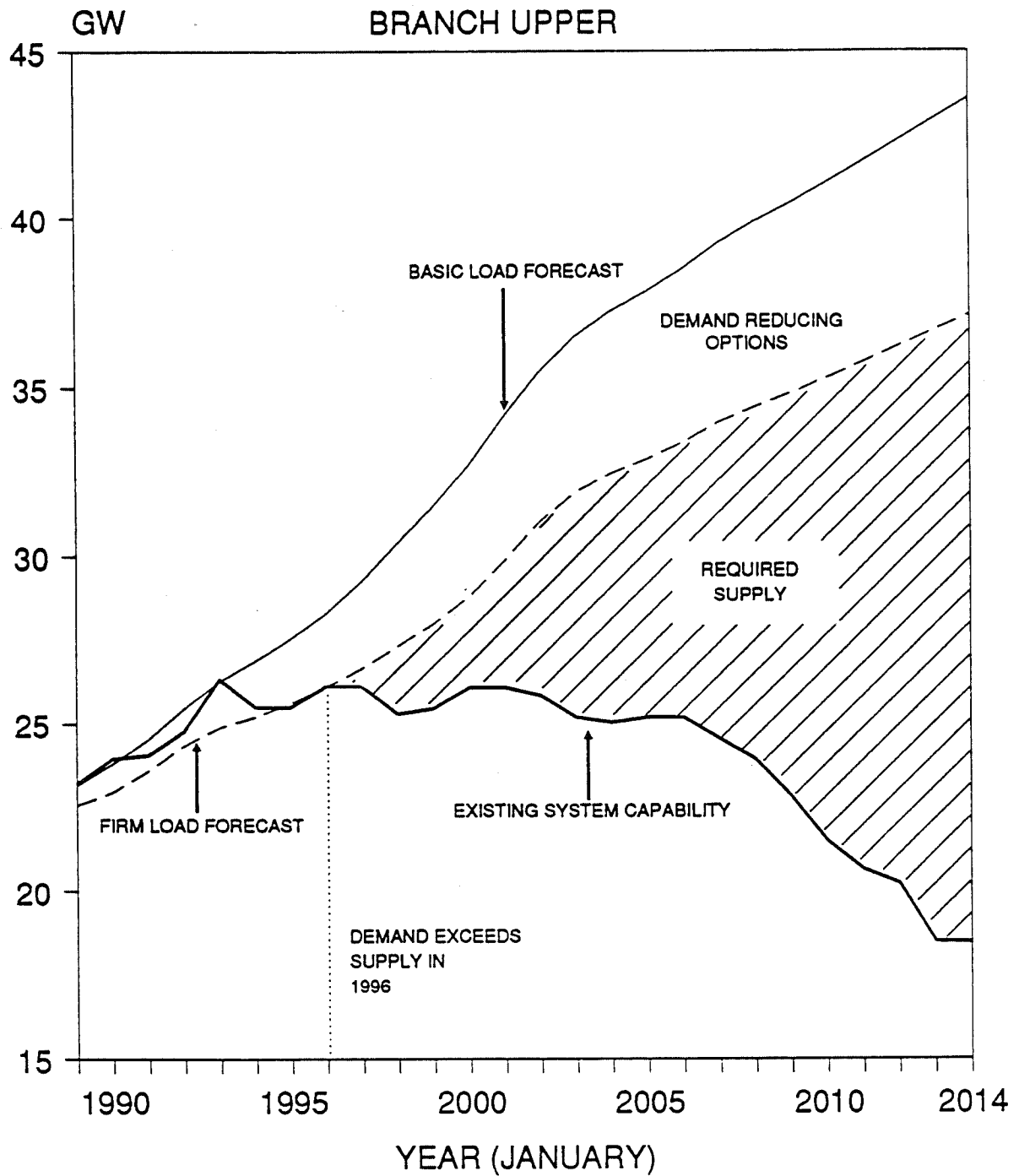


FIGURE 4.11-5

REQUIRED SUPPLY - LMC - PEAK POWER DEMAND
(DATA USED IN ANALYSIS)

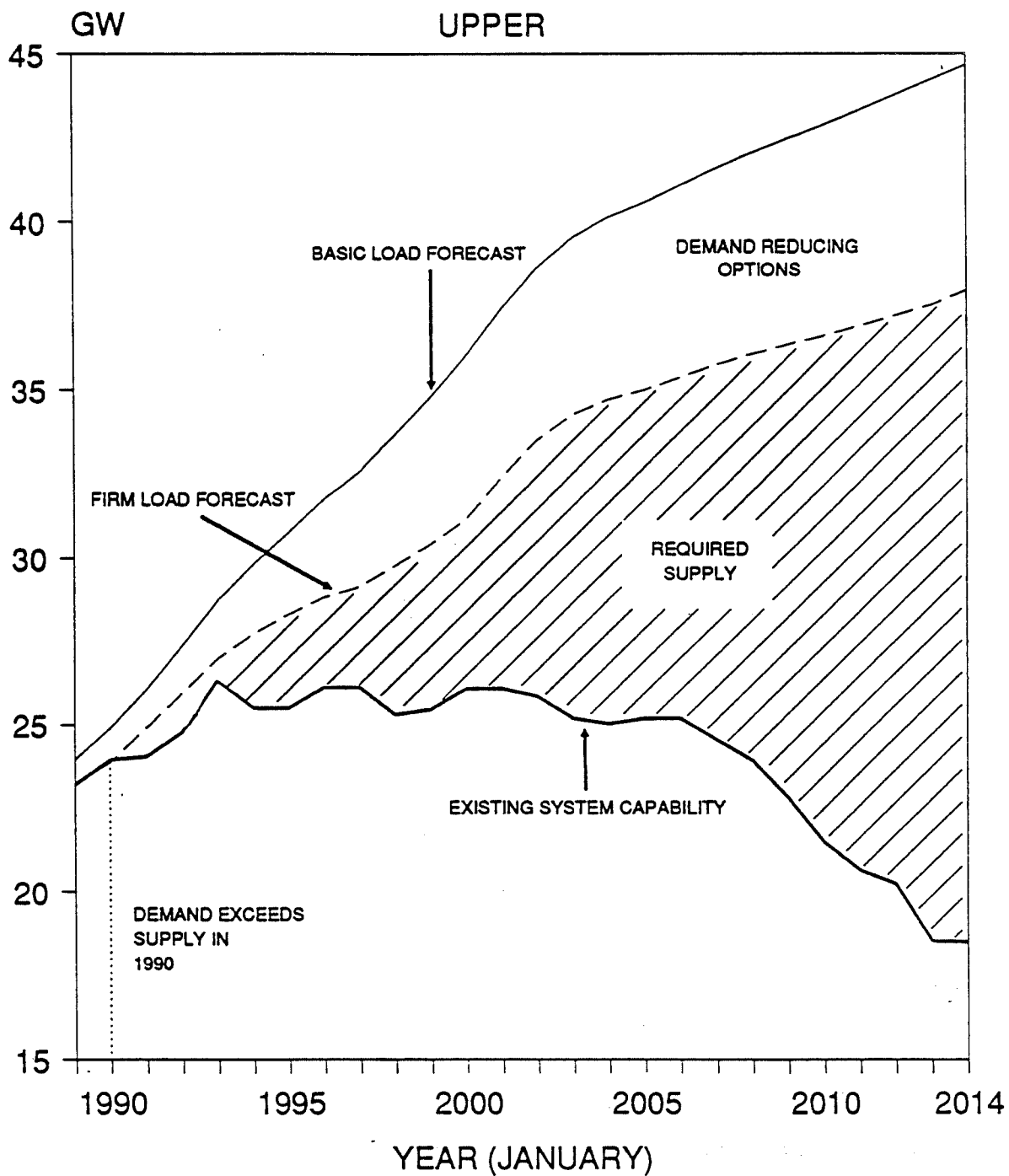
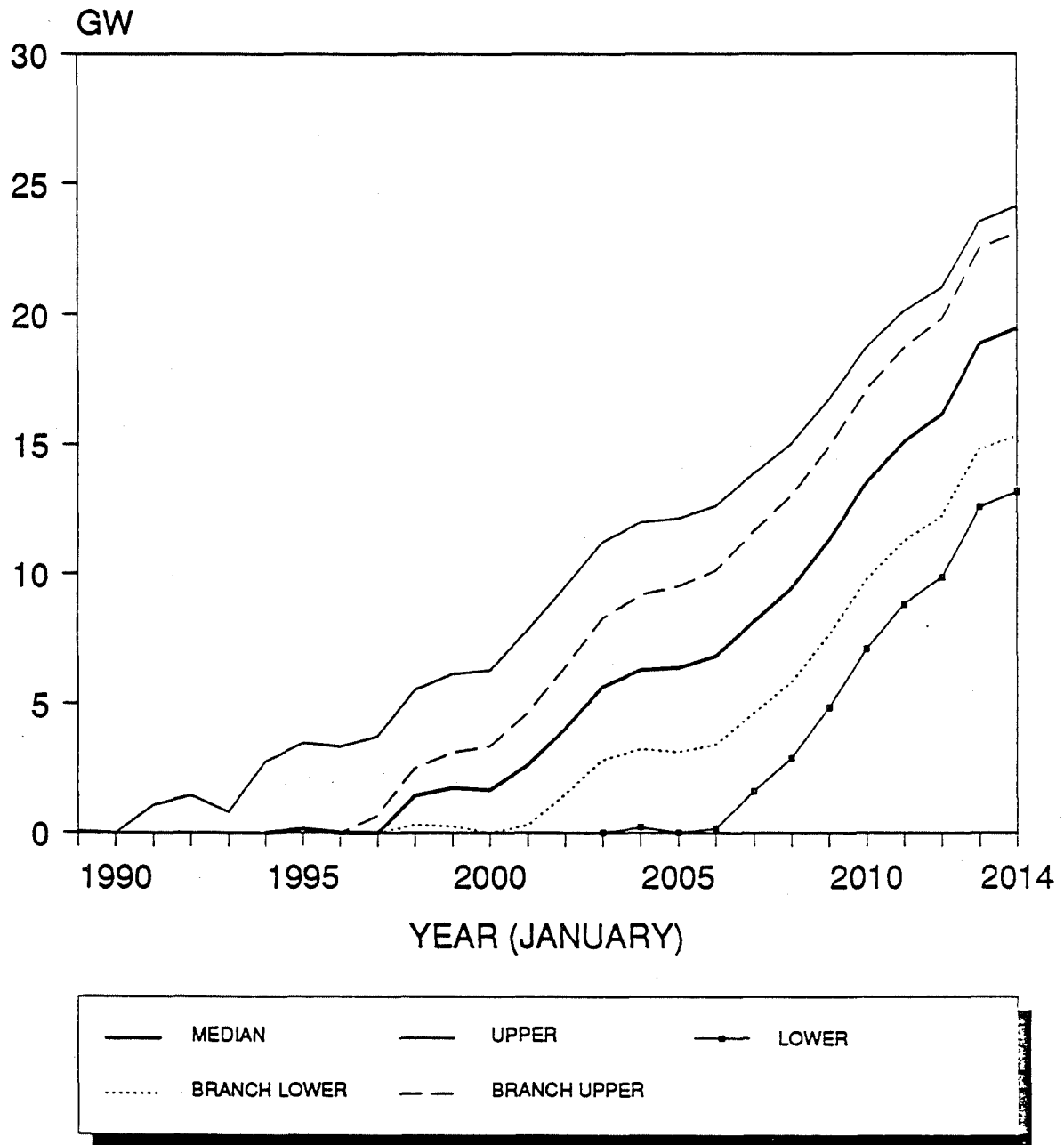


FIGURE 4.11-6
 REQUIRED SUPPLY CAPACITY - PEAK POWER DEMAND
 (DATA USED IN ANALYSIS)



4.12 THE HYDRAULIC PLAN

Chapter 12 of the Plan Report presents Ontario Hydro's proposed Hydraulic Plan. The plan presented is a relatively detailed listing of the specific hydraulic sites which will be developed by a given date, the capacity to be installed, and the energy generating capability to be realised. These details are summarised in Figure 12-7 in the Plan Report.

During demand/supply case formulation, the complete details of this hydraulic program were not finalized. For instance, until recently, the installed capacity of every site was not finalized, nor was the exact sequence of site development. In order to avoid delaying the planning process until such final details became available, demand/supply case formulation proceeded using the then current best estimates of new hydraulic generation. In fact, the projection of new hydraulic generation assumed during the final iterations of case analysis did capture the essence of what would eventually become the proposed Hydraulic Plan.

Figure 4.12-1 below shows the new hydraulic capacity and annual energy production capability which was assumed to be installed by a given date. The same hydraulic program was used throughout the final two phases of demand/supply case formulation and was common to all load forecast paths. Note that Figure 4.12-1 lists the capacity assumed to be in place by January of each given year whereas Figure 12-7 of the Plan Report quotes capacity in-service by the end of the year stated.

Figures 4.12-2 and 4.12-3 are representations of the data in Figure 4.12-1. These figures show new hydraulic capacity and annual energy producing capability, respectively which were assumed when formulating cases.

Figure 4.12-4 compares the hydraulic data used for case formulation with the now current hydraulic plan, as presented in Figure 12-7 of the Plan Report. This comparison shows that the two are generally in close agreement, although in the latter years of the study period the hydraulic capacity assumed during plan formulation differed from that in the current Hydraulic Plan by up to 84 MW. These differences have no significant effect on the applicability of the plans developed and presented in the Plan Report.

**FIGURE 4.12-1: NEW HYDRAULIC PROGRAM
(DATA USED IN PLAN FORMULATION)**

<u>YEARS</u>	<u>NEW CAPACITY (MW)</u>	<u>CUMULATIVE NEW CAPACITY (MW)</u>	<u>CUMULATIVE NEW ANNUAL ENERGY (TWh)</u>
1989	0	0	0
1990	0	0	0
1991	0	0	0
1992	0	0	0
1993	16	16	0.098
1994	0	16	0.098
1995	66	82	0.191
1996	256	338	0.796
1997	180	518	1.432
1998	0	518	1.432
1999	550	1068	2.872
2000	0	1068	2.872
2001	200	1268	3.129
2002	200	1468	3.386
2003	200	1668	3.643
2004	200	1868	3.900
2005	200	2068	4.157
2006	0	2068	4.157
2007	0	2068	4.157
2008	0	2068	4.157
2009	200	2268	4.414
2010	200	2468	4.671
2011	200	2668	4.928
2012	0	2668	4.928
2013	0	2668	4.928
2014	200	2868	5.185

FIGURE 4.12-2
NEW HYDRUALIC PROGRAM
CUMULATIVE INSTALLED CAPACITY USED IN ANALYSIS

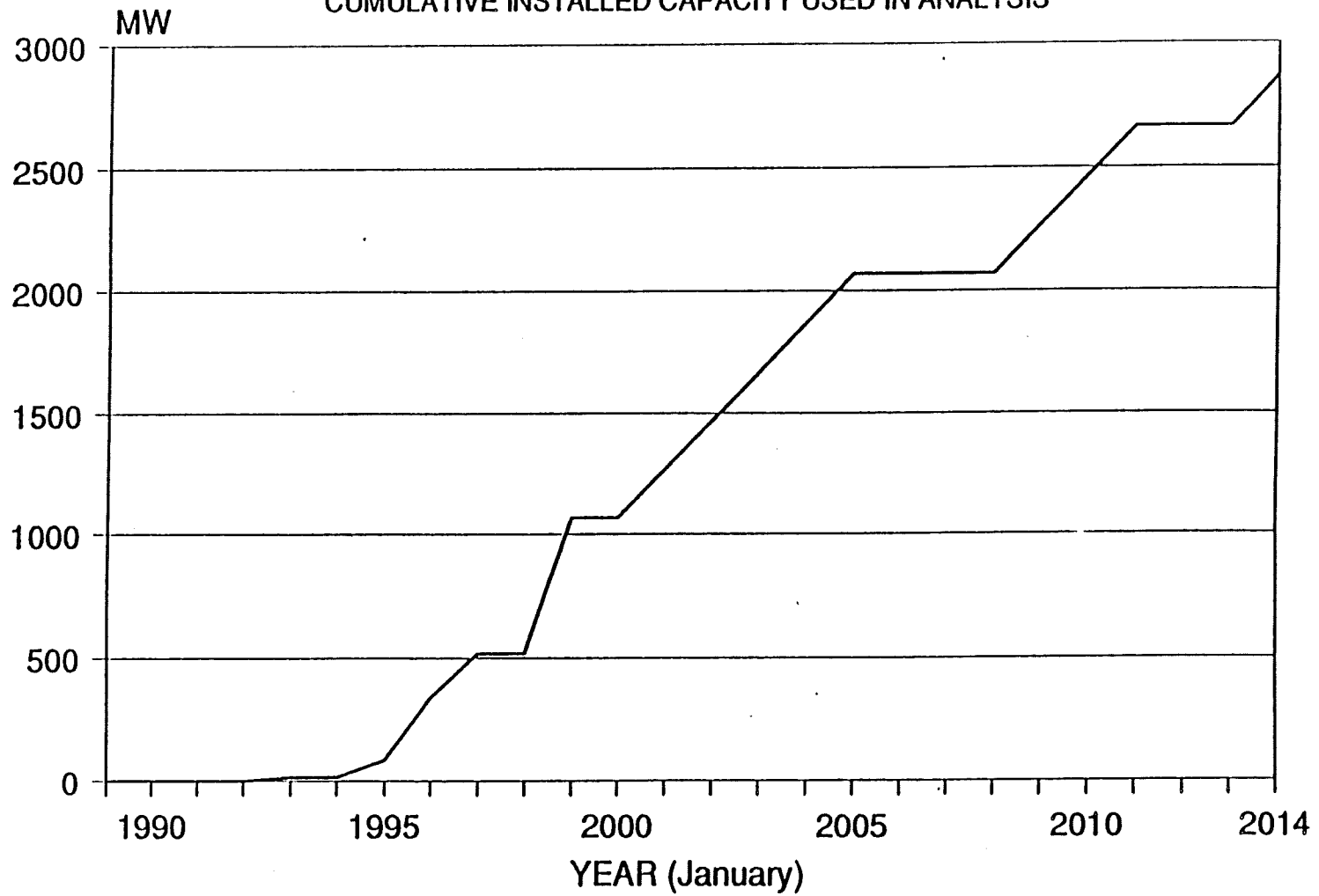


FIGURE 4.12-3 NEW HYDRUALIC PROGRAM ENERGY

(DATA USED IN ANALYSIS)

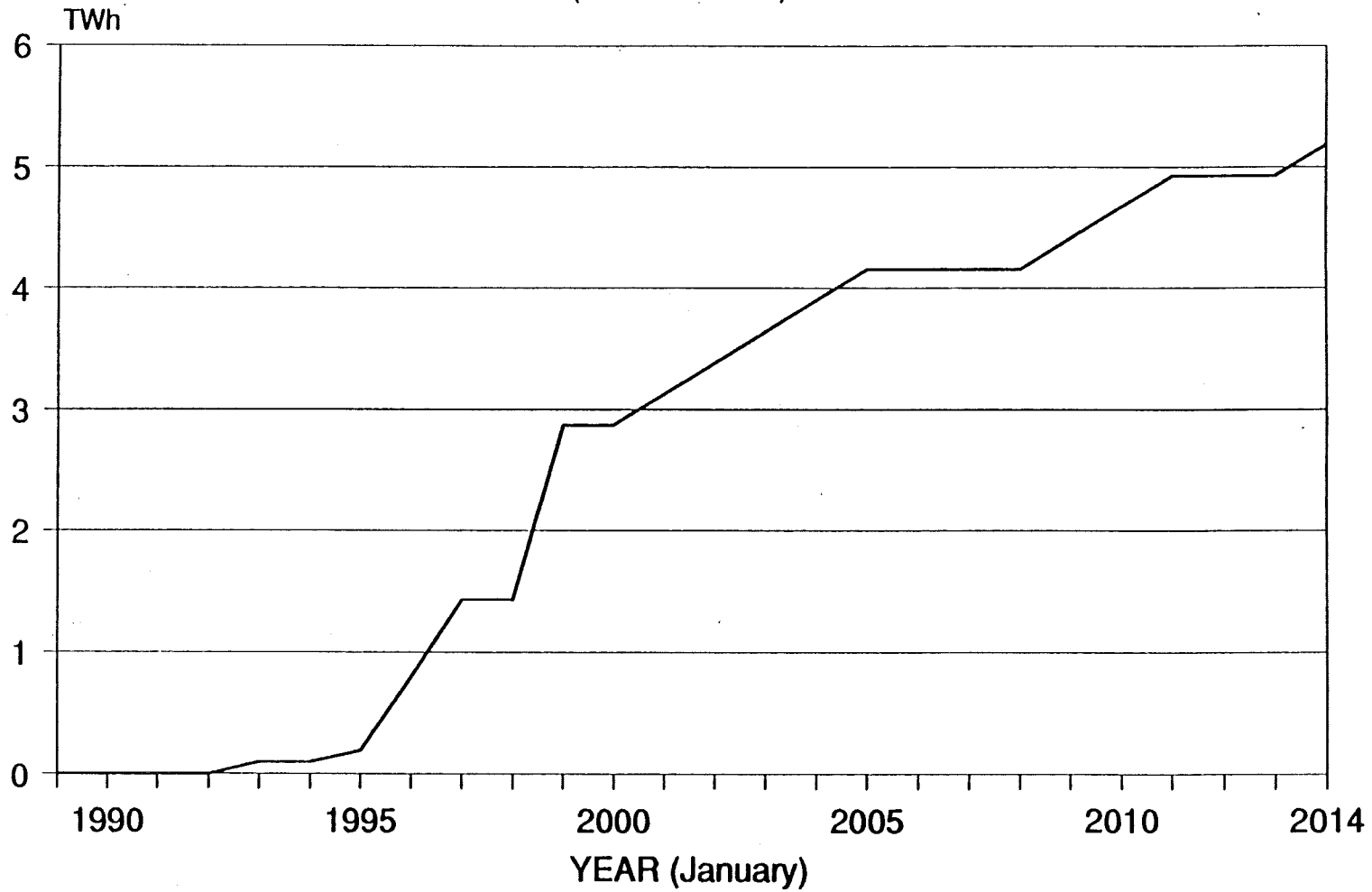


FIGURE 4.12-4

COMPARISON OF NEW HYDRAULIC PROGRAM CAPACITIES
MAIN REPORT vs PLAN ANALYSIS

YEAR (January)	CUMULATIVE CAPACITY (MW)		DIFFERENCE (MW)
	MAIN REPORT	ANALYSIS	
1989	-	0	0
1990	-	0	0
1991	-	0	0
1992	-	0	0
1993	3	16	-13
1994	15	16	-1
1995	83	82	1
1996	333	338	-5
1997	526	518	8
1998	526	518	8
1999	1076	1068	8
2000	1076	1068	8
2001	1209	1268	-59
2002	1409	1468	-59
2003	1608	1668	-60
2004	1808	1868	-60
2005	2008	2068	-60
2006	2053	2068	-15
2007	2120	2068	52
2008	2143	2068	75
2009	2241	2268	-27
2010	2514	2468	46
2011	2584	2668	-84
2012	2653	2668	-15
2013	2718	2668	50
2014	2784	2868	-84

4.13 REQUIREMENT FOR MAJOR SUPPLY

The need for major supply is determined by calculating the difference between the firm load forecast (see Section 4.9) and the ability of the existing system to supply that load, after the additional load meeting capability of the assumed new hydraulic additions (Section 4.12) and purchase non-utility generation (Section 4.8) are considered.

Figures 4.13-1 through 4.13-5 show how this was determined for each of the five load forecast cases. These curves are analogues of Figures 13-1 through 13-3 of the Plan Report.

Figure 4.13-6 shows the projected need for new major supply (in capacity terms) for all five load forecast paths and is analogous to Figure 13-5 in the Plan Report. These two figures are in general agreement. Any differences are insignificant compared to the uncertainty in load growth which is captured by the bandwidth forecast.

4.14 MAJOR SUPPLY OPTIONS

Chapter 13 of the Plan Report and Section 4.13 above identify the projected need for new major supply under the five load forecast paths considered. Chapter 14 of the Plan Report presents a full discussion of the process and rationale which Hydro employed when selecting supply options in order to meet these requirements. That discussion will not be repeated.

Chapter 14 also presents the siting and transmission considerations which were factored into the demand/supply case formulation process. These siting and transmission considerations will not be discussed further here. However, the specific illustrative sites selected for analysis and the transmission facilities required for demand/supply cases under the Branch Upper and Branch Lower forecast conditions are discussed in Chapter 5.

FIGURE 4.13-1
REQUIRED MAJOR SUPPLY - LMC - PEAK POWER DEMAND
(DATA USED IN ANALYSIS)

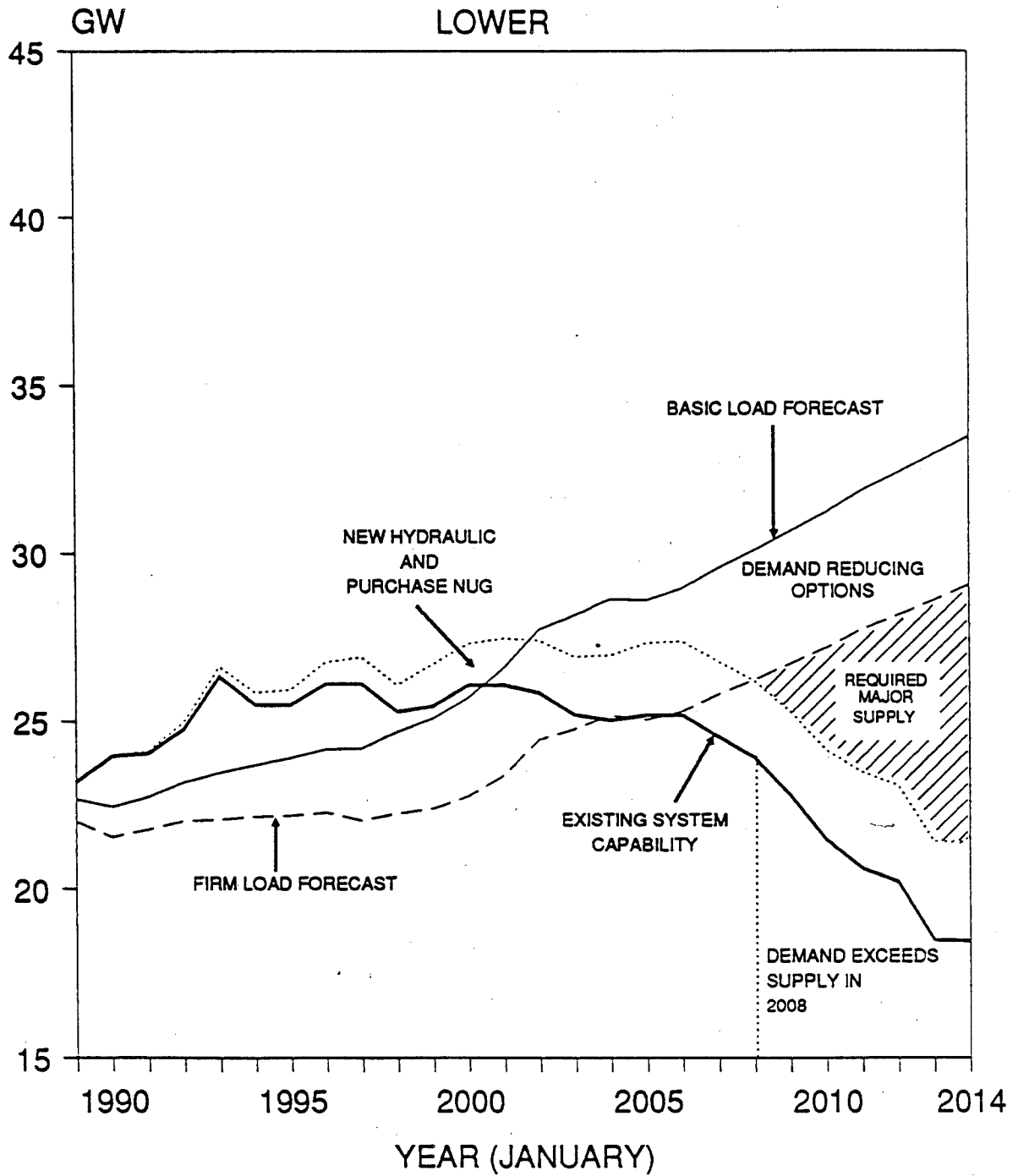


FIGURE 4.13-2
 REQUIRED MAJOR SUPPLY - LMC - PEAK POWER DEMAND
 (DATA USED IN ANALYSIS)

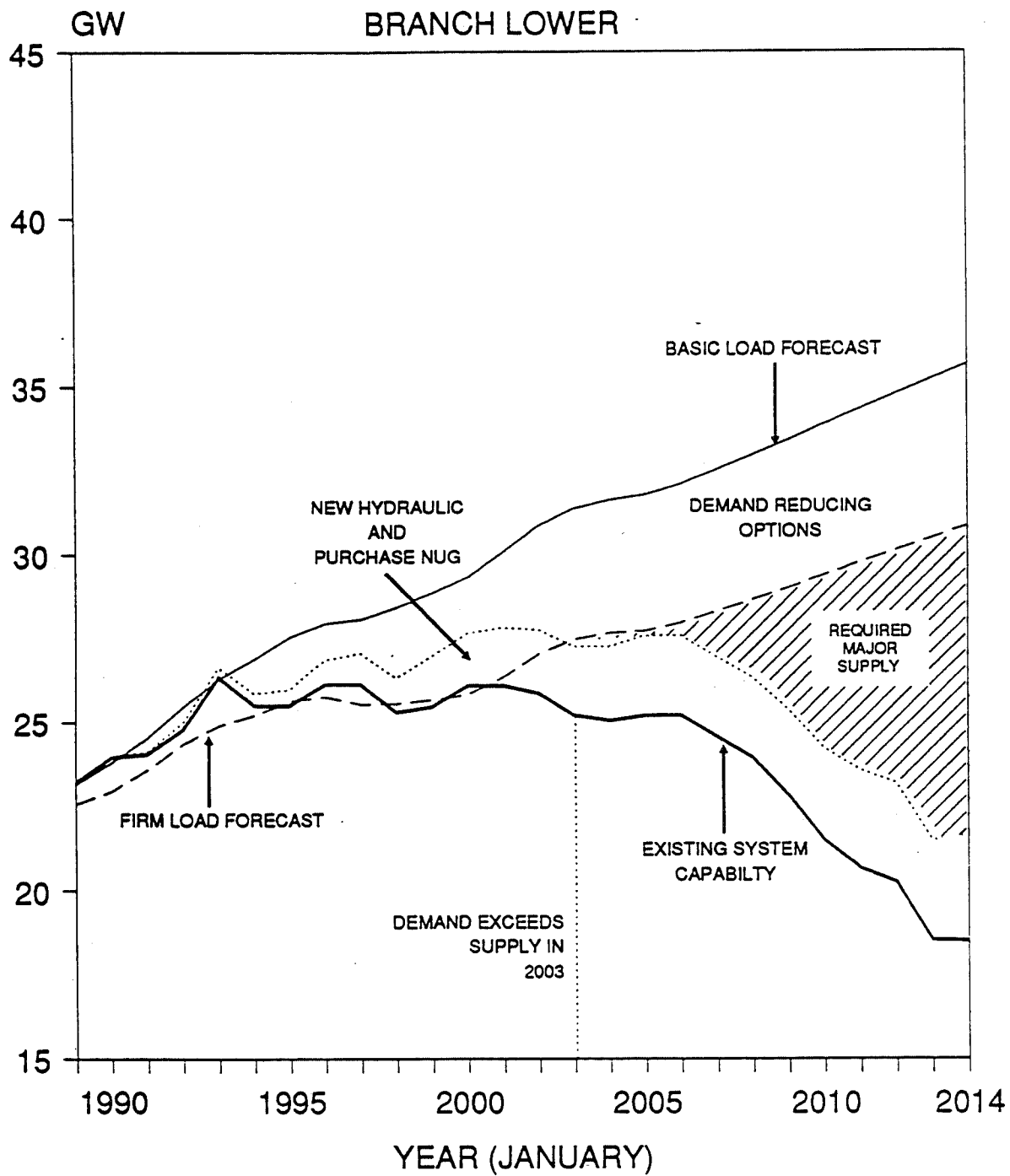


FIGURE 4.13-3
REQUIRED MAJOR SUPPLY - LMC - PEAK POWER DEMAND
 (DATA USED IN ANALYSIS)

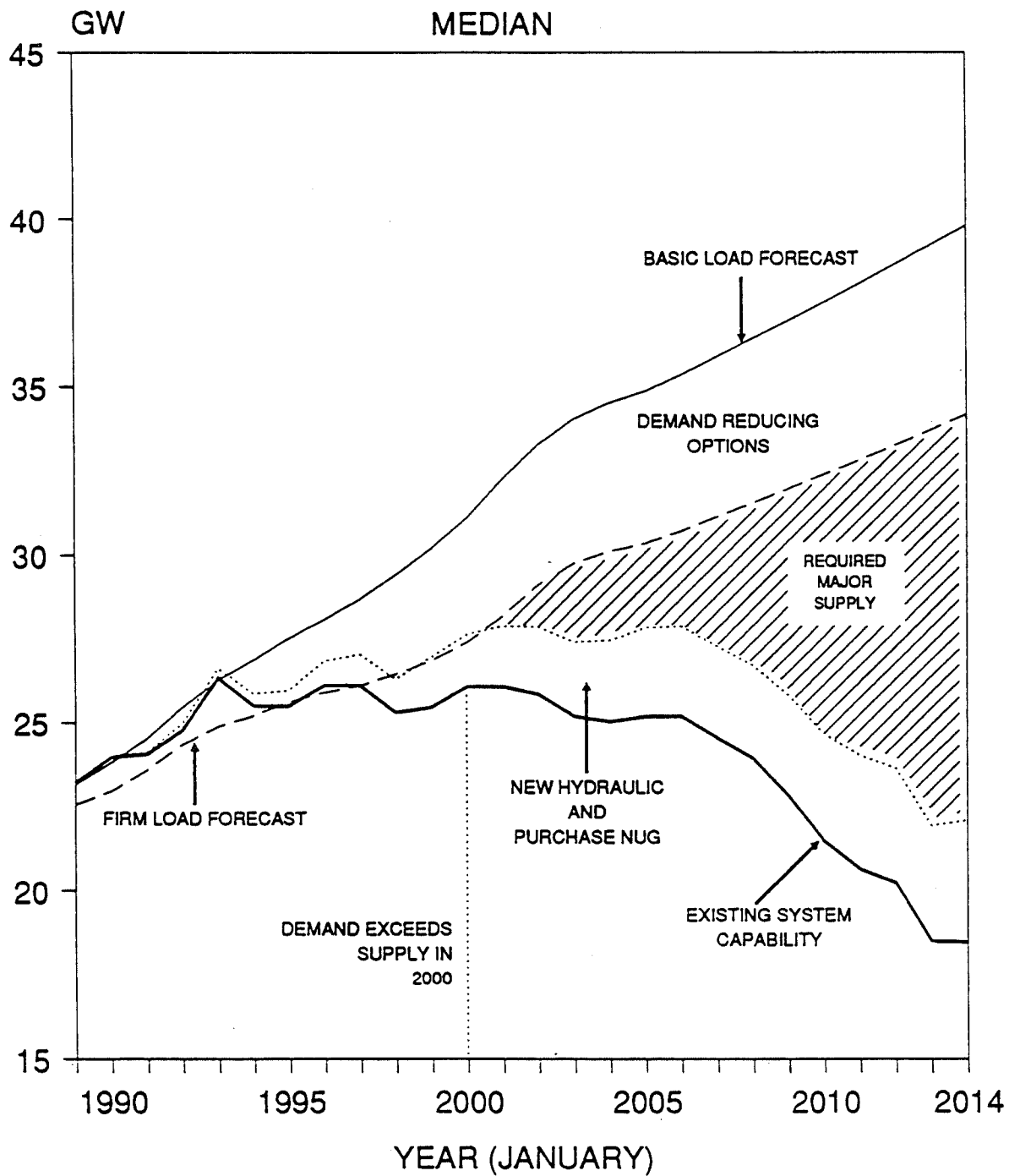


FIGURE 4.13-4
REQUIRED MAJOR SUPPLY - LMC - PEAK POWER DEMAND
(DATA USED IN ANALYSIS)

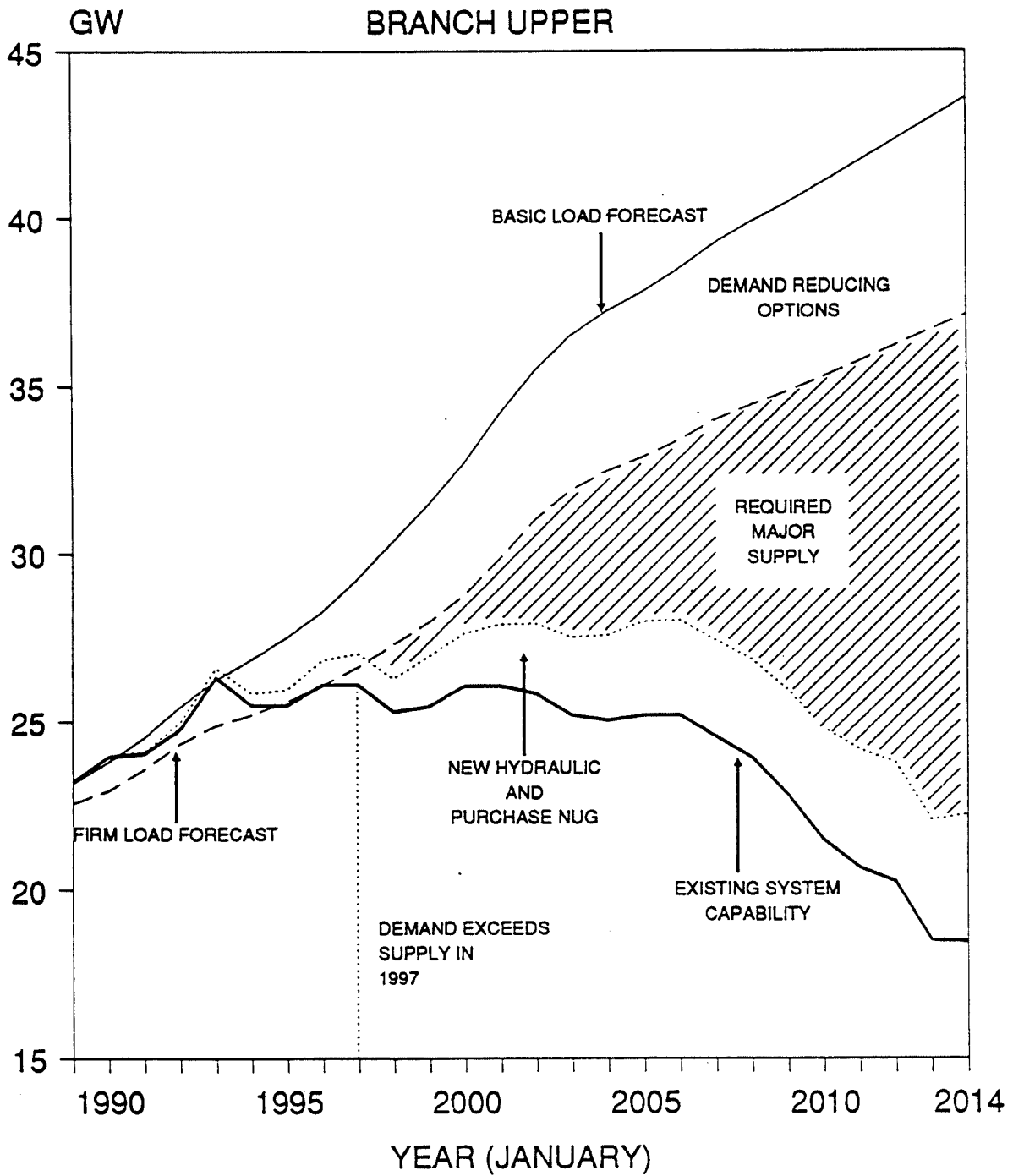


FIGURE 4.13-5
REQUIRED MAJOR SUPPLY - LMC - PEAK POWER DEMAND
 (DATA USED IN ANALYSIS)

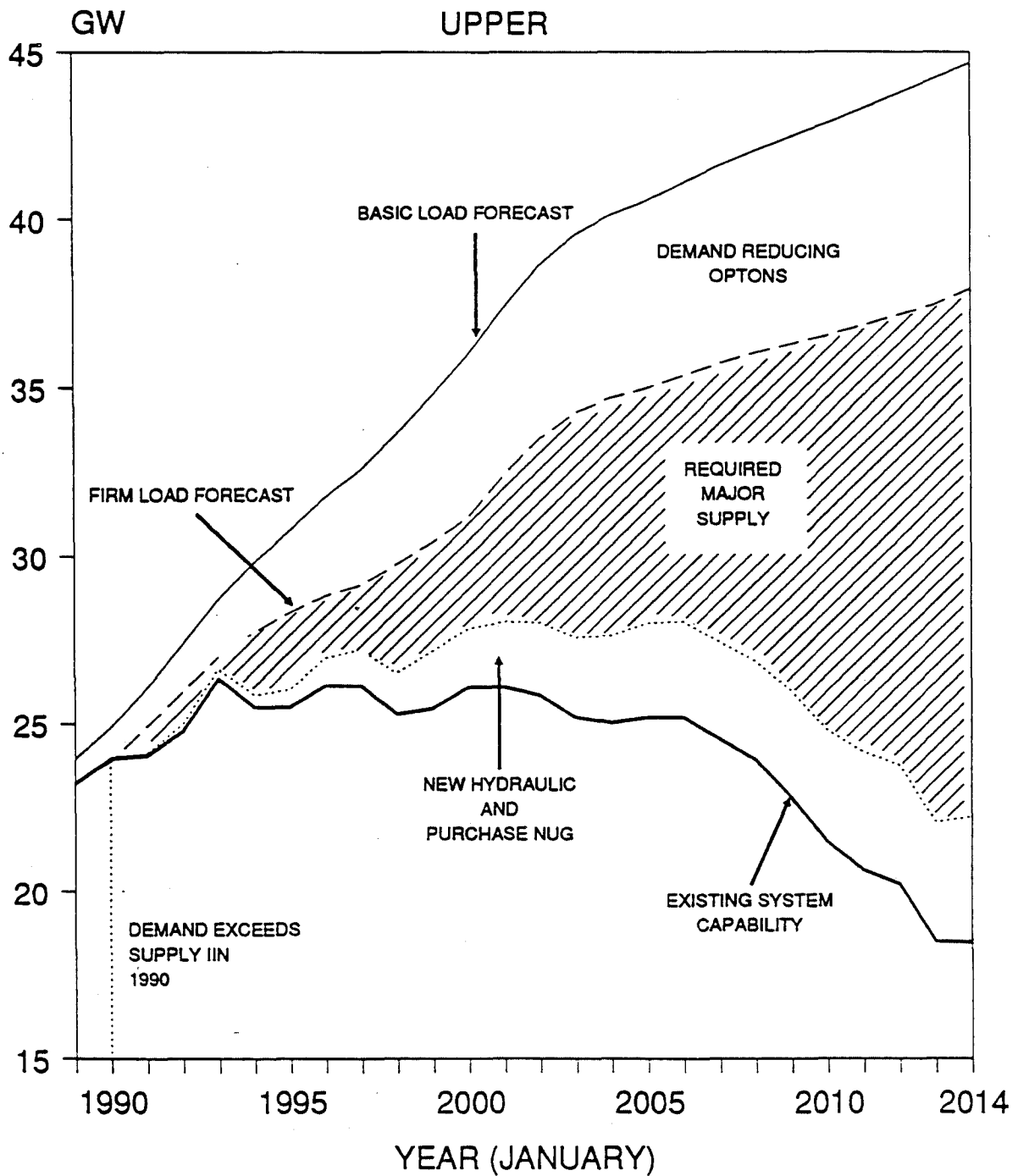
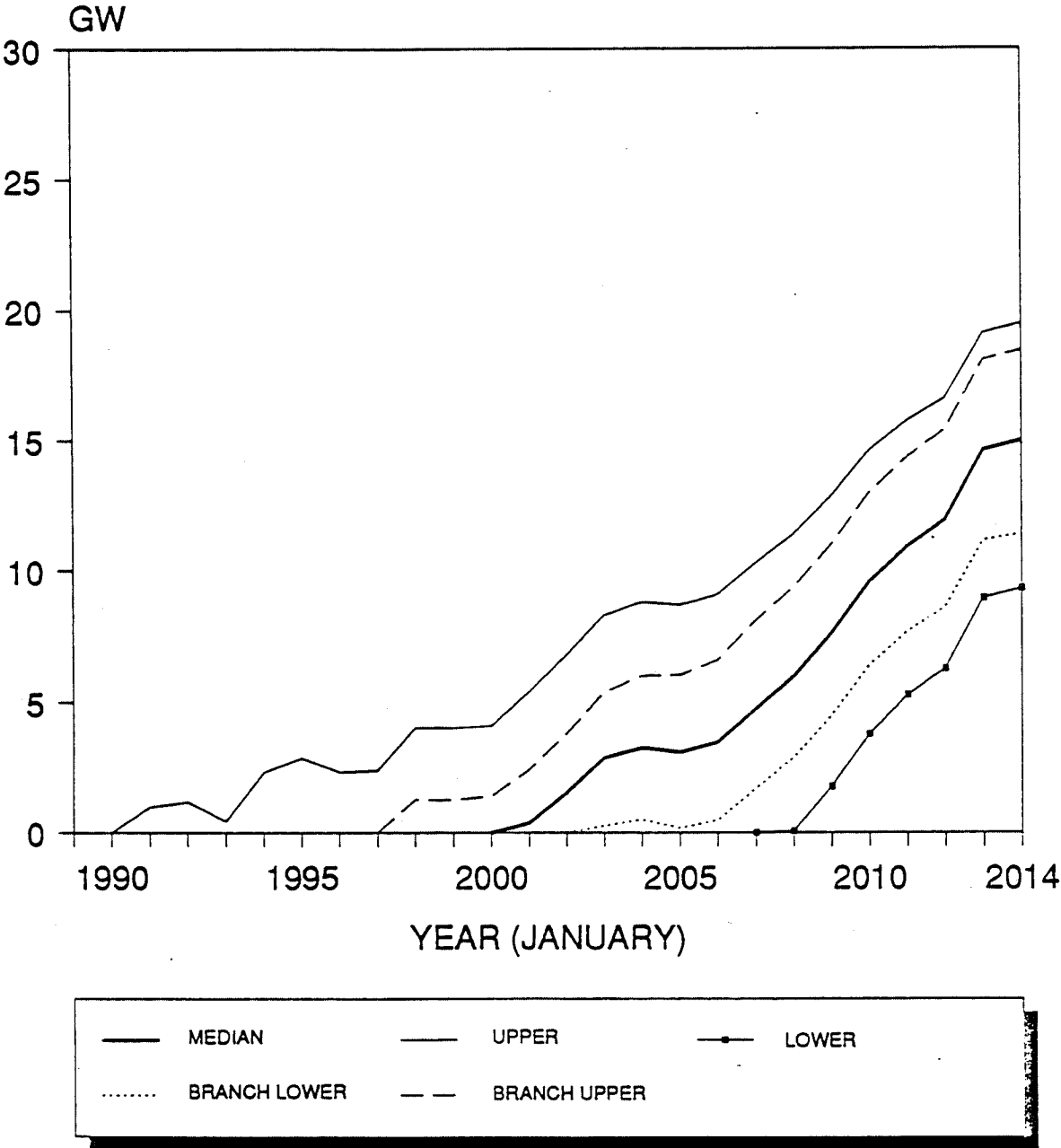


FIGURE 4.13-6
REQUIRED MAJOR SUPPLY CAPACITY - PEAK POWER DEMAND



4.15 MAJOR SUPPLY PLANS

When formulating demand/supply cases, it is necessary to ensure that they can respond adequately to higher or lower demand than was originally expected. That is the reason that all of the cases considered in the Demand/Supply planning process were tested against the five load path constituents of the bandwidth forecast.

One major influence on plan flexibility is the time that it takes to provide a new generating facility. This "leadtime" can be conveniently broken down into two phases: definition and acquisition. The definition phase is the period from the formulation of the intent to install a facility to the date on which that project is committed. The acquisition phase is the period from the decision to build to the in-service date.

The shorter the acquisition phase for a new facility, the closer to the need date that the commitment decision can be made. This is advantageous as there will be less uncertainty as to the eventual need for the facility.

The total leadtime (definition + acquisition) of a facility also has an important influence on plan flexibility. The longer the total leadtime of an option, the more difficult it is to respond to unexpectedly high load growth with that option.

Figure 15-6 of the Plan Report presents typical ranges of leadtimes which are projected for the options which appear in the demand/supply cases. For purposes of analysis, point estimates of the definition and acquisition leadtimes were used rather than ranges. These are tabulated in Figure 4.15-1.

Chapter 15 of the Plan Report presents the in-service dates and capacities of new facilities appearing in major supply cases. Figures 15-10, 15-13, 15-16, 15-19, and 15-22 in the Plan Report provide this detailed information for the Upper, Median, and Lower load forecast paths. Figures 4.15-2 through 4.15-6 in the following pages present the same information, supplemented by the corresponding data for the Branch Upper and Branch Lower load forecasts.

4.16 AVOIDED COST DETERMINATION

The subject of avoided costs is addressed fully in the Plan Report. Hence, it is not discussed in the Analysis Report.

FIGURE 4.15-1: OPTION LEAD TIMES USED IN ANALYSES

OPTION	DESCRIPTION	ASSUMED LEADTIMES (YEARS) *						MONTHS BE- TWEEN UNITS IN-SERVICE
		DEFINITION	EXISTING SITES		TOTAL	NEW SITES		
			CONSTRUCTION			CONSTRUCTION		
1	4x800 MW US COAL CSC/FGD/SCR	5.75	5.5	11.25	5.75	6.5	12.25	12
5	2x150 MW CTU/NC	2	1.25	3.25	-	-	-	6
7	CTU/CC (1st PHASE)	5.75	2	7.75	5.75	3	8.75	9
8	CTU/IGCC (1st PHASE)	5.75	2	7.75	5.75	3	8.75	9
11	4x881 MW CANDU	4.75	7.5	12.25	4.75	8.5	13.25	12
	HEARN REHABILITATION	-	-	4	N/A	N/A	N/A	N/A

* CONSTRUCTION LEADTIME COVERS THE PERIOD FROM PROJECT COMMITMENT TO FIRST UNIT, FIRST POWER

Figure 4.15-2

MAJOR SUPPLY ADDITIONS BY 2014

Case 15

LOWER FORECAST

Capacity Added By Year End

Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Manitoba Purchase			1,000									800		800	200	400											
CTUWCC	A	1-6	1,008																		672	336					
CTUWCC	A	1-12	2,016																				1,008	336	336	336	
CANDU	B	1-4	3,524																				881	881	881	881	
CTUWCC	B	13-14	0,336																							336	
CANDU	A	5-6	1,762																							881	881
Total (GW)																											

BRANCH LOWER FORECAST

Capacity Added By Year End

Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Manitoba Purchase			1,000									200		200	200	400											
CANDU	A	1-4	3,524														881	881	881	881							
CTUWCC	A	1-6	1,008																			1,008					
CTUWCC	A	1-12	2,016																			1,008	1,008				
CANDU	B	5-7	2,643																						881	881	881
CTUWCC	B	13-22	1,680																							1,680	
Total (GW)			11.871																								

MEDIUM FORECAST

Capacity Added By Year End

Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Manitoba Purchase			1,000									200		200	200	400											
CTUWCC	A	1-6	1,008												336	672											
CTUWCC	A	1-12	2,016													336						1680					
CANDU	A	1-4	3,524														881	881	881	881							
CTUWCC	B	13-24	2,016																				1008	672		336	
CANDU	B	5-8	3,524																				881	881	881	881	
CTUWCC	C	25-26	0,336																							336	
CANDU	C	9-10	1,762																							881	881
Total (GW)			15,186																								

Figure 4.15-2(Cont'd)

BRANCH UPPER FORECAST												
Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998
Market Purchase												
CTUWCC	A	1.006	1.006									
CTUWCC	A	2.016	2.016									
CTUWCC	B	1.006	1.006									
CANDU	A	3.524	3.524									
CANDU	B	2.016	2.016									
CTUWCC	B	3.524	3.524									
CTUWCC	C	1.006	1.006									
Total (GW)				18.626								

UPPER FORECAST												
Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998
Market Purchase												
CTU	A	1.4	1.000									
CTU	B	5.6	0.672				672	672				
CTUWCC	A	1-12	2.016									
CTU	C	6-10	0.328									
CTUWCC	B	13-16	1.006									
CANDU	A	1-4	3.524									
CTUWCC	C	16-24	1.006									
CANDU	B	6-9	3.524									
CANDU	C	6-12	3.524									
CTUWCC	D	25-26	0.672									
CANDU	D	13-14	1.762									
Total (GW)				19.716								

Figure 4.15-3

MAJOR SUPPLY ADDITIONS BY 2014

Case 22

LOWER FORECAST					Capacity Added By Year End (MW)																							
Option	Station	Units	Capacity	(GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Manitoba Purchase			1,000												200		200	200	400									
CANDU	A	1-4	3,524																			881	881	881	881			
CANDU	B	5-8	3,524																						881	881	881	881
CTU/AGCC	A	1-10	1,680																									1,680
Total (GW)				9.728																								

BRANCH LOWER FORECAST					Capacity Added By Year End (MW)																							
Option	Station	Units	Capacity	(GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Manitoba Purchase			1,000												200		200	200	400									
CANDU	A	1-4	3,524														881	881	881	881								
CTU/AGCC	A	1-6	1,008																					1,008				
CTU/AGCC	A	1-12	2,016																						1,008	336	672	
CANDU	B	5-8	3,524																						881	881	881	881
CTU/AGCC	B	13-16	0,672																									672
Total (GW)				11.744																								

MEDIAN FORECAST					Capacity Added By Year End (MW)																							
Option	Station	Units	Capacity	(GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Manitoba Purchase			1,000												200		200	200	400									
CANDU	A	1-4	3,524														881	881	881	881								
CANDU	B	5-8	3,524																		881	881	881	881				
CTU/AGCC	A	1-6	1,008																				336	672				
CTU/AGCC	A	1-12	2,016																					336	672	1,008		
CANDU	C	9-12	3,524																						881	881	881	881
CTU/AGCC	B	13-16	0,672																									672
Total (GW)				15.268																								

Figure 4.15-3(Cont'd)

BRANCH UPPER FORECAST				Capacity Added By Year End (MW)																									
Option	Station	Units	Capacity (GW)	1900	1901	1902	1903	1904	1905	1906	1907	1908	1909	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013		
Marble Purchase																													
GTUOC	A	1-4	1,008																										
CANOU	A	1-4	3,524																										
GTUOC	A	1-12	2,016																										
CANOU	B	5-9	3,524																										
CANOU	C	9-12	3,524																										
GTUOC	B	13-24	2,016																										
GTUOC	C	25-36	0,336																										
CANOU	D	13-14	1,762																										
Total (GW)			18,710																										

UPPER FORECAST				Capacity Added By Year End (MW)																									
Option	Station	Units	Capacity (GW)	1900	1901	1902	1903	1904	1905	1906	1907	1908	1909	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013		
Marble Purchase																													
GTUWC	A	1-4	1,000																										
GTUWC	B	5-9	0,672																										
GTUWC	A	1-12	2,016																										
CANOU	A	1-4	3,524																										
GTUWC	A	1-4	0,672																										
GTUWC	B	5-10	1,008																										
CANOU	B	5-9	3,524																										
CANOU	C	9-12	3,524																										
GTUWC	B	13-16	0,672																										
CANOU	D	13-15	2,643																										
Total (GW)			19,927																										

Figure 4.15-4

MAJOR SUPPLY ADDITIONS BY 2014

Case 23

LOWER FORECAST

Capacity Added By Year End (MW)

Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Manitoba Purchase			1,000									200		200	200	400											
CANDU	A	1-4	3,524										881	881	881	881											
CANDU	B	5-8	3,524																					881	881	881	881
CANDU	C	9-10	1,762																							881	881
CTUGCC	A	1-2	0.336																							236	
Total (GW)																											
10,146																											

BRANCH LOWER FORECAST

Capacity Added By Year End (MW)

Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Manitoba Purchase			1,000									200		200	200	400											
CANDU	A	1-4	3,524										881	881	881	881											
CANDU	B	5-8	3,524														881	881	881								
CANDU	C	9-11	2,843																						881	881	881
CANDU	D	12-13	1,762																							881	881
Total (GW)																											
12,453																											

MEDIAN FORECAST

Capacity Added By Year End (MW)

Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Manitoba Purchase			1,000									200		200	200	400											
CANDU	A	1-4	3,524										881	881	881	881											
CANDU	B	5-8	3,524													881	881	881	881								
CANDU	C	9-12	3,524																					881	881	881	881
CANDU	D	13-16	3,524																					881	881	881	881
Total (GW)																											
15,006																											

Figure 4.15-4 (Cont'd)

BRANCH UPPER FORECAST

Capacity Added By Year End (MW)

Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Mantabeg Purchase			1.000									200		200	200	400											
CANDU A	A	1-4	3.524										881	881	881	881											
CANDU B	B	5-8	3.524														881	881	881								
CANDU C	C	9-12	3.524																		881	881	881	881			
CANDU D	D	13-16	3.524																								
CTUWGOC A	A	1-4	1.008																								1008
CANDU E	E	17-18	1.782																							881	881
CANDU F	F	19-20	1.782																							881	881

Total (GW) 19.628

UPPER FORECAST

Capacity Added By Year End (MW)

Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Mantabeg Purchase			1.000									200		200	200	400											
CTUWG A	A	1-4	0.672				672																				
CTUWG B	B	5-8	0.672					672																			
CTUWGOC A	A	1-4	1.344							1344																	
CANDU A	A	1-4	3.524										881	881	881	881											
CANDU B	B	5-8	3.524														881	881	881	881							
CANDU C	C	9-12	3.524																		881	881	881	881			
CANDU D	D	13-16	3.524																								
CANDU E	E	17-18	1.782																							881	881

Total (GW) 19.546

Figure 4.15-5

MAJOR SUPPLY ADDITIONS BY 2014

Case 24

LOWER FORECAST				Capacity Added By Year End (MW)																							
Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Manitoba Purchase			1,000									200		200	200	400											
CTU/GC	A	1-6	1,008																		672	336					
CTU/GCC	A	1-12	2,016																			1,008	336	336	336		
CANDU	A	1-4	3,524																				881	881	881	881	
CSC COAL	A	1-2	1,482																							741	741
CTU/GCC	B	13-14	0,336																							336	

BRANCH LOWER FORECAST				Capacity Added By Year End (MW)																							
Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Manitoba Purchase			1,000									200		200	200	400											
CANDU	A	1-4	3,524														881	881	881	881							
GTU/GC	A	1-6	1,008																			672	336				
GTU/GCC	A	1-12	2,016																				1,008	336			
GTU/GCC	B	13-24	2,016																					672		1,344	
CSC COAL	A	1-4	2,223																						741	741	741
Total (GW)			11,787																								

MEDIAN FORECAST				Capacity Added By Year End (MW)																									
Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013		
Manitoba Purchase			1,000									200		200	200	400													
CTU/GCC	A	1-6	1,008												336	672													
CTU/GCC	A	1-12	2,016													836						672	1,008						
CANDU	A	1-4	3,524														881	881	881	881									
CTU/GCC	B	13-24	2,016																			672	1,008	336					
CSC COAL	A	1-4	2,964																				741	741	741	741			
GTU/GCC	C	25-30	1,008																					336		672			
CANDU	B	5-6	1,762																							881	881		
Total (GW)			15,298																										

Figure 4.15-5(cont'd)

BRANCH UPPER FORECAST				Capacity Added By Year End (MW)																									
Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013		
Manitoba Purchase			1.000									200		200	200	400													
CTU/CC	A	1-6	1.008											1008															
CTU/GCC	A	1-12	2.016												1344	672													
CTU/CC	B	7-12	1.008													336					672								
CANDU	A	1-4	3.524														881	881	881	881									
CSC COAL	A	1-4	2.964																			741	741	741	741				
CTU/GCC	B	13-24	2.016																		336	672	336				672		
CANDU	B	5-8	3.524																				881	881	881	881			
CTU/GCC	C	25-34	1.680																							1008	672		
Total (GW)			18.740																										

UPPER FORECAST					Capacity Added By Year End (MW)																							
Option	Station	Units	Capacity (GW)		1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Manitoba Purchase			1.000										200		200	200	400											
CTU/CC	A	1-4	0.872					872																				
CTU/CC	B	5-8	0.872						872																			
CTU/GCC	A	1-12	2.016									1344			336	336												
CTU/GCC	B	13-18	1.008													1008												
CTU/CC	A	1-4	0.872														672											
CANDU	A	1-4	3.524															881	881	881	881							
CTU/CC	B	5-10	1.008																				672					
CTU/GCC	C	19-24	1.008																				336					672
CSC COAL	A	1-4	2.964																					741	741	741	741	
CANDU	B	5-8	3.524																					881	881	881	881	
CANDU	C	9-10	1.762																								881	881
Total (GW)			19.830																									

Figure 4.15-6

MAJOR SUPPLY ADDITIONS BY 2014

Case 26

LOWER FORECAST

Capacity Added By Year End (MW)

Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Montrose Purchase			1,000									200		200	200	400											
CTUWCC	A	1-6	1,008																		672	336					
CTUWGCC	A	1-12	2,016																				1,008	336	672		
CSC COAL	A	1-4	2,964																				741	741	741	741	
CSC COAL	B	5-8	1,482																							741	741
CTUWGCC	B	13-18	1,008																							1,008	

Total (GW) 9.478

BRANCH LOWER FORECAST

Capacity Added By Year End (MW)

Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Montrose Purchase			1,000									200		200	200	400											
CSC COAL	A	1-4	2,964														741	741	741	741							
CTUWCC	A	1-6	1,008																			336	672				
CTUWGCC	A	1-12	2,016																				1,344	672			
CTUWGCC	B	13-24	2,016																					672	336	1,008	
CSC COAL	B	5-7	2,223																						741	741	741
CTUWGCC	C	25-28	0,672																							672	

Total (GW) 11.699

MEDIAN FORECAST

Capacity Added By Year End (MW)

Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Montrose Purchase			1,000									200		200	200	400											
CTUWCC	A	1-6	1,008												336	672											
CTUWGCC	A	1-12	2,016													336					672	1,008					
CSC COAL	A	1-4	2,964														741	741	741	741							
CTUWGCC	B	13-24	2,016																			672	1,008	336			
CSC COAL	B	5-8	2,964																				741	741	741	741	
CTUWGCC	C	25-34	1,482																					336	336	1,008	
CSC COAL	C	9-10	1,482																							741	741

Total (GW) 15.130

Figure 4.15-6 (Cont'd)

BRANCH UPPER FORECAST

Capacity Added By Year End (MW)

Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Manitoba Purchase			1.000											200	200	200	400										
CTU/CC	A	1-4	1.008											1008													
CTU/GCC	A	1-12	2.016												1344	872											
CTU/GCC	B	13-18	1.008													336											
CSC COAL	A	1-4	2.964														741	741	741	741							
CTU/CC	B	7-12	1.008																		836	672					
CSC COAL	B	5-8	2.964																		741	741	741	741			
CTU/GCC	C	19-30	2.016																			336	672				
CSC COAL	C	9-12	2.964																				741	741	741	741	
CTU/GCC	D	31-40	1.680																							1008	672

Total (GW) 18.628

UPPER FORECAST

Capacity Added By Year End (MW)

Option	Station	Units	Capacity (GW)	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013
Manitoba Purchase			1.000											200	200	200	400										
CTU/NC	A	1-4	0.672				672																				
CTU/NC	B	5-8	0.672					672																			
CTU/GCC	A	1-12	2.016								1344			336	336												
CTU/GCC	B	13-18	1.008												1008												
CTU/CC	A	1-4	1.008													872	336										
CSC COAL	A	1-4	2.964													741	741	741	741								
CTU/CC	B	5-12	1.008														336										
CTU/GCC	C	19-30	2.016																			336					
CSC COAL	B	5-8	2.964																			741	741	741	741		
CSC COAL	C	9-12	2.964																				741	741	741	741	
CSC COAL	D	13-14	1.482																							741	741

Total (GW) 19.774

4.17 DEMAND/SUPPLY PLANS

Figures 17-16, 17-17, and 17-18 in the Plan Report provide a convenient summary of the components of the three Alternative Demand/Supply Plans under Median forecast conditions. These were created from data appearing in Appendix I of this analysis report. Figures 4.17-1 through 4.17-15 below are comparable figures based on the data used in demand/supply case formulation. Figures are provided pertaining to the three Alternative Demand/Supply Plans under all five load forecast conditions.

For any given load forecast condition, the Demand Management contribution shown in these figures is that assumed to pertain to the corresponding load path during demand/supply case formulation and presented in Section 4.7 of this Analysis Report. The non-utility generation contribution is discussed in Section 4.8.

Common Rehabilitation and Hydraulic Generation Plans were assumed for all cases under all load forecast conditions, as shown in Figures 4.17-1 through 4.17-15. The assumed contributions are discussed in Analysis Report Sections 4.10 and 4.12, respectively. The Manitoba Purchase, which is also common to the five cases presented in the Plan Report, is discussed in detail in Chapters 14 and 15 of that Report.

For details on the magnitude and timing of major supply additions (new fossil or nuclear plant), which are shown for each of the Alternative Demand/Supply Plans in Figures 4.17-1 through 4.17-15, refer to the appropriate table appearing in Section 4.15.

4.18 ACTION PLANS

As stated in the Plan Report, an Action Plan is a set of timely actions which must be taken to implement a Demand/Supply Plan to meet effectively the future energy needs of the province. An Action Plan was developed for each of the Candidate Demand/Supply Plans which, if approved, would allow facilities required for the Upper load forecast condition to be placed into service in a timely manner. If the actual load growth trend is below the Upper forecast, project commitments would be delayed accordingly. Therefore, the Action Plans will cater to all five of the load forecast paths considered during plan formulation and analysis. Chapter 18 of the Plan Report presents these detailed Action Plans for the three Candidate Demand/Supply Plans and describes how these were developed. This discussion will not be repeated here.

FIGURE 4.17-1
PLAN 15
DATA USED IN ANALYSIS - LOWER

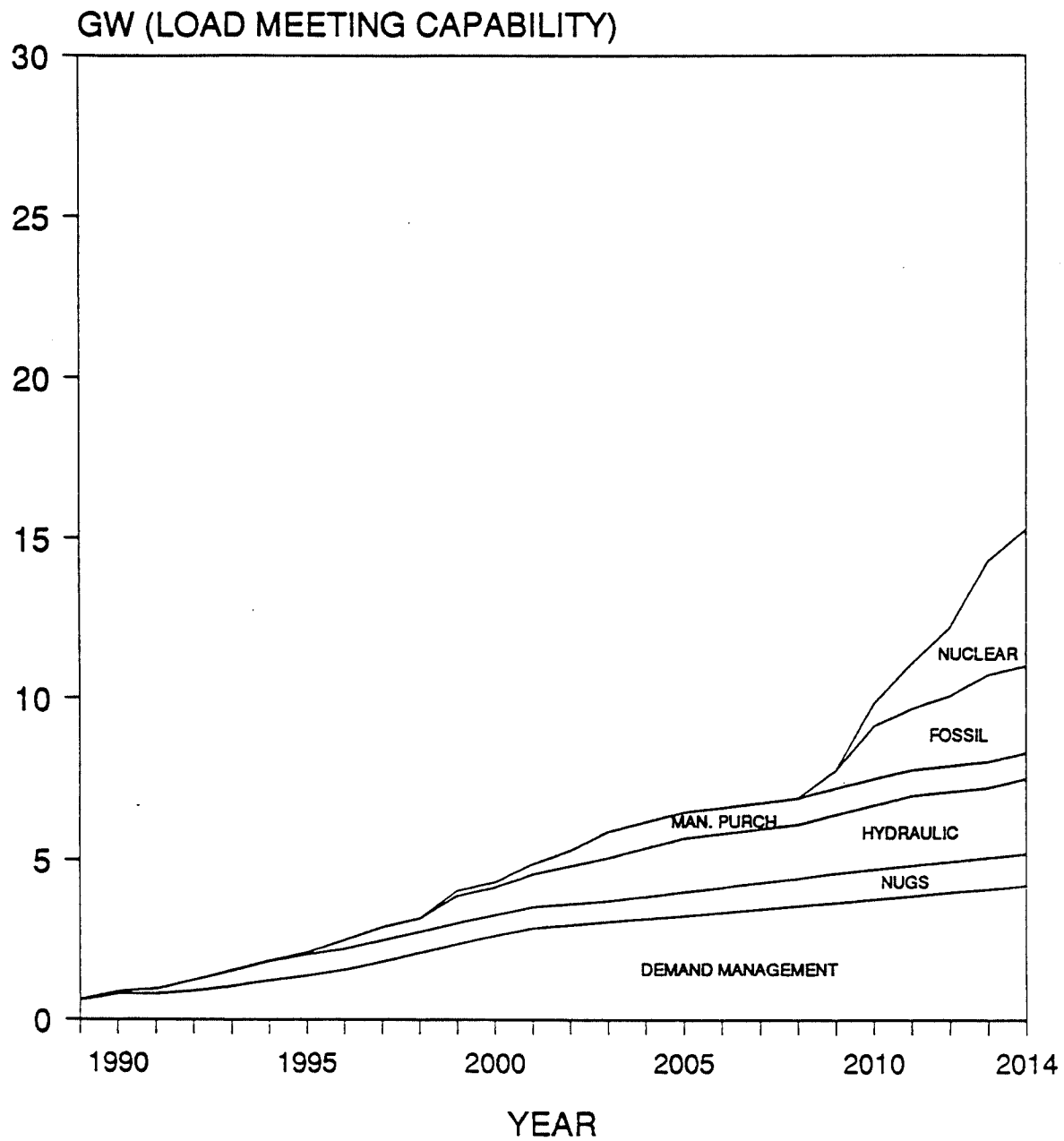


FIGURE 4.17-2
PLAN 15
DATA USED IN ANALYSIS - BRANCH LOWER

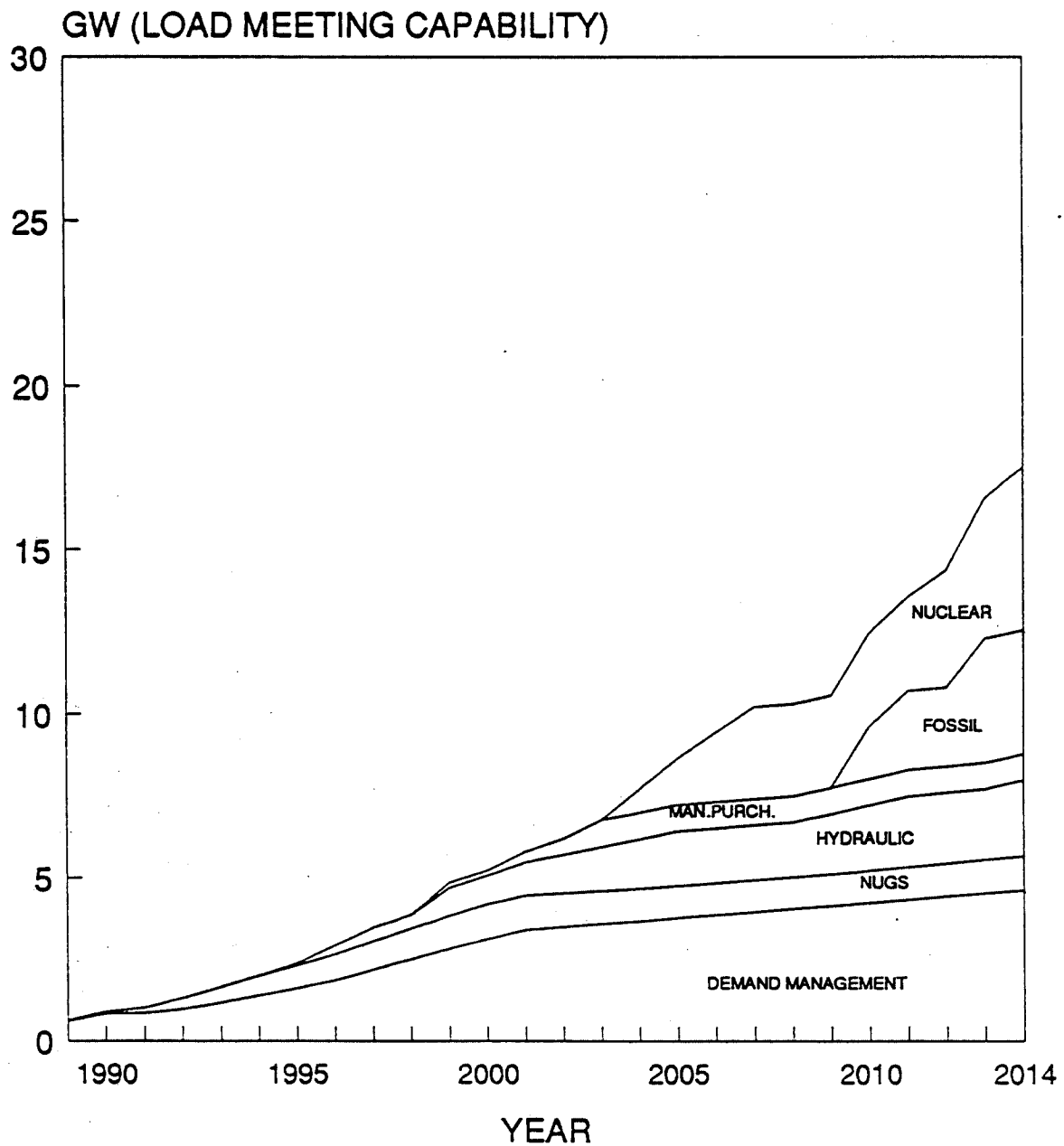


FIGURE 4.17-3
PLAN 15
DATA USED IN ANALYSIS - MEDIAN

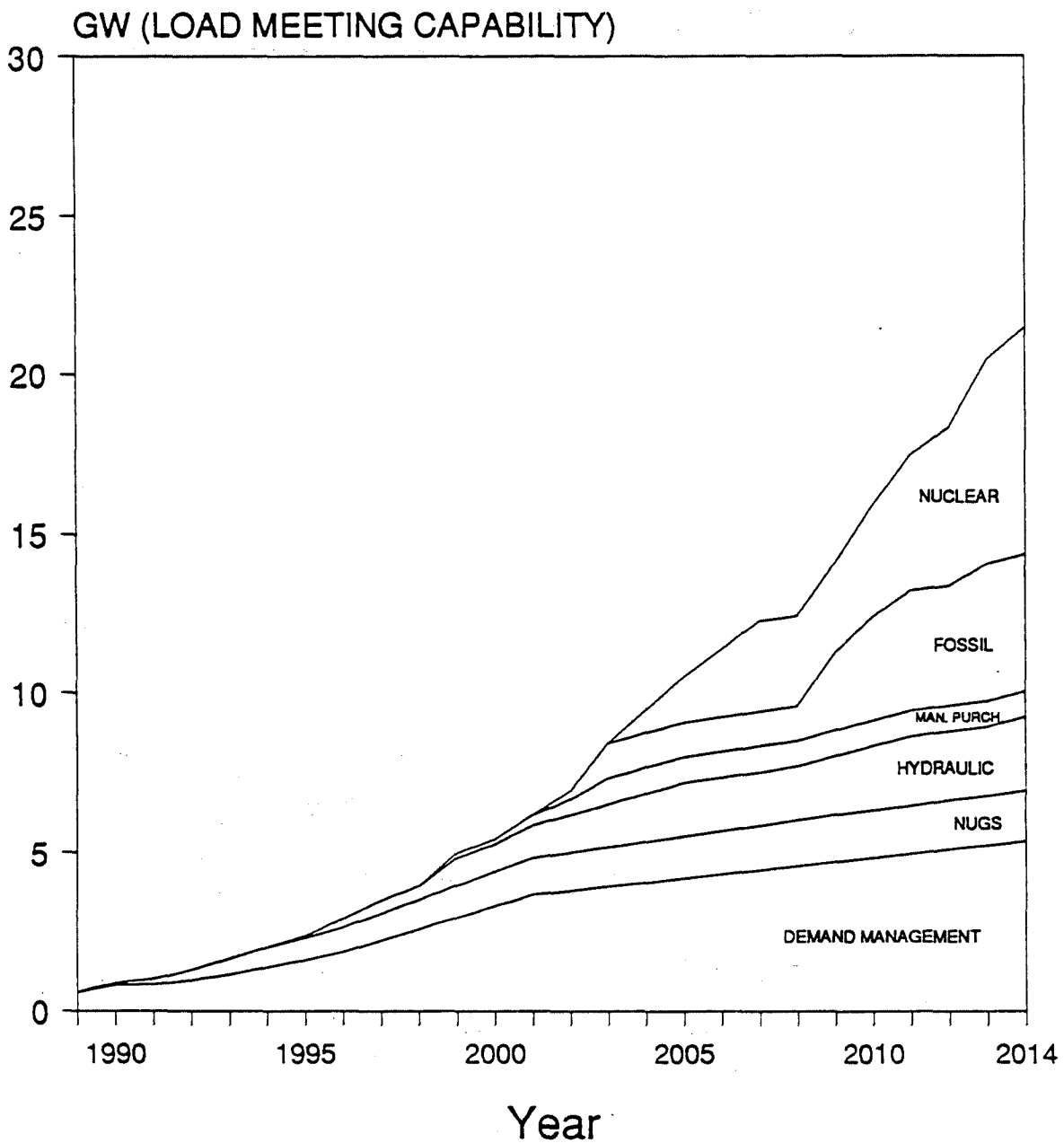


FIGURE 4.17-4
PLAN 15
DATA USED IN ANALYSIS - BRANCH UPPER

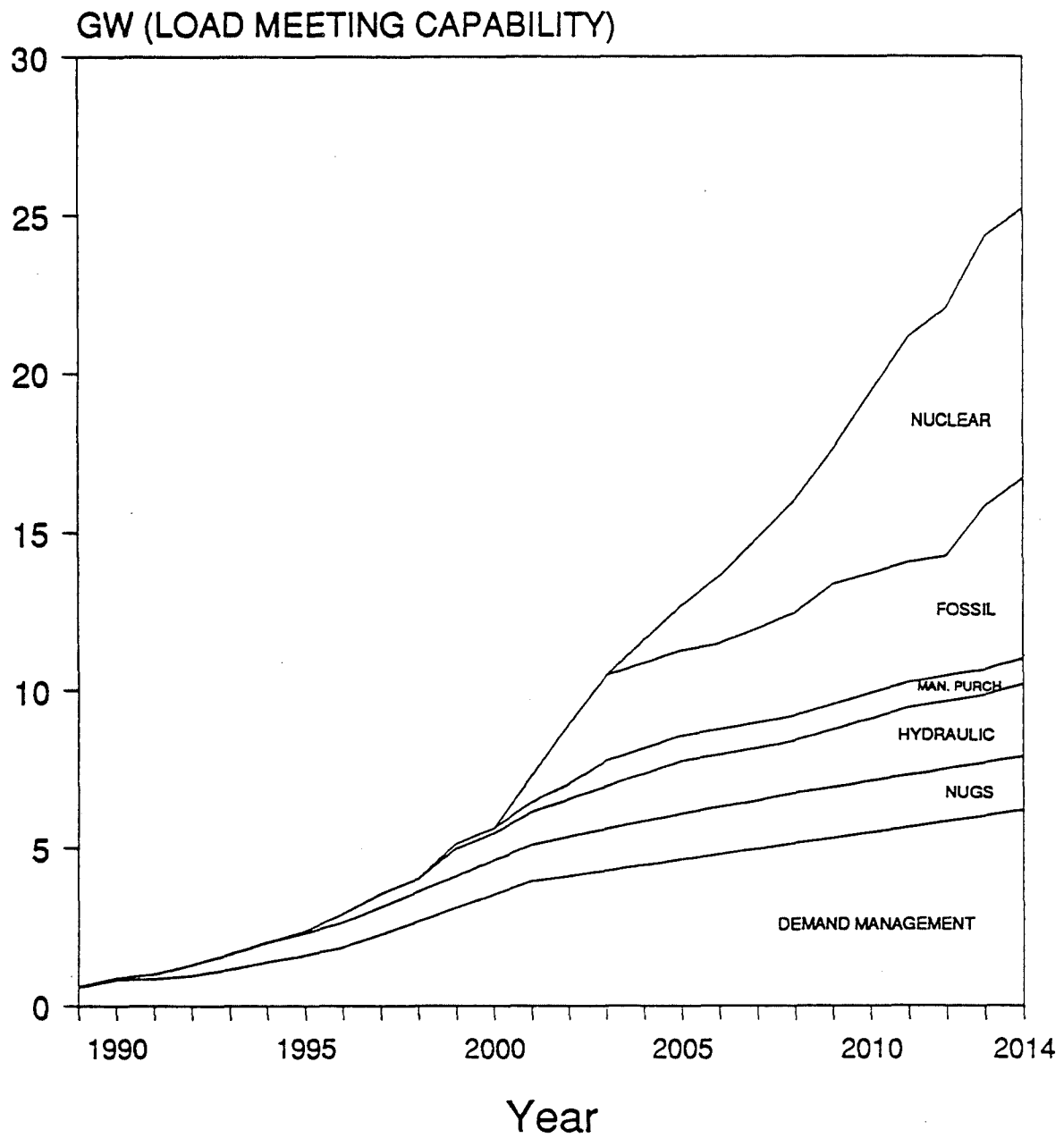


FIGURE 4.17-5
PLAN 15
DATA USED IN ANALYSIS - UPPER

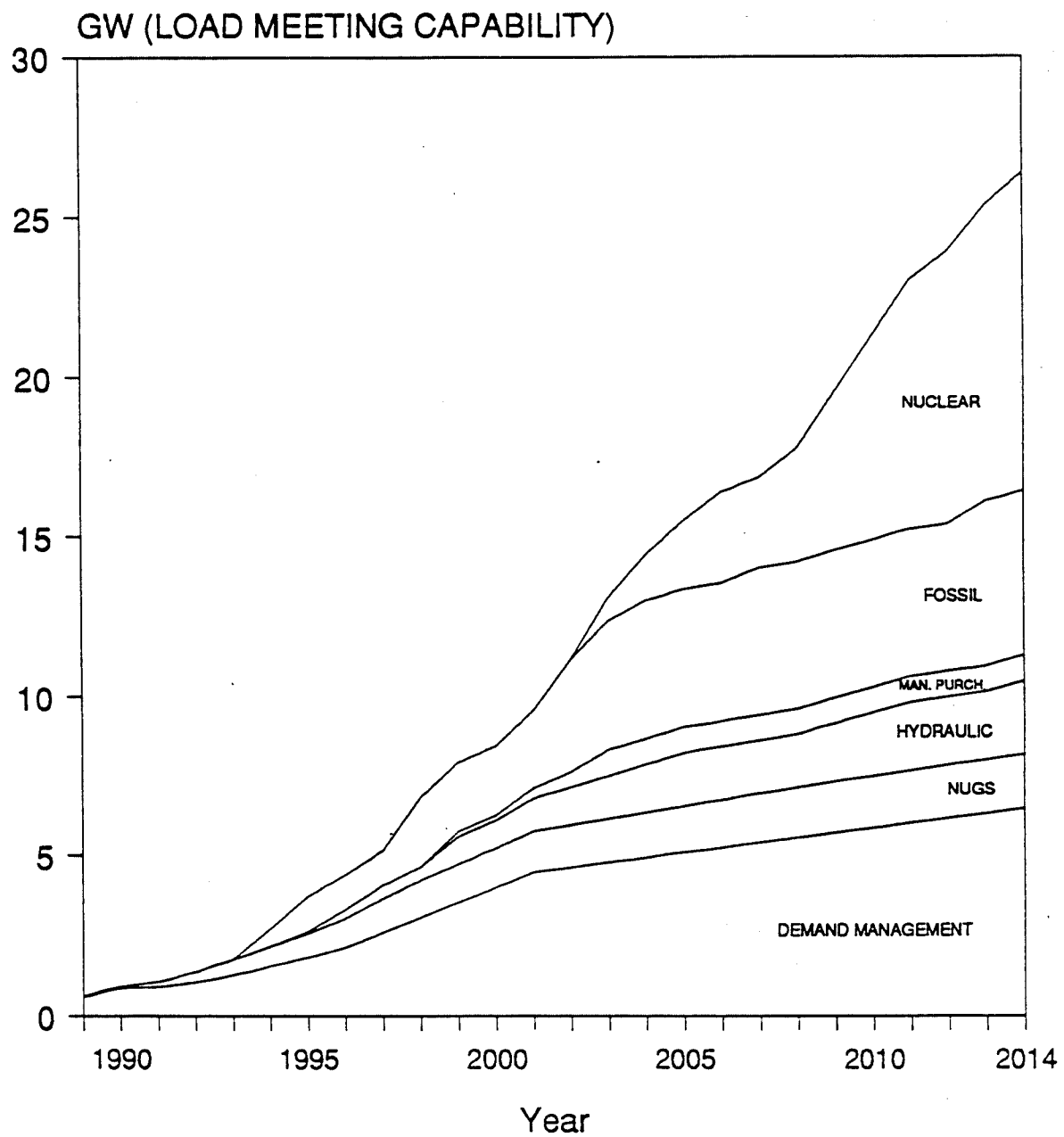


FIGURE 4.17-6
PLAN 22
DATA USED IN ANALYSIS - LOWER

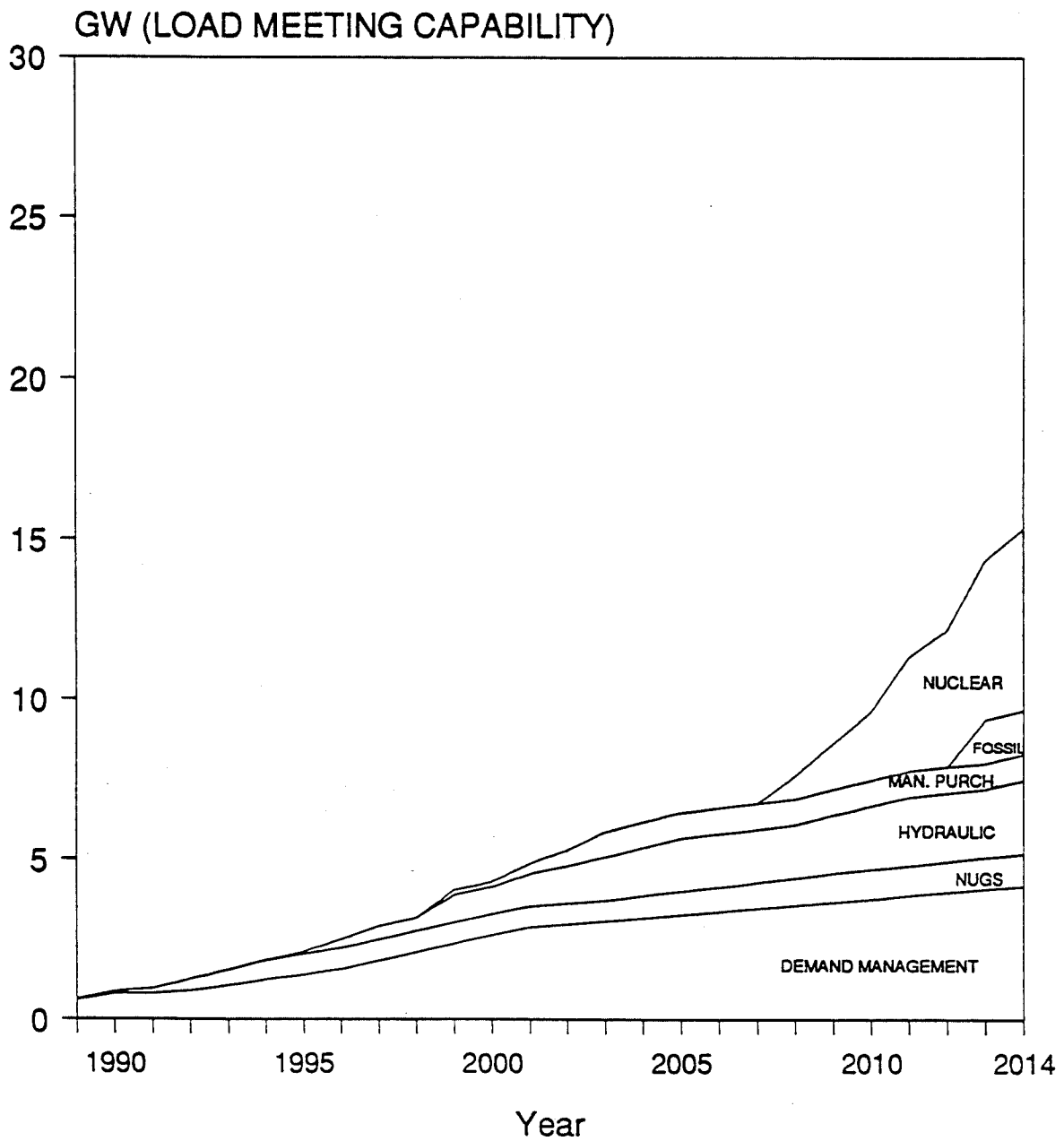


FIGURE 4.17-7
PLAN 22
DATA USED IN ANALYSIS - BRANCH LOWER

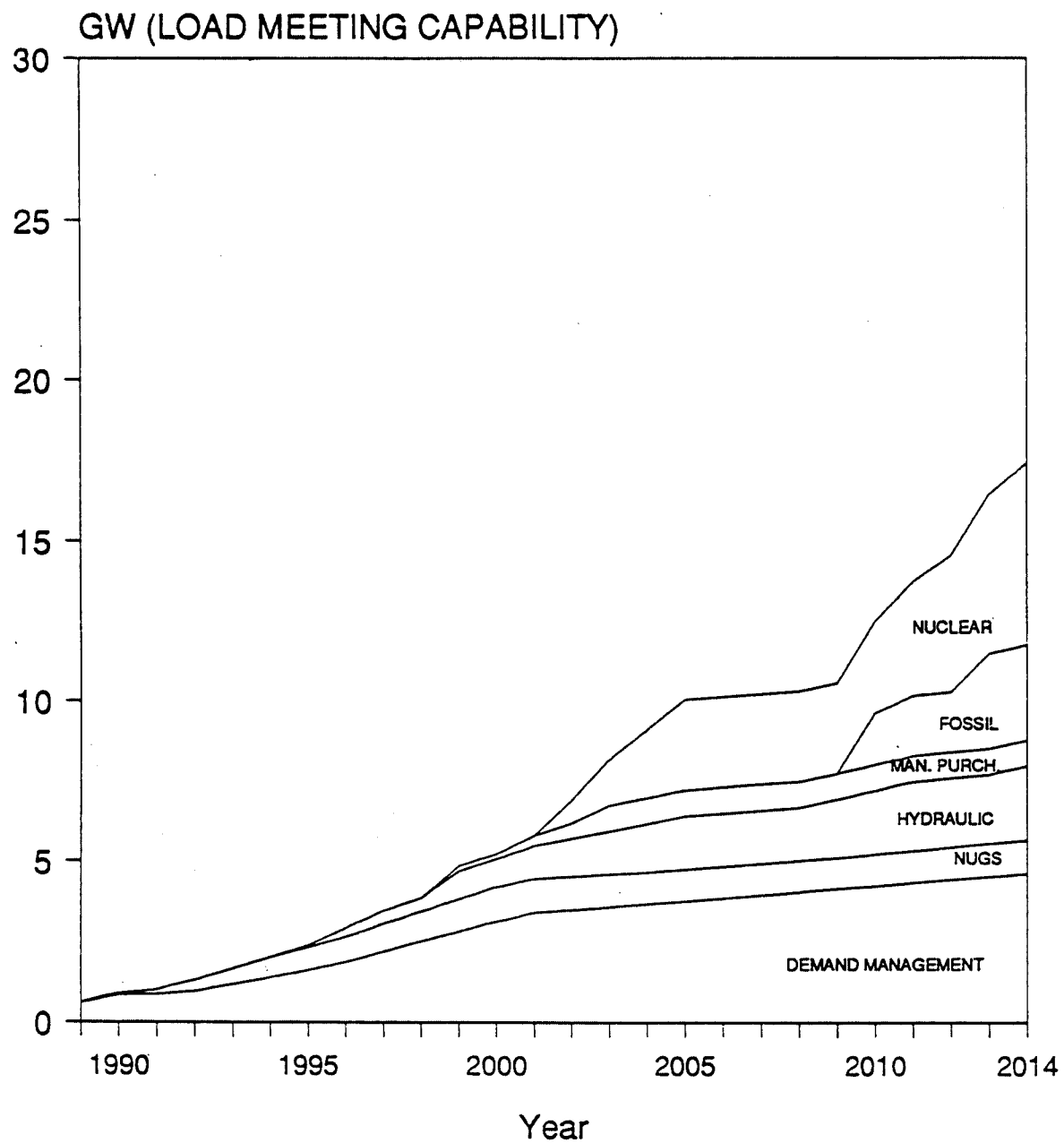


FIGURE 4.17-8
PLAN 22
DATA USED IN ANALYSIS - MEDIAN

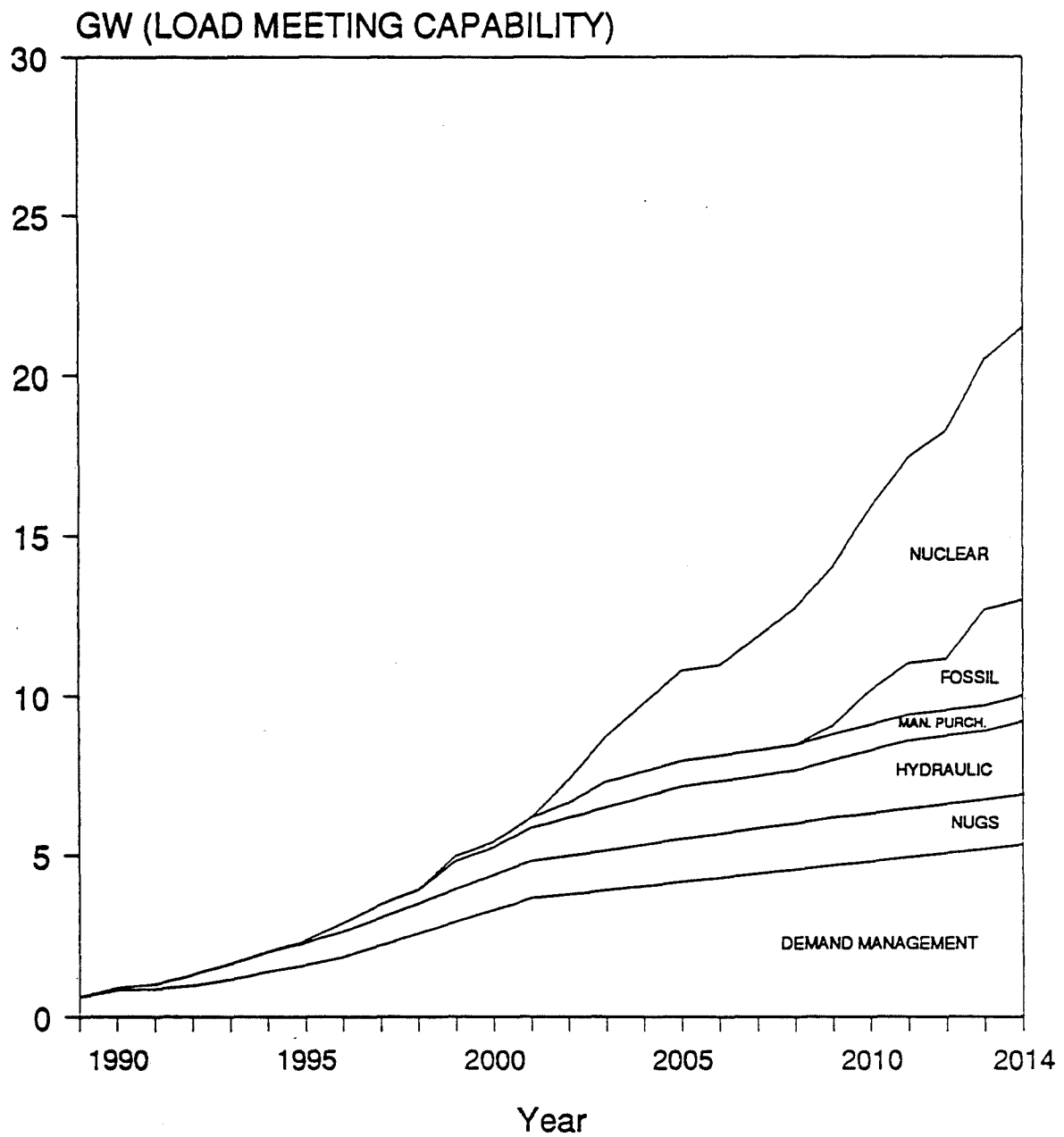


FIGURE 4.17-9
PLAN 22
DATA USED IN ANALYSIS - BRANCH UPPER

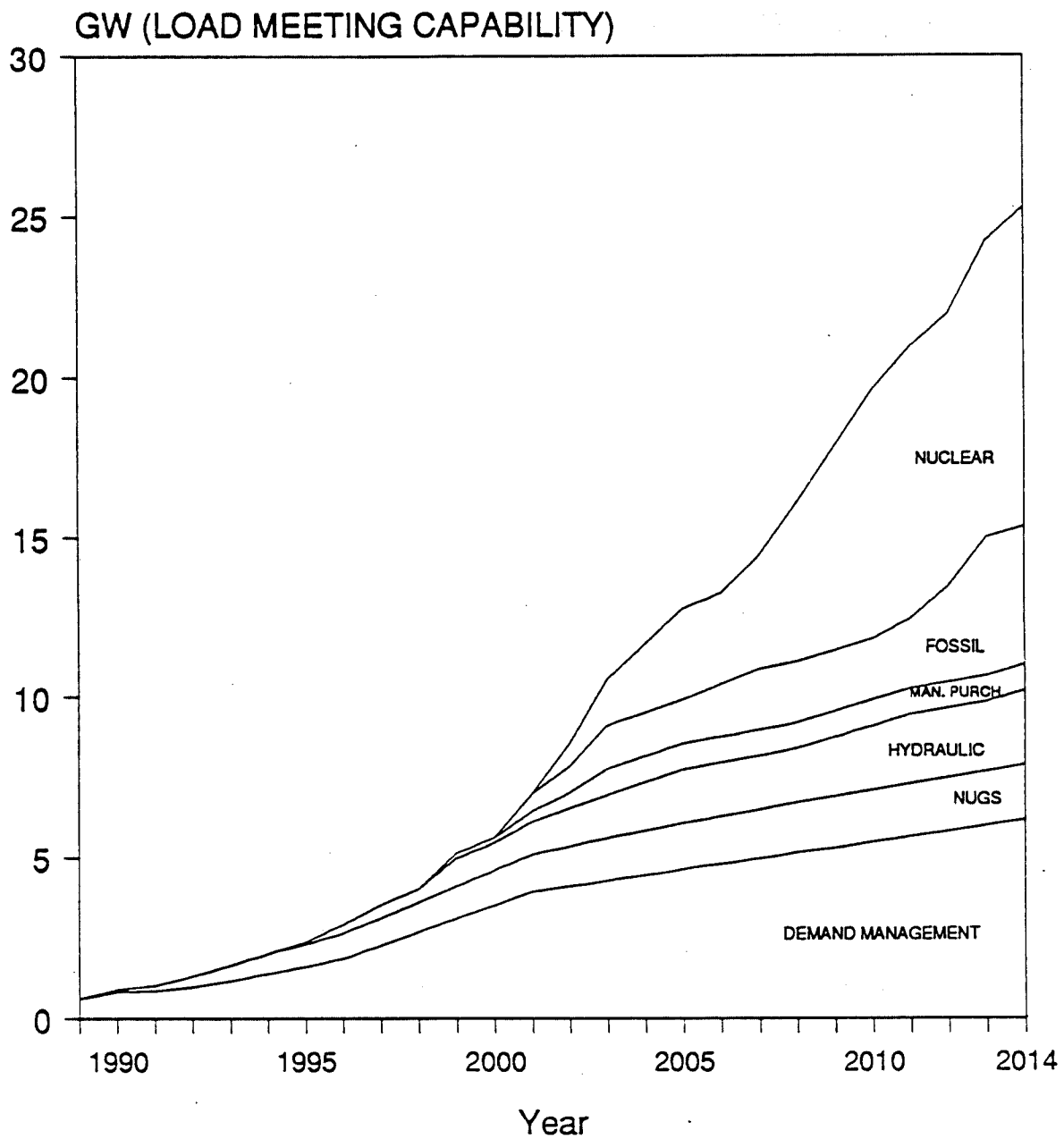


FIGURE 4.17-10
PLAN 22
DATA USED IN ANALYSIS - UPPER

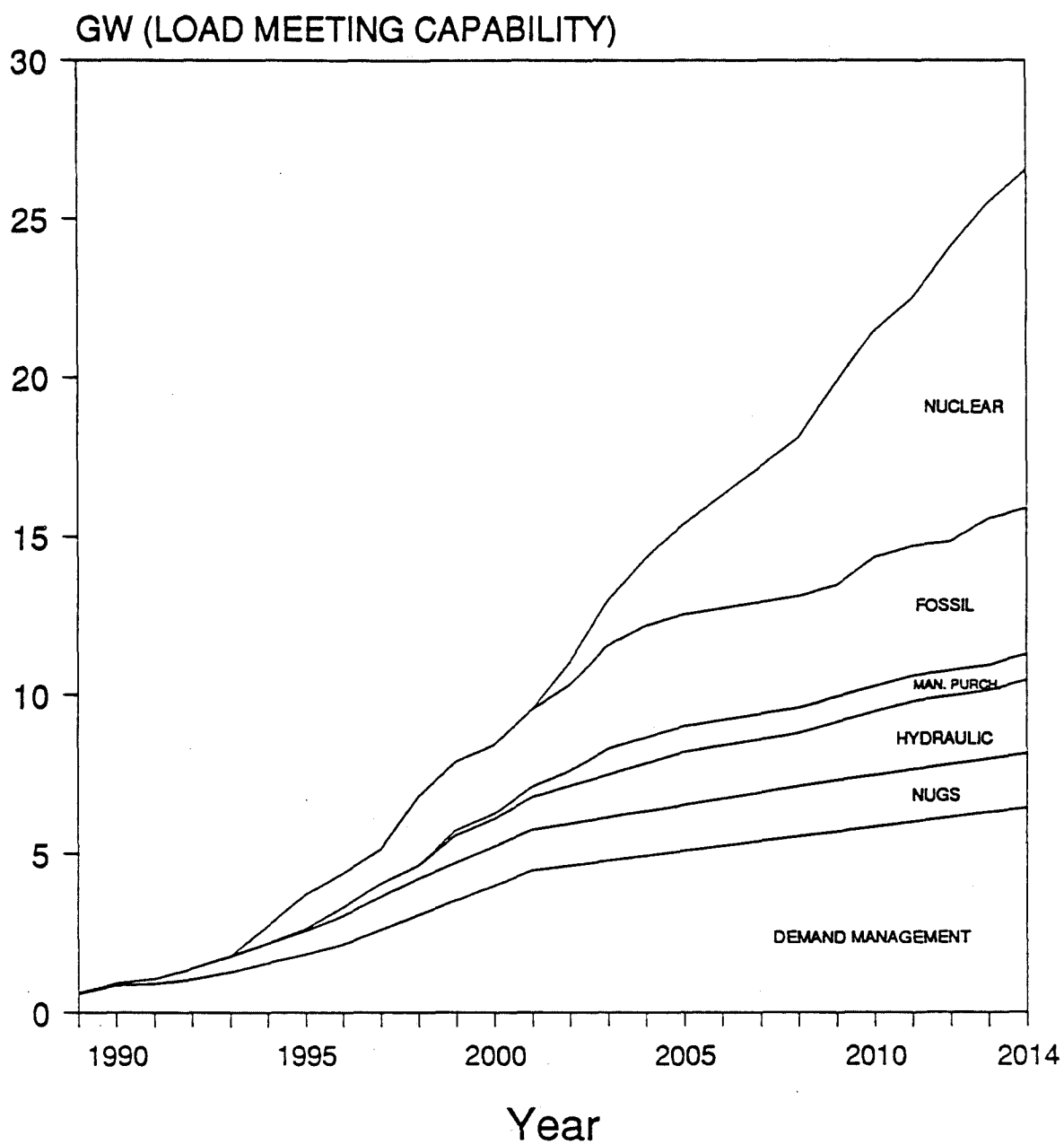


FIGURE 4.17-11
PLAN 24
DATA USED IN ANALYSIS - LOWER

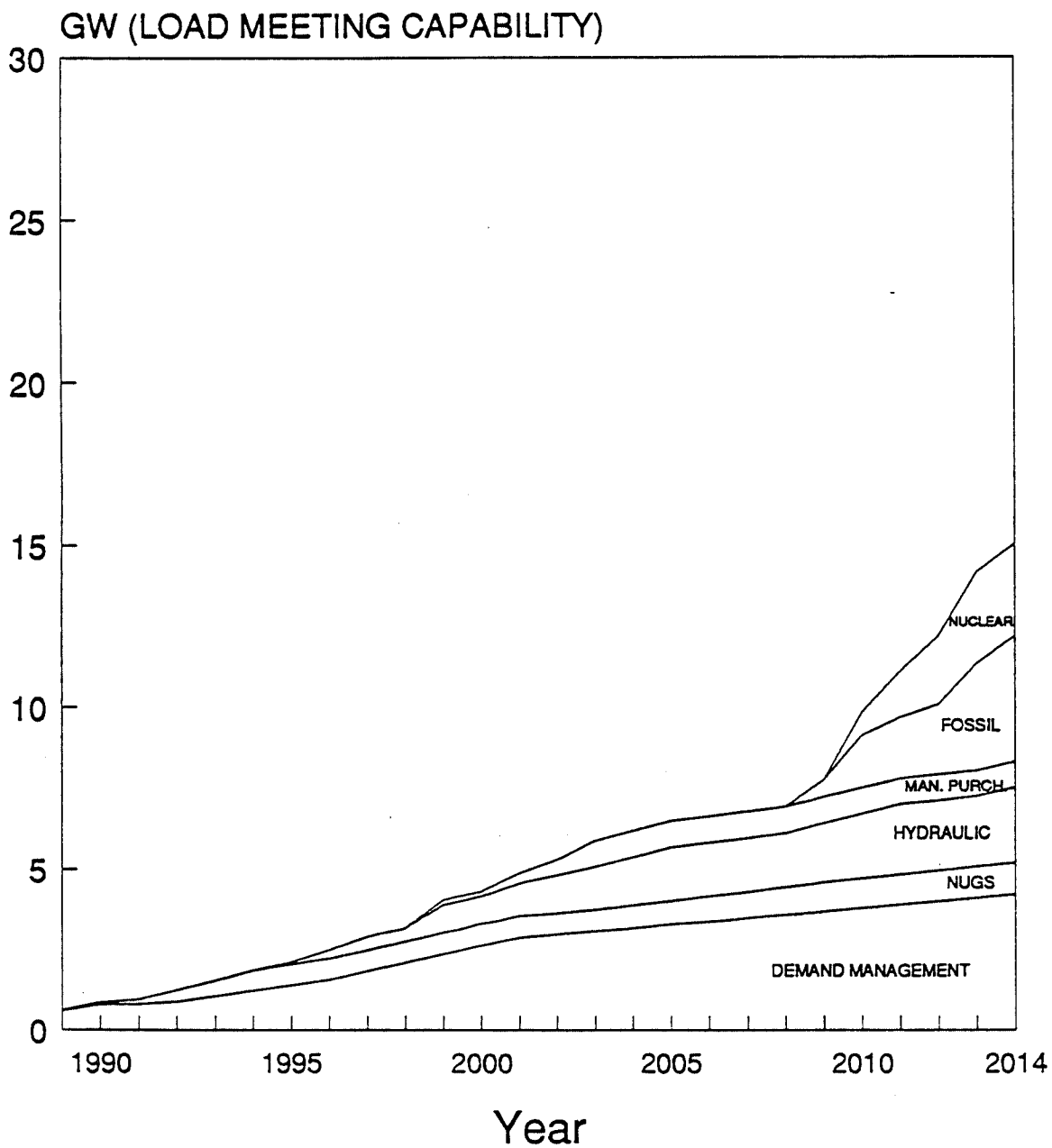


FIGURE 4.17-12
PLAN 24
DATA USED IN ANALYSIS - BRANCH LOWER

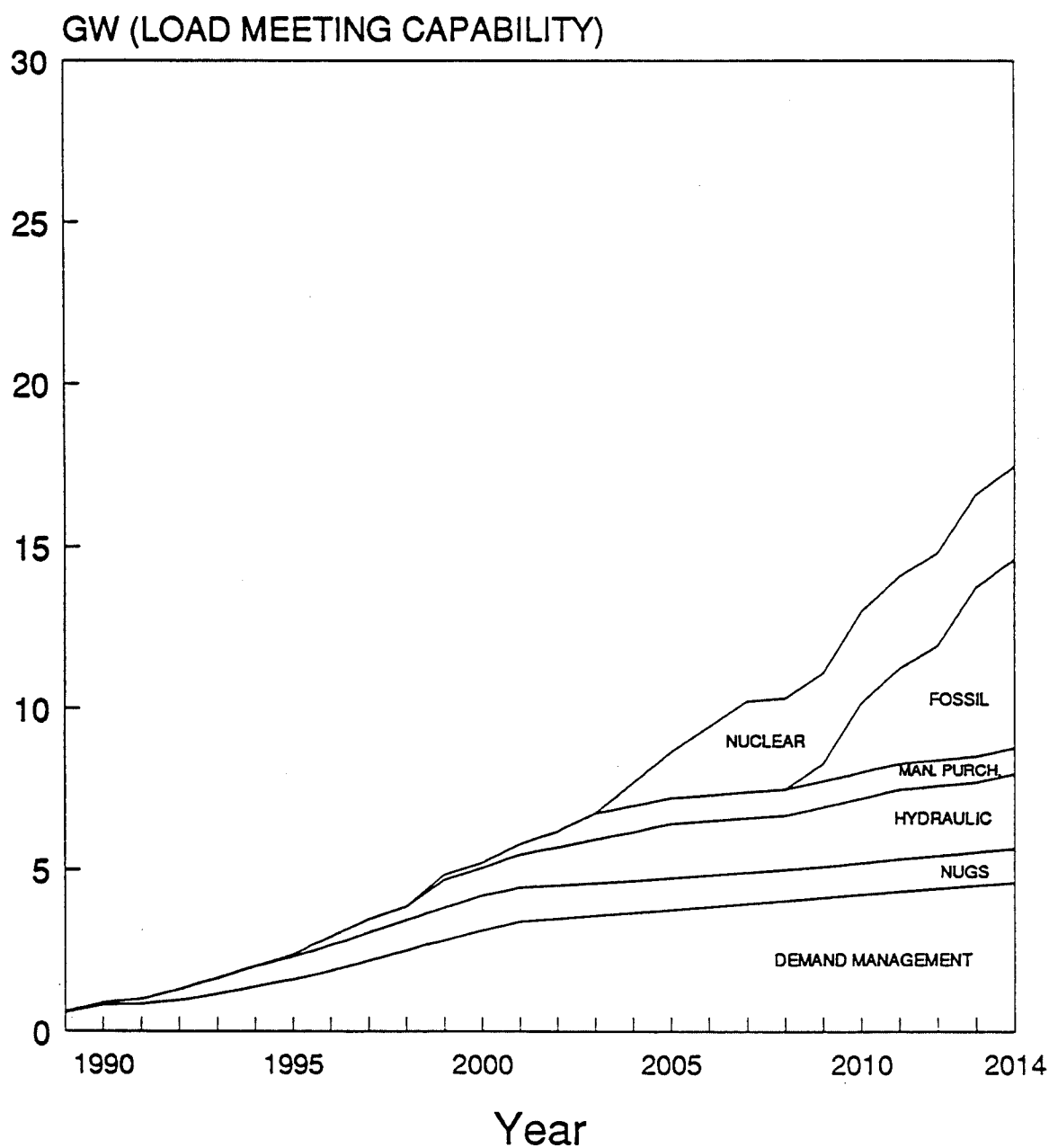


FIGURE 4.17-13
PLAN 24
DATA USED IN ANALYSIS - MEDIAN

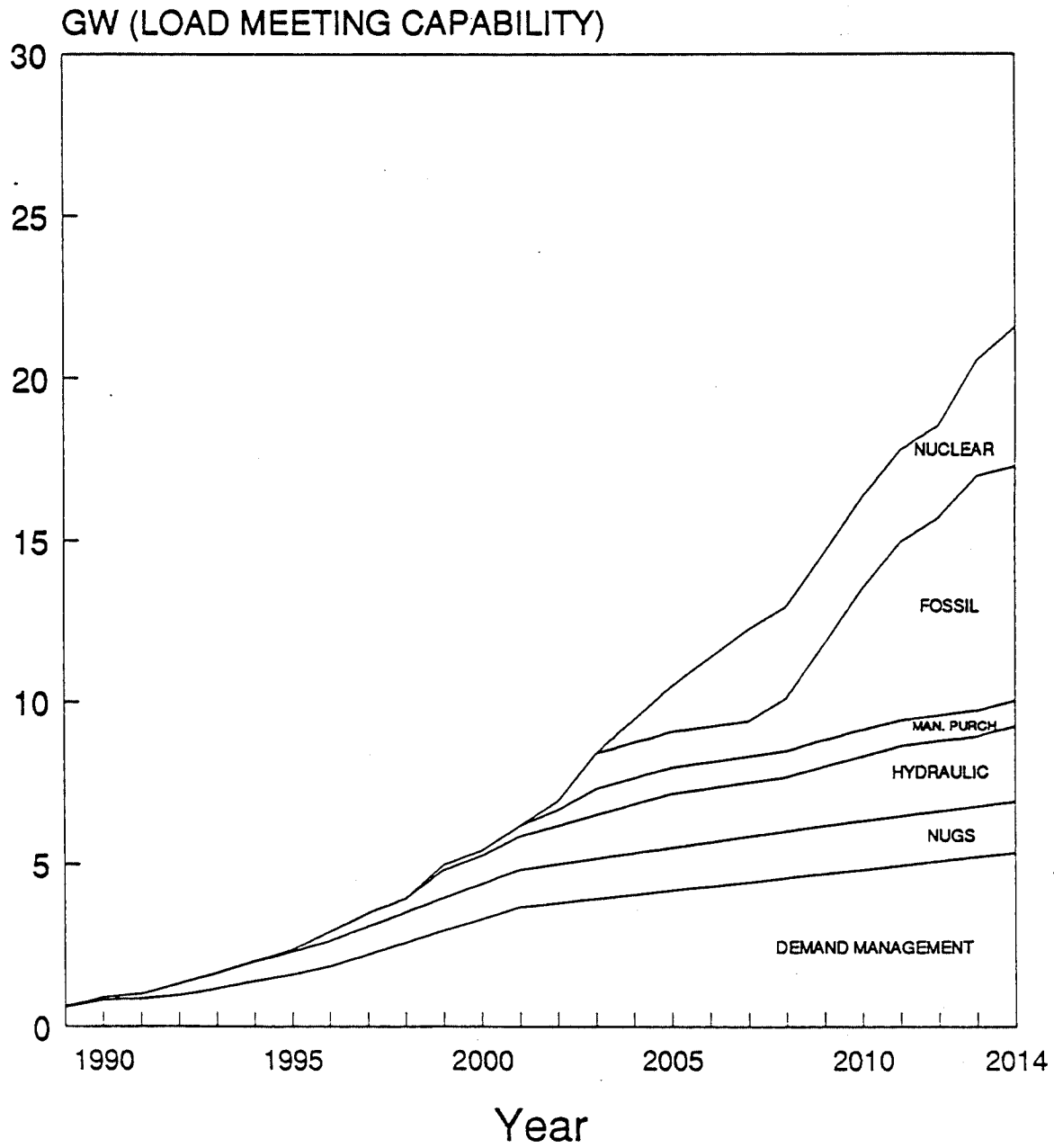


FIGURE 4.17-14
PLAN 24
DATA USED IN ANALYSIS - BRANCH UPPER

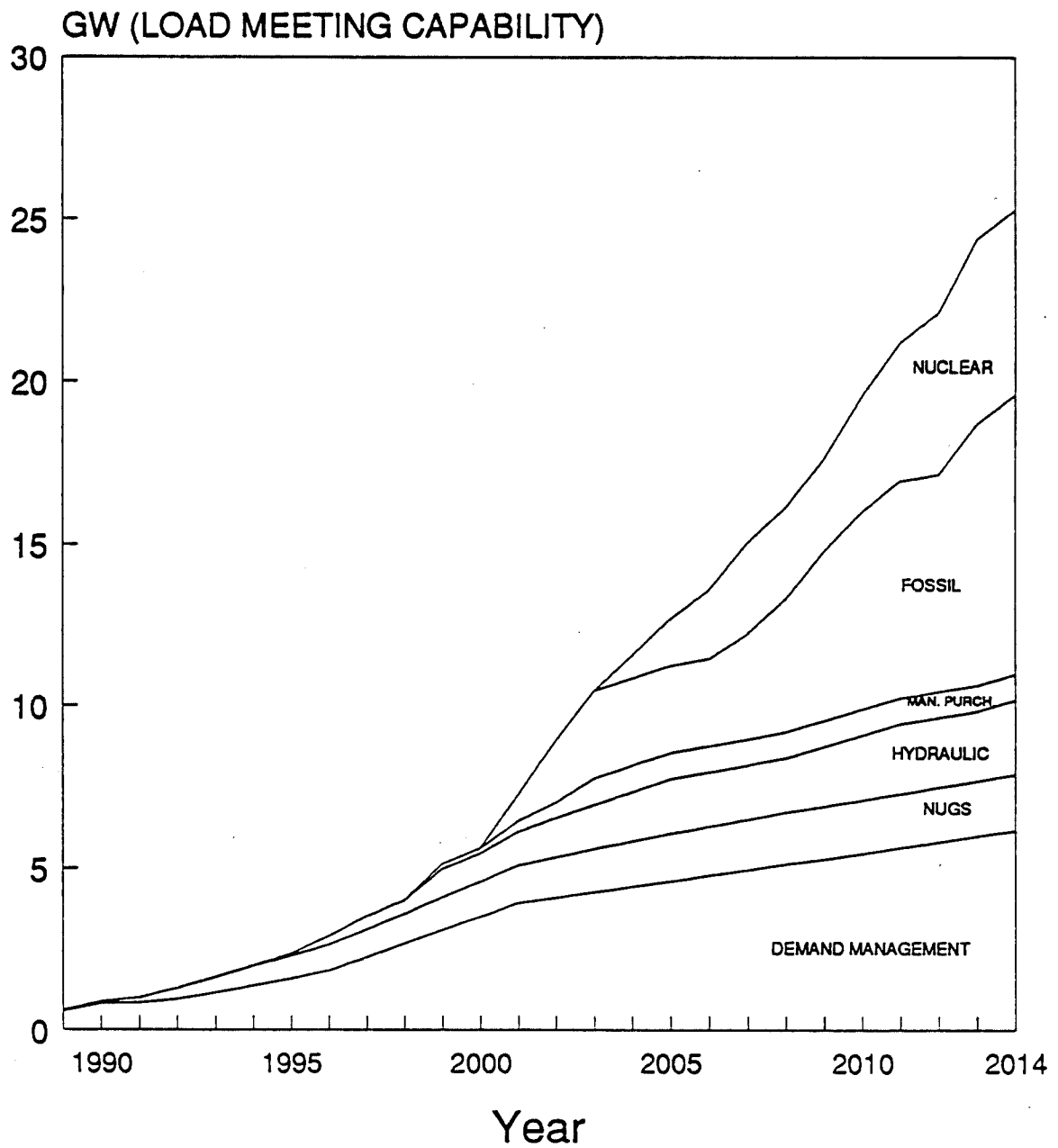
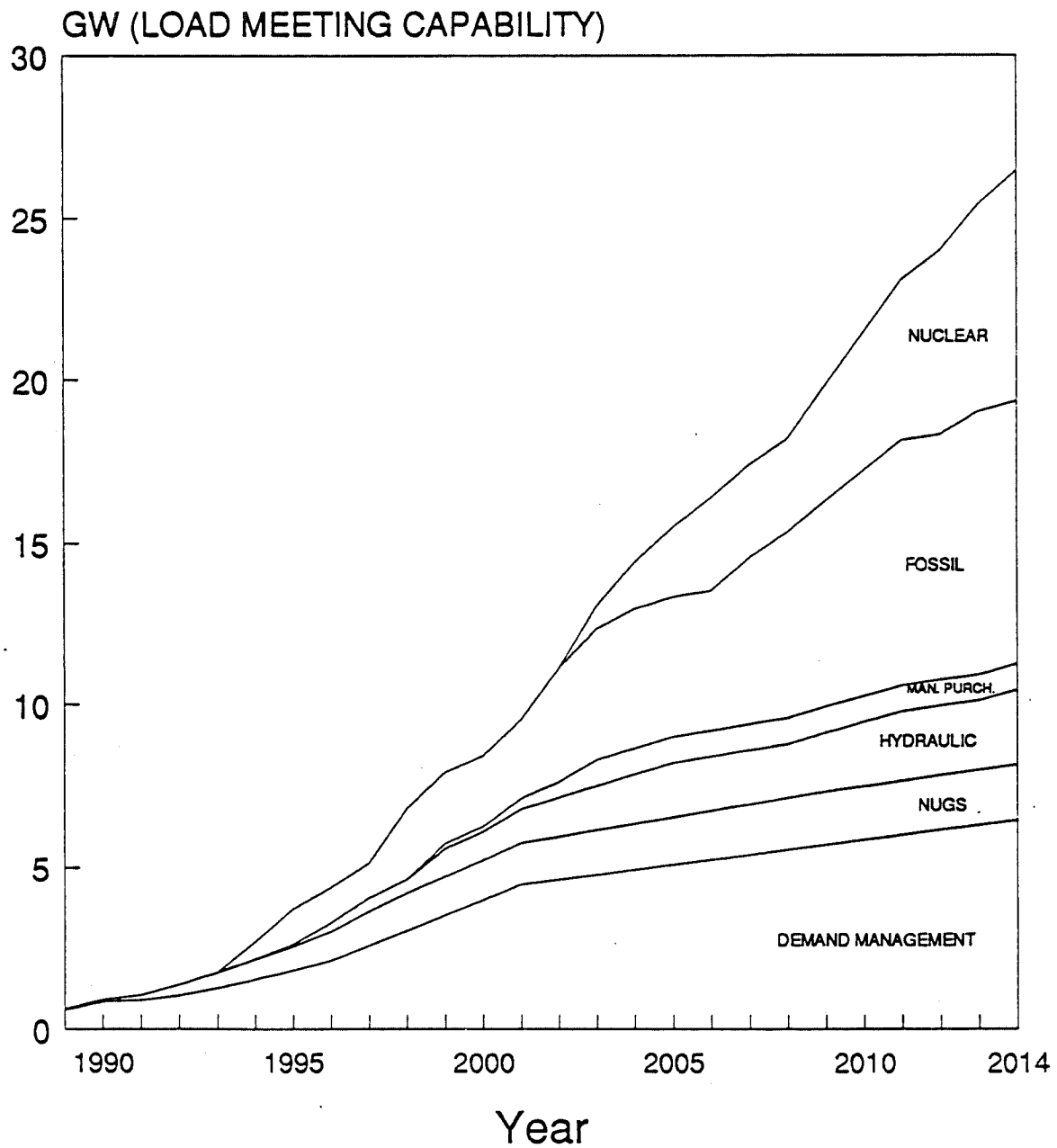


FIGURE 4.17-15
PLAN 24
DATA USED IN ANALYSIS - UPPER



4.19 APPROVALS

Refer to Chapter 19 of the Plan Report for a detailed description of the approvals which Ontario Hydro is seeking with respect to the Candidate Demand/Supply Plans.

4.20 REVIEW

The formulation of demand/supply cases began with the Basic Load Forecast and a projection of the load meeting capability of the existing system. In situations where the basic forecast exceeded the existing system's load meeting capability (LMC), the priority demand reducing options were turned to first. These options are economic electrical efficiency improvements, load shifting, demand displacement non-utility generators, and customer interruptible loads. The firm load forecast was obtained by subtracting the contributions of the demand reducing options from the basic forecast.

When the firm load forecast exceeded the LMC of the existing system, the priority supply options were then considered. These options are the economic purchase NUGs and remaining potential hydraulic developments within the province. If this was not sufficient to meet the forecast demand, it was then necessary to plan for the addition of new major supply options.

Combinations of the major supply options (utility purchases, CANDU nuclear generation, and fossil fired generation) were formulated into demand/supply cases. These cases were evaluated, modified and refined in the planning process. Dozens of cases were considered and, from these, five promising Major Supply Cases were identified and carried through for full evaluation and subsequent presentation in the DSP Report.

Demand/supply plans were developed for the five load forecast paths (Median, Branch Upper, Upper, Branch Lower and Lower) which cover the bandwidth of the load forecast. This chapter provided details on the formulation and description of the demand/supply cases, particularly for the branch load forecast paths. The Branch Upper and Branch Lower load paths provide a means to evaluate the way in which the cases respond to changes in demand.

All cases formulated had common Demand Management, Non-Utility Generation, Rehabilitation and Hydraulic Plans. Differences between demand/supply cases arose

from differences between the timing and amount of the various options used to meet the need for new major supply after the common elements were considered. Major supply options considered included Candu nuclear, CTU, CTU/CC, CTU/IGCC, and CSC-Coal. All of the Major Supply Cases presented in the Plan Report have the Manitoba Purchase in common.

This chapter also identified some differences between the data that was used when demand/supply cases were developed and the data presented in the Plan Report. The differences between data are small and would not significantly change the nature of the cases or the results of the evaluations.

APPENDIX

This Appendix contains tables which summarize the components of the Proposed Plan and the two Alternative Plans for the Upper, Median, and Lower load forecast paths. One table is provided for each plan and each load forecast path with needs, expected demand reduction, and new supply additions expressed in terms of capacity. These are followed by similar tables expressed in terms of load meeting capability. The data in these tables describe in detail the Plans as presented in the Plan Report. Differences between data presented here and that used for demand/supply case formulation and analysis are discussed in Chapter 4 of this Analysis Report.

**DEMAND / SUPPLY BALANCE - PEAK POWER (MW) - SUPPLY ENTERED IN CAPACITY
BASED ON DEMAND/SUPPLY PLAN 13**

OTHER LOAD FORECAST

YEAR (JANUARY)	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	DIST.
EXISTING FIRM LOAD MEETING CAPABILITY	23932	24907	26019	27256	28714	30600	32754	35251	38100	41240	44680	48420	52450	56770	61380	66280	71480	76980	82780	88880	95280	101980	108880	116080	123580	131380	139180
	719	917	1097	1372	1771	2291	2941	3741	4701	5821	7101	8541	10151	11941	13911	16071	18431	21001	23781	26781	30001	33441	37101	41001	45141	49521	
	0	14	34	58	86	118	153	192	235	282	332	385	441	500	562	627	696	769	846	927	1012	1101	1194	1291	1392	1497	
	0	84	186	282	373	458	538	613	683	748	808	863	913	958	1000	1038	1073	1105	1135	1162	1187	1210	1231	1250	1267	1282	
DEMAND/SUPPLY REQUIRED - LDC	719	917	1097	1372	1771	2291	2941	3741	4701	5821	7101	8541	10151	11941	13911	16071	18431	21001	23781	26781	30001	33441	37101	41001	45141	49521	
ELECTRICAL EFFICIENCY IMPROVEMENTS	0	14	34	58	86	118	153	192	235	282	332	385	441	500	562	627	696	769	846	927	1012	1101	1194	1291	1392	1497	
	0	84	186	282	373	458	538	613	683	748	808	863	913	958	1000	1038	1073	1105	1135	1162	1187	1210	1231	1250	1267	1282	
	0	35	90	152	219	284	347	407	464	518	568	614	656	694	728	758	784	807	826	842	856	868	878	886	892	897	
	23932	24907	26019	27256	28714	30600	32754	35251	38100	41240	44680	48420	52450	56770	61380	66280	71480	76980	82780	88880	95280	101980	108880	116080	123580	131380	
PEAKDAY LOAD FORECAST	719	917	1097	1372	1771	2291	2941	3741	4701	5821	7101	8541	10151	11941	13911	16071	18431	21001	23781	26781	30001	33441	37101	41001	45141	49521	
CAPACITY INTERMITTIBLE LOADS	719	917	1097	1372	1771	2291	2941	3741	4701	5821	7101	8541	10151	11941	13911	16071	18431	21001	23781	26781	30001	33441	37101	41001	45141	49521	
FIRM LOAD FORECAST	23217	23996	25037	26466	28202	30266	32566	35106	37886	40916	44206	47746	51546	55616	59956	64566	69456	74626	80076	85806	91826	98146	104766	111586	118806	126426	
SUPPLY REQUIRED - LDC	14	26	55	93	130	167	203	239	275	311	347	383	419	455	491	527	563	599	635	671	707	743	779	815	851	887	
SUPPLY REQUIRED - CAPACITY	17	31	1214	1886	1065	2921	3788	4835	6114	7572	9211	11031	13041	15251	17661	20271	23081	26091	29301	32811	36521	40431	44541	48851	53361	58071	
NUCLEAR RUCS CAPACITY	0	20	35	52	71	91	112	134	157	181	205	229	253	277	301	325	349	373	397	421	445	469	493	517	541	565	
BIODIESEL FIRM CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
NUCLEAR SUPPLY REQUIRED - CAPACITY	17	4	1179	1460	720	2309	3221	4307	5460	6680	7960	9290	10670	12100	13580	15110	16690	18320	19990	21710	23480	25300	27170	29090	31060	33080	
NUCLEAR PURCHASE CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
NEW FOSSIL CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
NEW NUCLEAR CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
NEW NUCLEAR SUPPLY CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

LOWER LOAD FORECAST

OPENING / SUPPLY BALANCE - PLAN FORM (MW) - SUPPLY SUPPLEMENTED IN CAPACITY
 PROJECTED DEMAND/SUPPLY PLAN IS

	TOTAL (JANUARY)																										
	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015
BASIC LOAD FORECAST	22450	22463	22716	22214	22403	22723	22921	24139	24212	24710	25104	25723	26794	27390	28171	28661	29430	29972	30677	30677	30677	30677	30677	30677	30677	30677	30677
EXISTING FIRM LOAD NETTING CAPABILITY	23313	23910	24062	23764	23543	23510	23510	24131	24210	25310	25712	26792	26922	28092	28286	29064	32305	24359	22928	21404	20542	20226	20226	20226	20226	20226	20226
DEMAND/SUPPLY REQUIRED - LMC	0	0	0	0	0	0	0	0	0	0	0	0	302	1981	2955	2617	2623	2768	3012	6158	7841	9733	12173	14410	15023		
ELECTRICAL EFFICIENCY IMPROVEMENTS	0	14	36	62	101	146	231	400	610	900	1120	1360	1600	1840	2080	2320	2560	2800	3040	3280	3520	3760	4000	4240	4480	4720	4960
LOAD SHEDDING	0	78	161	246	331	519	576	610	643	707	749	750	800	820	840	860	900	910	910	910	910	910	910	910	910	910	910
DEFERRABLE LOAD DISPLACEMENT MISC	0	51	78	172	279	206	210	242	242	241	242	242	242	242	242	242	246	250	252	257	260	264	268	271	275	278	282
PAYMENT LOAD FORECAST	22450	22716	22712	22714	22716	22716	22716	23023	23567	23701	23707	23723	23723	24023	24623	25461	25534	25810	26226	26782	27347	27723	28029	28220	28315	28462	28621
CAPACITY UTILIZABLE LOADS	723	709	599	582	586	556	526	546	546	572	580	587	599	607	616	625	633	642	653	668	682	697	713	727	742	756	771
FIRM LOAD FORECAST	21455	21607	21812	22151	22510	22700	22786	22772	23001	23208	23213	23464	23733	24016	24460	25046	24721	25167	25669	26094	26545	27033	27548	28080	28453	28796	29104
SUPPLY REQUIRED - LMC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1110	2135	3729	5518	7461	9394	10417		
SUPPLY REQUIRED - CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1276	2672	4656	6596	8520	10229	12219	13917	
POWERSHIP MISC CAPACITY	0	20	35	226	212	210	435	435	435	435	435	435	435	435	435	435	435	435	435	435	435	435	435	435	435	435	435
HYDROELECTRIC FIRM CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
MAJOR SUPPLY REQUIRED - CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
POWERSHIP FORECAST CAPACITY	0	0	0	0	0	0	0	0	0	0	200	200	200	400	600	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000
NEW FOSIL CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW NUCLEAR CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW MAJOR SUPPLY CAPACITY	0	0	0	0	0	0	0	0	0	0	200	200	400	600	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000

DEMAND / SUPPLY BALANCE - YEAR 2014 (MW) - SUPPLY EXPANDED IN CAPACITY
CANDIDATE DEMAND/SUPPLY PLAN 22 (BROWN NUCLEAR)

MEDIUM LOAD FORECAST

YEAR (JANUARY)	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	DEC.
BASIC LOAD FORECAST	23156	23089	23433	23403	23403	23403	23403	23403	23403	23403	23403	23403	23403	23403	23403	23403	
EXISTING FIRM LOAD MEETING CAPABILITY	23213	23310	23403	23403	23403	23403	23403	23403	23403	23403	23403	23403	23403	23403	23403	23403	
DEMAND/SUPPLY REQUIRED - LDC	0	0	471	679	0	1376	3033	1940	3542	4192	4735	5019	6140	7422	8446	9406	
ELECTRICAL EFFICIENCY IMPROVEMENTS	0	14	43	70	116	123	214	300	400	500	600	700	800	900	1000	1100	
LOAD SHEDDING	0	61	171	264	433	592	656	717	776	836	895	946	1000	1040	1080	1120	
DEPENDABLE LOAD DISPLACEMENT RUCS	0	39	102	176	242	310	374	439	503	567	631	695	759	823	887	951	
PEAK LOAD FORECAST	23156	23433	23403	23403	23403	23403	23403	23403	23403	23403	23403	23403	23403	23403	23403	23403	
CAPACITY INTERPOLATED LOADS	725	725	612	612	612	612	612	612	612	612	612	612	612	612	612	612	
FIRM LOAD FORECAST	23156	23310	23310	23310	23310	23310	23310	23310	23310	23310	23310	23310	23310	23310	23310	23310	
SUPPLY REQUIRED - LDC	0	0	0	0	0	0	97	0	0	0	0	0	0	0	0	0	
SUPPLY REQUIRED - CAPACITY	0	0	0	0	0	0	120	0	0	0	0	0	0	0	0	0	
PURCHASE RUCS CAPACITY	0	28	33	216	212	210	471	344	416	481	551	621	691	761	831	901	
HYDROLOGIC FIRM CAPACITY	0	0	0	0	0	0	15	0	0	0	0	0	0	0	0	0	
MAJOR SUPPLY REQUIRED - CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
MAINTENANCE PURCHASE CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
NEW THERMAL CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
NEW NUCLEAR CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
NEW MAJOR SUPPLY CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

[illegible]

DEMAND / SUPPLY BALANCE - PEAK POWER (MW) - SUPPLY EXPRESSED IN CAPACITY
CANDIDATE DEMAND/SUPPLY PLAN 22 (BIGLER NUCLEAR)

LOWER LOAD FORECAST	YEAR (JANUARY)												DEC.													
	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
BASIC LOAD FORECAST	22460	22463	22766	23214	23403	23733	23921	24153	24312	24710	25104	25732	26594	27759	28771	28661	28420	28392	28371	28097	27667	27229	26892	26469	25960	25312
EXISTING FIRM LOAD INCLUDING CAPABILITY	22312	21970	21662	21364	21043	20710	20350	20011	19691	19300	18844	18324	17754	17134	16464	15754	15004	14224	13424	12604	11764	10914	10054	9184	8304	7414
DEMAND/SUPPLY REQUIRED - LNC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
ELECTRICAL EFFICIENCY IMPROVEMENTS	0	14	36	62	101	146	231	400	640	980	1320	1660	2000	2340	2680	2820	2960	3100	3240	3380	3520	3660	3800	3940	4080	4220
LOAD SHIFTING	0	78	141	246	367	519	716	950	1210	1490	1790	2110	2450	2810	3190	3590	3990	4390	4790	5190	5590	5990	6390	6790	7190	7590
DEFERRABLE LOAD DISPLACEMENT RUCS	0	33	59	172	219	266	330	342	342	342	342	342	342	342	342	342	342	342	342	342	342	342	342	342	342	342
PRIMARY LOAD FORECAST	22460	22316	22471	22726	23056	23356	23704	24032	24341	24701	25031	25331	25631	25931	26231	26531	26831	27131	27431	27731	28031	28331	28631	28931	29231	29531
CAPACITY INTERAVAILABLE LOADS	215	709	339	583	846	1124	1416	1716	2016	2316	2616	2916	3216	3516	3816	4116	4416	4716	5016	5316	5616	5916	6216	6516	6816	7116
FIRM LOAD FORECAST	22665	22407	22807	23309	23809	24309	24809	25309	25809	26309	26809	27309	27809	28309	28809	29309	29809	30309	30809	31309	31809	32309	32809	33309	33809	34309
SUPPLY REQUIRED - LNC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
SUPPLY REQUIRED - CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
FORECAST RUCS CAPACITY	0	20	33	226	312	318	435	435	435	435	435	435	435	435	435	435	435	435	435	435	435	435	435	435	435	435
HYDRAULIC FIRM CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
MAJOR SUPPLY REQUIRED - CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
MONITORA FURCHASE CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW FOSIIL CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW NUCLEAR CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW MAJOR SUPPLY CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

DEMAND / SUPPLY BALANCE - PEAK PERIOD (PM) - SUPPLY EXPANDED IN CAPACITY
 CAPACITIES DEMAND/SUPPLY PLAN 35 (ORIGINAL FORECAST)

PEAK LOAD FORECAST		1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015
DEMAND / SUPPLY REQUIRED - LMC		0	0	411	619	0	1214	2033	1846	2541	4189	4725	5019	6160	7322	6844	9466	9632	10135	11333	12504	14149	16033	17431	18468	20714	21323	2400
ELECTRICAL EFFICIENCY IMPROVEMENTS		0	14	43	70	136	183	314	508	608	1108	1400	1700	2000	2100	2208	2300	2400	2500	2600	2700	2800	2900	3000	3100	3200	3300	3400
LOAD SHEDDING		0	0	171	266	423	582	656	717	776	826	873	946	1000	1020	1040	1060	1100	1120	1150	1180	1200	1220	1240	1260	1280	1300	1320
DIFFERENTIAL LOAD DISPLACEMENT RUCS		0	39	102	176	249	310	336	339	332	284	291	292	403	403	411	414	418	422	426	430	433	437	441	445	449	453	456
PEAK LOAD FORECAST		23136	23133	24113	24943	25463	25809	26233	26744	27089	27513	28032	28649	29164	29339	29342	29336	29319	29142	28713	27582	25996	23912	21479	18935	16400	14000	11600
CAPACITY AVAILABLE FROM LOADS		735	735	632	435	421	422	622	641	632	644	632	646	676	702	712	724	727	749	762	775	788	802	816	830	844	859	874
PEAK LOAD FORECAST		23431	23910	23583	24318	24882	25186	25401	25882	26091	26439	26831	27285	27841	28032	28013	28019	28030	28036	28091	28163	28263	28383	28503	28623	28743	28863	28983
SUPPLY REQUIRED - LMC		0	0	0	0	0	0	91	0	0	1119	1345	1293	2033	2199	4469	4915	5023	5715	6432	7466	9134	10700	11930	12779	14864	15417	15970
SUPPLY REQUIRED - CAPACITY		0	0	0	0	0	0	120	0	0	1330	1693	1603	2340	2939	3542	4149	4231	4645	5076	5466	5856	6246	6636	7026	7416	7806	8196
PURCHASE RUCS CAPACITY		0	20	35	226	213	290	431	546	616	691	771	857	932	981	1020	1078	1126	1176	1222	1269	1316	1360	1403	1449	1490	1537	1582
HYDRAULIC FILM CAPACITY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
MAJOR SUPPLY REQUIRED - CAPACITY		0	0	0	0	0	0	0	0	0	171	0	0	407	1349	2803	2882	2097	2418	4432	5821	7346	9131	10930	11779	14370	14864	15417
MAJOR SUPPLY REQUIRED - CAPACITY		0	0	0	0	0	0	0	0	0	200	208	400	608	1008	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000
NEW PEAK CAPACITY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW PEAK CAPACITY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW MAJOR SUPPLY CAPACITY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

OTHER LOAD FORECAST		DEMAND / SUPPLY BALANCE - PEAK POWER (MW) - SUPPLY REPRESENTED IN CAPACITY																												DEC. 2014
CANDIDATE DEMAND/SUPPLY PLAN 24 (HIGHER POSSIBLE)																														
TECA (JAWAHAR)		1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014			
BASIC LOAD FORECAST		23052	24503	24509	27254	28714	29808	30754	31753	32861	33449	34767	35978	37374	38622	39536	40124	40563	41019	41396	42023	42469	43206	43769	44221	44678				
EXISTING FIRM LOAD MEETING CAPABILITY		23113	23976	24692	24784	25143	25310	25310	25310	25310	25422	26032	26032	26032	26032	26032	26032	26032	26032	26032	26032	26032	26032	26032	26032	26032	26032			
DEMAND/SUPPLY REQUIRED - LDC		739	927	1587	2572	2771	4396	5444	6423	6423	8239	8239	9355	10866	11282	12763	14310	15356	15874	17027	18112	18643	21286	22654	23227	23711	26109			
ELECTRICAL EFFICIENCY IMPROVEMENTS		0	14	36	54	158	229	322	425	528	705	916	1017	1100	1200	1320	1440	1560	1680	1800	1920	2040	2160	2280	2400	2520	2640			
LOAD SHEDDING		0	84	168	252	336	420	504	588	672	756	840	924	1008	1092	1176	1260	1344	1428	1512	1596	1680	1764	1848	1932	2016	2100			
DEFERRABLE LOAD DISPLACEMENT MUCS		0	55	55	172	239	306	373	440	507	574	641	708	775	842	909	976	1043	1110	1177	1244	1311	1378	1445	1512	1579	1646			
FIRM LOAD FORECAST		23122	24734	25713	28084	29683	30538	30961	31939	32533	33070	33516	34285	35202	36202	37267	38317	39377	40444	41523	42608	43700	44800	45908	47024	48148	49280			
CAPACITY INTERLUPTIBLE LOAD		123	128	610	660	660	672	696	705	724	744	765	782	798	811	826	841	857	871	884	896	907	917	926	934	941	954			
FIRM LOAD TOBECAIT		23227	25396	26327	28144	29202	30646	31565	32524	33229	33826	34311	34785	35248	35691	36114	36516	36897	37257	37597	37916	38214	38491	38748	38985	39202	39409			
SUPPLY REQUIRED - LDC		14	36	955	1740	2329	2936	3553	4091	4548	4916	5199	5411	5552	5622	5644	5644	5622	5588	5543	5488	5423	5348	5263	5168	5063	4948			
SUPPLY REQUIRED - CAPACITY		17	32	1294	1686	1645	1621	1608	1605	1605	1605	1605	1605	1605	1605	1605	1605	1605	1605	1605	1605	1605	1605	1605	1605	1605	1605			
POURCHASE MUCS CAPACITY		0	20	35	216	212	298	484	595	740	906	1035	1084	1133	1181	1230	1279	1327	1375	1423	1471	1516	1565	1609	1652	1694	1736			
HYDRAULIC FIRM CAPACITY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
MAJOR SUPPLY REQUIRED - CAPACITY		17	4	1179	1600	730	3506	2271	3901	3901	4140	4140	4350	4465	4574	4684	4794	4904	5014	5124	5234	5344	5454	5564	5674	5784	5894			
POMITORA POURCHASE CAPACITY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
NEW FOSIL CAPACITY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
NEW NUCLEAR CAPACITY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
NEW MAJOR SUPPLY CAPACITY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			

LOWER LOAD FORECAST		DURATION / SUPPLY BALANCE - PEAK PERIOD (PM) - SUPPLY EXPRESSED IN CAPACITY		CANDIDATE DURATION/SUPPLY PLAN 34 (WIGGERS POSSIBLE)		DRC.									
YEAR (2000-2014)	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
BASIC LOAD FORECAST	22500	22400	22300	22200	22100	22000	21900	21800	21700	21600	21500	21400	21300	21200	21100
EXISTING FIRM LOAD WITHIN CAPABILITY	22213	22100	22000	21900	21800	21700	21600	21500	21400	21300	21200	21100	21000	20900	20800
OTHER/SUPPLY REQUIRED - LMC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
ELECTRICAL EFFICIENCY IMPROVEMENTS	0	14	26	42	61	84	110	139	169	199	229	259	289	319	349
LOAD SHEDDING	0	18	161	146	107	519	376	240	107	749	508	276	146	80	36
DIFFERABLE LOAD DISPLACEMENT BUSES	0	55	90	132	179	230	282	334	386	438	490	542	594	646	698
PRIMAAT LOAD FORECAST	22500	22216	22401	22704	22904	23104	23304	23504	23704	23904	24104	24304	24504	24704	24904
CAPACITY WITHIN/OUTSIDE, LOADS	715	769	819	869	919	969	1019	1069	1119	1169	1219	1269	1319	1369	1419
FIRM LOAD FORECAST	21565	21607	21673	21751	21840	21940	22040	22140	22240	22340	22440	22540	22640	22740	22840
SUPPLY REQUIRED - LMC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
SUPPLY REQUIRED - CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PURCHASE WIRE CAPACITY	0	38	55	84	113	142	171	200	229	258	287	316	345	374	403
REDUCIBLE FIRM CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
WALTON SUPPLY REQUIRED - CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
MAINTAIN PURCHASE CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW FIRMAL CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW WALTON SUPPLY CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

INDIAN LOAD FORECAST		1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
TOTAL (JULY/AUG)		22136	23069	24533	25403	26778	28664	29423	30893	30893	30413	30191	31111	32321	33381	34036	34330	34873	35312	35912	36423	36975	37315	38073	38464	39224	39612
BASEIC LOAD FORECAST		0	14	45	76	126	193	314	500	800	1100	1400	1700	2000	2100	2200	2400	2500	2600	2700	2800	2900	3000	3100	3200	3300	3300
ELECTRICAL EFFICIENCY IMPROVEMENTS		0	61	171	245	423	582	656	713	776	836	893	946	1000	1020	1040	1040	1040	1100	1120	1140	1160	1180	1200	1220	1240	1240
LOAD SHIFTING		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
DEFERRABLE LOAD DISPLACEMENT RUCS		0	59	101	176	243	310	314	359	373	384	391	392	403	407	411	414	418	422	426	430	433	437	441	445	449	452
FIRM LOAD FORECAST		22136	23069	24533	25403	26778	28664	29423	30893	30893	30413	30191	31111	32321	33381	34036	34330	34873	35312	35912	36423	36975	37315	38073	38464	39224	39612
PRIMATE LOAD FORECAST		713	713	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632
CAPACITY INTERMITTIBLE LOADS		713	713	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632	632
FIRM LOAD FORECAST		22136	23069	24533	25403	26778	28664	29423	30893	30893	30413	30191	31111	32321	33381	34036	34330	34873	35312	35912	36423	36975	37315	38073	38464	39224	39612
EXISTING FIRM LOAD MEETING CAPABILITY		22136	23069	24533	25403	26778	28664	29423	30893	30893	30413	30191	31111	32321	33381	34036	34330	34873	35312	35912	36423	36975	37315	38073	38464	39224	39612
PUCABASE RUCS IAC		0	23	41	102	232	311	340	433	493	557	622	686	751	821	891	968	1047	1127	1207	1287	1367	1447	1527	1607	1687	1767
HYDRAULIC FIRM IAC		0	0	0	0	2	12	43	269	424	424	440	466	492	518	544	570	596	622	648	674	700	726	752	778	804	830
HARITABA PUCABASE IAC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW FIRM IAC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
FIRM LOAD MEETING CAPABILITY		22136	23069	24533	25403	26778	28664	29423	30893	30893	30413																

**DEMAND / SUPPLY BALANCE - PEAK POWER (MW) - SUPPLY EXPRESSED IN LOAD METTING CAPABILITY
PROPOSED REFERENCE PLAN IS**

TOTAL LOAD FORECAST		YEAR (ANNUAL)																														
		1999	1999	2000	2000	2001	2001	2002	2002	2003	2003	2004	2004	2005	2005	2006	2006	2007	2007	2008	2008	2009	2009	2010	2010	2011	2011	2012	2012	2013	2013	2014
TOTAL LOAD FORECAST		2000	2000	2001	2001	2002	2002	2003	2003	2004	2004	2005	2005	2006	2006	2007	2007	2008	2008	2009	2009	2010	2010	2011	2011	2012	2012	2013	2013	2014	2014	2015
BASIC LOAD FORECAST		2000	2000	2001	2001	2002	2002	2003	2003	2004	2004	2005	2005	2006	2006	2007	2007	2008	2008	2009	2009	2010	2010	2011	2011	2012	2012	2013	2013	2014	2014	2015
ELECTRICAL EFFICIENCY IMPROVEMENTS		0	16	36	39	139	239	339	439	1009	1219	1319	1419	1519	1619	1719	1819	1919	2019	2119	2219	2319	2419	2519	2619	2719	2819	2919	3019	3119	3219	3319
LOAD SHEDDING		0	0	100	200	300	400	500	600	700	800	900	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	2000	2100	2200	2300	2400	2500	2600	2700	2800	2900
DEFERRABLE LOAD DISPLACEMENT BUS		0	35	30	112	210	305	312	405	410	505	605	705	805	905	1005	1105	1205	1305	1405	1505	1605	1705	1805	1905	2005	2105	2205	2305	2405	2505	2605
PAIRED LOAD FORECAST		2000	2000	2001	2001	2002	2002	2003	2003	2004	2004	2005	2005	2006	2006	2007	2007	2008	2008	2009	2009	2010	2010	2011	2011	2012	2012	2013	2013	2014	2014	2015
CAPACITY UTILIZABLE LOADS		715	710	610	610	610	612	610	612	610	612	610	612	610	612	610	612	610	612	610	612	610	612	610	612	610	612	610	612	610	612	610
FIRM LOAD FORECAST		2000	2000	2001	2001	2002	2002	2003	2003	2004	2004	2005	2005	2006	2006	2007	2007	2008	2008	2009	2009	2010	2010	2011	2011	2012	2012	2013	2013	2014	2014	2015
EXISTING FIRM LOAD METTING CAPABILITY		2000	2000	2001	2001	2002	2002	2003	2003	2004	2004	2005	2005	2006	2006	2007	2007	2008	2008	2009	2009	2010	2010	2011	2011	2012	2012	2013	2013	2014	2014	2015
PURCHASE BUS INC		0	23	46	102	202	302	402	502	602	702	802	902	1002	1102	1202	1302	1402	1502	1602	1702	1802	1902	2002	2102	2202	2302	2402	2502	2602	2702	2802
HYDROELECTRIC PLANT INC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NATURAL GAS PLANT INC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW FOSBIL INC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW NUCLEAR INC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PLANNED FIRM LOAD METTING CAPABILITY		2000	2000	2001	2001	2002	2002	2003	2003	2004	2004	2005	2005	2006	2006	2007	2007	2008	2008	2009	2009	2010	2010	2011	2011	2012	2012	2013	2013	2014	2014	2015
DEMAND/SUPPLY REQUIRED - INC		715	717	1007	1012	1017	1022	1027	1032	1037	1042	1047	1052	1057	1062	1067	1072	1077	1082	1087	1092	1097	1102	1107	1112	1117	1122	1127	1132	1137	1142	1147
SUPPLY REQUIRED - CAPACITY		11	21	1211	1016	1021	1026	1031	1036	1041	1046	1051	1056	1061	1066	1071	1076	1081	1086	1091	1096	1101	1106	1111	1116	1121	1126	1131	1136	1141	1146	1151
NATURAL GAS REQUIRED - CAPACITY		11	4	1119	1010	1015	1020	1025	1030	1035	1040	1045	1050	1055	1060	1065	1070	1075	1080	1085	1090	1095	1100	1105	1110	1115	1120	1125	1130	1135	1140	1145

DEMAND / SUPPLY BALANCE - PEAK POWER (MW) - SUPPLY EXPRESSED IN LOAD MEETING CAPABILITY
 BALANCED REFERENCE YEAR IS

LOWER LOAD FORECAST	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
YEAR (LUMPY)	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
BASIC LOAD FORECAST	21610	21613	21766	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816
ELECTRICAL EFFICIENCY IMPROVEMENTS	0	16	36	62	101	146	251	400	640	880	1120	1360	1600	1840	1725	1780	1830	1913	1974	2038	2100	2163	2225	2288	2350	2412
LOAD SHIFTING	0	10	161	246	307	319	376	420	463	507	549	591	633	675	717	759	800	842	884	926	968	1000	1042	1084	1126	1168
DEFERRABLE LOAD DISPLACEMENT RUCS	0	16	36	172	320	506	730	942	1142	1342	1542	1742	1942	2142	2342	2542	2742	2942	3142	3342	3542	3742	3942	4142	4342	4542
PRIMAAT LOAD FORECAST	21610	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716
CAPACITY INTERMITTIBLE LOADS	725	709	399	383	366	354	336	361	366	373	380	387	394	401	416	423	433	443	453	466	482	497	513	529	545	561
FIRM LOAD FORECAST	21610	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716
EXISTING FIRM LOAD MEETING CAPABILITY	21610	21616	21662	21764	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816	21816
PURCHASE RUCS LDC	0	31	46	102	322	321	331	331	331	331	331	331	331	331	331	331	331	331	331	331	331	331	331	331	331	331
HYDRAULIC FIRM LDC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NUCLEAR PURCHASE LDC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW FIRM LDC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW NUCLEAR LDC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PLANNED FIRM LOAD MEETING CAPABILITY	21610	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716	21716
DEMAND/SUPPLY REQUIRED - LDC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
SUPPLY REQUIRED - CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
MAJOR SUPPLY REQUIRED - CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Medien und Politik

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DEMAND / SUPPLY BALANCE - PEAK POWER (MW) - SUPPLY EXPRESSED IN LOAD MEETING CAPABILITY
ALTERNATIVE DEMAND/SUPPLY PLAN 22 (SIOGRA NUCLEAR)

OTHER LOAD FORECAST		1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
YEAR (JANUARY)																											
BASIC LOAD FORECAST		21952	24907	26649	27356	28714	29608	30154	31752	32541	33649	34747	35976	37374	38622	39526	40124	40543	41079	41596	42022	42469	42910	43264	43703	44221	44678
ELECTRICAL EFFICIENCY IMPROVEMENTS		0	14	36	58	130	239	393	625	1008	1731	2756	4139	5760	7623	9730	12075	14658	17480	20540	23950	27800	32100	36950	42350	48300	54800
ELECTRICAL EFFICIENCY LOAD SHIFTING		0	84	100	202	435	735	120	793	978	946	1017	1109	1200	1280	1340	1380	1400	1400	1390	1360	1300	1200	1000	800	600	400
DEFERRABLE LOAD DISPLACEMENT WOOD		0	35	56	172	336	306	372	403	430	466	466	466	472	475	478	482	485	490	493	497	500	504	508	511	515	518
PRIMARY LOAD FORECAST		21952	24714	25715	26606	28043	29338	29741	31929	32623	33876	35356	37025	38853	40853	43027	45357	47843	50492	53315	56333	59660	63301	67256	71537	76146	81093
CAPACITY INTERFERABLE LOADS		735	758	658	660	640	672	656	705	724	744	765	782	796	811	826	841	857	871	884	896	907	917	928	938	948	951
FIRM LOAD FORECAST		22227	25556	25557	26144	27202	27666	28365	29244	29529	30126	30771	31503	32404	33491	34674	35940	37323	38849	40523	42349	44326	46454	48730	51157	53733	56462
EXISTING FIRM LOAD MEETING CAPABILITY		22213	23710	24642	25784	26743	27510	28131	28631	29131	29632	30132	30632	31132	31632	32132	32632	33132	33632	34132	34632	35132	35632	36132	36632	37132	37632
FURCHASE WOOD LDC		0	23	44	102	253	321	390	400	403	421	435	454	474	494	514	534	554	574	594	614	634	654	674	694	714	734
HYDRAULIC FIRM LDC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NATURAL GAS FIRM LDC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW FIRM LDC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
FIRM LOAD MEETING CAPABILITY		22213	23710	24642	25784	26743	27510	28131	28631	29131	29632	30132	30632	31132	31632	32132	32632	33132	33632	34132	34632	35132	35632	36132	36632	37132	37632
DEMAND/SUPPLY REQUIRED - LDC		735	917	1967	3372	3771	4200	3244	3621	4630	6139	9235	9186	11202	12763	14230	15590	15330	15374	17027	18113	19603	21360	22454	23327	23711	24109
SUPPLY REQUIRED - CAPACITY		17	32	1234	1666	1045	1931	2768	3035	4216	5972	6531	6710	7027	8444	11203	11944	12071	12309	13752	14886	16364	18353	19784	20800	22318	23713
MAJOR SUPPLY REQUIRED - CAPACITY		17	4	1179	1460	750	2500	3221	3307	3940	4140	4180	4150	3465	4074	4344	4856	4736	5081	10200	11272	12827	14473	15753	16552	16976	17268

DEMAND / SUPPLY BALANCE - PEAK POWER (MW) - SUPPLY EXPRESSED IN LOAD MEETING CAPABILITY
 ALTERNATIVE DEMAND/SUPPLY PLAN 22 (BROWN FUEL)A

LOCAL LOAD FORECAST		1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
TOTAL (MW/HR)		1199	1240	1276	1314	1352	1390	1428	1466	1504	1542	1580	1618	1656	1694	1732	1770	1808	1846	1884	1922	1960	2000	2040	2080	2120	2160
BASIC LOAD FORECAST		1199	1240	1276	1314	1352	1390	1428	1466	1504	1542	1580	1618	1656	1694	1732	1770	1808	1846	1884	1922	1960	2000	2040	2080	2120	2160
ELECTRICAL EFFICIENCY IMPROVEMENTS		0	14	26	42	101	146	231	400	640	880	1100	1300	1500	1685	1725	1760	1850	1912	1974	2028	2100	2185	2225	2280	2330	2400
LOAD SHEDDING		0	70	161	245	287	319	316	430	603	707	749	780	808	820	840	860	900	920	960	980	1000	1020	1040	1060	1080	1100
DEFERRABLE LOAD REPLACEMENT		0	35	98	172	239	206	330	342	342	342	342	342	342	342	342	342	346	350	353	357	360	364	368	371	375	378
PRIMARY LOAD FORECAST		2210	2216	2247	2324	2336	2374	2374	2383	2383	2381	2383	2391	2393	2403	2435	2511	2554	2610	2624	2652	2717	2723	2829	2830	2919	2968
CAPACITY INTERCHANGEABLE LOADS		725	709	699	689	679	669	659	649	639	629	619	609	599	589	579	569	559	549	539	529	519	509	499	489	479	469
FIRM LOAD FORECAST		2195	2167	2147	2131	2119	2100	2086	2072	2061	2050	2039	2026	2013	2004	1998	1984	1969	1954	1939	1924	1909	1894	1879	1864	1849	1834
EXISTING FIRM LOAD MEETING CAPABILITY		2210	2210	2202	2186	2170	2150	2131	2110	2089	2067	2044	2021	1998	1975	1950	1926	1902	1878	1854	1830	1806	1781	1757	1733	1709	1685
PULSAR PUMP INC		0	23	41	102	232	321	351	351	351	351	351	351	351	351	351	351	351	351	351	351	351	351	351	351	351	
HYDRAULIC PUMP INC		0	0	0	0	12	67	269	424	640	840	1040	1240	1439	1639	1839	2039	2239	2439	2639	2839	3039	3239	3439	3639	3839	
HYDRAULIC PUMP INC		0	0	0	0	0	0	0	0	0	141	361	323	484	804	804	804	804	804	804	804	804	804	804	804	804	
HYDRAULIC PUMP INC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
NEW FOSBIL INC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
PLANNED FIRM LOAD MEETING CAPABILITY		2210	2210	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106	2106
DEMAND/SUPPLY REQUIRED - INC		0	0	0	0	0	0	0	0	0	0	0	302	1091	2895	2617	2423	2106	5012	6130	7841	9127	11440	12172	14440	15072	
SUPPLY REQUIRED - CAPACITY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
PULSAR PUMP INC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

DEMAND / SUPPLY BALANCE - PEAK POWER (MW) - SUPPLY EXPANDED IN LOAD MEETING CAPABILITY
REFERENCE PLAN 24

MEDIUM LOAD FORECAST	YEAR (MONTH)															
	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004
BASIC LOAD FORECAST	23156	23069	24033	23463	24078	24084	23943	24089	24613	24013	24197	24111	23232	23251	24038	24336
ELECTRICAL EFFICIENCY IMPROVEMENTS	0	16	45	78	126	183	214	306	406	498	1100	1700	2050	2188	2350	2400
ELECTRICAL EFFICIENCY LOAD SHIFTING	0	81	171	266	423	583	636	717	774	826	893	946	1000	1030	1040	1040
DIFFERABLE LOAD DISPLACEMENT	0	35	96	172	239	306	330	333	369	386	387	388	399	403	407	410
PEAK LOAD FORECAST	23156	23153	24219	24643	24687	24688	24688	24688	24688	24688	24688	24688	24688	24688	24688	24688
CAPACITY AVAILABLE	723	723	622	623	623	623	623	623	623	623	623	623	623	623	623	623
FIRM LOAD FORECAST	23431	23216	23367	23222	23866	23190	23411	23866	24036	24033	24041	23989	24131	24036	23879	23823
EXISTING FIRM LOAD MEETING CAPABILITY	23213	23078	24042	24184	24343	23310	23310	24131	24131	24131	24131	24131	24131	24131	24131	24131
PURCHASED FIRM LOAD	0	23	44	182	332	321	300	439	497	537	612	691	732	791	831	849
HYDRAULIC FIRM LOAD	0	0	0	0	0	2	12	67	269	424	424	424	424	424	424	424
MAINTENANCE FIRM LOAD	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW FIRM LOAD	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW NUCLEAR FIRM LOAD	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PLANNED FIRM LOAD MEETING CAPABILITY	23213	23093	24106	24366	24397	23803	23557	24038	24038	24038	24038	24038	24038	24038	24038	24038
DEMAND/SUPPLY SHORTFALL - FIRM	0	0	411	619	0	1376	2623	1946	2362	4102	4725	5019	6160	7422	8844	9186
SUPPLY SHORTFALL - CAPACITY	0	0	0	0	0	0	123	0	0	1393	1690	1600	2552	2844	3347	4176
MAJOR SUPPLY SHORTFALL - CAPACITY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

DEMAND / SUPPLY BALANCE - TOTAL FORTIA (MW) - SUPPLY EXPRESSED IN LOAD MEETING CAPABILITY		REFERENCE PLAN 26	
OFFER LOAD FORECAST		TOTAL (JANUARY)	
		1999	2000
BASIC LOAD FORECAST	2000	2001	2002
ELECTRICAL EFFICIENCY IMPROVEMENTS	0	0	0
LOAD SHIFTING	0	0	0
DISTRIBUTABLE LOAD DISPLACEMENT WOOD	0	0	0
PAVIMENT LOAD FORECAST	2003	2004	2005
CAPACITY LIMITATION LOADS	2006	2007	2008
FIRM LOAD FORECAST	2009	2010	2011
EXISTING FIRM LOAD MEETING CAPABILITY	2012	2013	2014
FORECAST FIRM LOAD	2015	2016	2017
HYDROLOGIC PLAN LOAD	2018	2019	2020
NONFIRM FORECAST LOAD	2021	2022	2023
NEW FIRM LOAD	2024	2025	2026
NEW WUCOLAN LOAD	2027	2028	2029
PLANNED FIRM LOAD MEETING CAPABILITY	2030	2031	2032
DEMAND/SUPPLY ACQUIRED - LDC	2033	2034	2035
SUPPLY ACQUIRED - CAPACITY	2036	2037	2038
PAVIA SUPPLY ACQUIRED - CAPACITY	2039	2040	2041

DEMAND / SUPPLY BALANCE - BEAM POWER (MW) - SUPPLY EXPRESSED IN LOAD MEETING CAPABILITY
REFERENCE PLAN 24

LOWER LOAD FORECAST		1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
YEAR (JANUARY)		1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
BASIC LOAD FORECAST		22690	22463	22766	22914	23003	23075	23121	23155	23212	23210	23104	23723	24594	27150	28171	28661
ELECTRICAL EFFICIENCY IMPROVEMENTS		0	14	36	62	101	146	251	400	648	888	1120	1360	1600	1842	2083	2325
LOAD SHIFTING		0	70	161	246	307	319	376	430	663	707	749	798	840	880	920	960
DEFERRABLE LOAD DISPLACEMENT RUCS		0	33	90	172	239	306	330	342	342	342	342	342	342	342	342	342
PRIMAARY LOAD FORECAST		22690	22316	22701	22914	23003	23075	23121	23155	23212	23210	23104	23723	24594	27150	28171	28661
CAPACITY INTERMITTIBLE LOADS		723	709	599	562	566	554	558	561	566	573	580	587	599	607	616	623
FIRM LOAD FORECAST		21965	21607	22102	22356	22437	22526	22562	22594	22648	22683	22684	22732	23244	24210	24608	24921
EXISTING FIRM LOAD MEETING CAPABILITY		22313	22970	24062	24704	25100	25310	25510	25710	25910	26110	26310	26510	26710	26910	27110	27310
PURCHASE RUCS LDC		0	33	44	102	252	251	251	251	251	251	251	251	251	251	251	251
HYDROPOWER PURCHASE LDC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NATURAL GAS PURCHASE LDC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NATURAL GAS PURCHASE LDC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NEW NUCLEAR LDC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PLANNED FIRM LOAD MEETING CAPABILITY		22313	22970	24062	24704	25100	25310	25510	25710	25910	26110	26310	26510	26710	26910	27110	27310
DEMAND/SUPPLY REQUIRED - LDC		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
SUPPLY REQUIRED - CAPACITY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
MAJOR SUPPLY REQUIRED - CAPACITY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

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DEMAND / SUPPLY BALANCE - ANNUAL ENERGY (TWH) FORT PLAN 15

MEDIUM LOAD FORECAST																											
YEAR	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	
BASE LOAD FORECAST	137.0	140.0	145.0	151.0	158.0	168.0	180.0	190.0	198.0	174.0	178.0	184.0	192.0	194.0	201.0	202.0	205.0	208.0	211.0	214.0	217.0	220.0	224.0	227.0	230.0	234.0	
ELECTR. EFFIC. IMPROVE.	0.1	0.2	0.4	0.6	0.8	1.6	2.5	4.0	5.5	7.0	8.5	10.0	10.5	11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.5	15.0	15.5	16.0	16.5	17.0	
LOAD SHIFTING	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
LOAD DISPLACEMENT KW09	0.1	0.4	1.3	1.8	2.3	2.5	2.7	2.8	2.8	2.9	2.9	3.0	3.0	3.0	3.1	3.1	3.1	3.2	3.2	3.2	3.2	3.3	3.3	3.3	3.3	3.4	
PRIMAUM LOAD FORECAST																											
	136.8	139.0	143.3	148.6	151.6	155.0	157.8	160.2	160.7	164.1	164.6	171.0	178.5	182.0	186.4	186.9	189.4	191.9	194.3	196.8	199.3	201.7	204.2	207.7	210.2	213.6	
HYDRAULIC																											
	35.6	35.6	35.6	35.6	35.7	35.7	35.8	36.4	37.1	37.1	38.5	38.5	38.6	39.0	39.3	39.5	39.8	39.8	39.8	39.8	40.0	40.3	40.6	40.6	40.6	40.8	
PURCHASE KW09																											
	0.3	0.6	1.7	2.3	2.9	3.4	3.8	4.3	4.8	5.2	5.8	6.4	6.7	7.1	7.4	7.7	8.0	8.4	8.7	9.0	9.3	9.6	9.8	10.0	10.2	10.5	
MAINTENANCE PURCHASE																											
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	1.4	1.7	3.3	5.1	6.8	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	
FOSNIL																											
	28.3	22.1	19.3	20.8	20.0	19.6	20.6	15.6	21.1	25.8	17.8	21.0	25.6	32.0	34.1	32.5	19.3	16.5	15.2	21.4	22.4	19.4	23.6	22.8	14.4	12.4	
NUCLEAR																											
	72.6	80.7	84.6	88.7	93.2	94.3	97.4	101.9	97.7	96.0	103.0	103.4	103.9	98.8	98.9	110.2	115.3	119.2	123.7	119.6	120.5	124.2	127.2	130.0	143.0		
TOTAL PRODUCTION																											
	136.8	139.0	143.3	148.6	151.6	155.0	157.8	160.2	160.7	164.1	164.6	171.0	178.5	182.0	186.4	186.9	189.4	191.9	194.3	196.8	199.3	201.7	204.2	207.7	210.2	213.6	

DEMAND / SUPPLY BALANCE - ANNUAL ENERGY (TWH) FORT PLAN 15

UPPER LOAD FORECAST																													
YEAR	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014			
BASE LOAD FORECAST	142.0	147.0	154.0	162.0	169.0	176.0	180.0	185.0	182.0	186.0	205.0	212.0	221.0	227.0	231.0	234.0	236.0	240.0	242.0	245.0	247.0	250.0	252.0	255.0	257.0	260.0			
ELECTR. EFFIC. IMPROVE.	0.1	0.3	0.5	0.8	1.1	2.0	3.1	5.0	6.9	8.7	10.8	12.5	13.1	13.7	14.4	15.0	15.6	16.2	16.8	17.5	18.1	18.7	19.4	20.0	20.6	21.2			
LOAD SHIFTING	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0			
LOAD DISPLACEMENT KW09	0.5	0.8	1.4	1.9	2.4	2.9	3.2	3.5	3.6	3.7	3.7	3.7	3.7	3.8	3.8	3.8	3.9	3.9	3.9	3.9	4.0	4.0	4.0	4.1	4.1	4.1			
PRIMAUM LOAD FORECAST																													
	141.4	145.9	152.2	159.3	165.4	171.1	173.7	178.6	181.5	185.8	190.7	195.8	204.1	209.5	212.6	215.2	216.5	219.9	221.2	223.6	224.9	227.3	229.6	230.9	232.3	234.6			
HYDRAULIC																													
	35.6	35.6	35.6	35.6	35.7	35.7	35.8	36.4	37.1	37.1	38.5	38.5	38.6	39.0	39.3	39.5	39.8	39.8	39.8	39.8	40.0	40.3	40.6	40.6	40.8	40.8			
PURCHASE KW09																													
	0.2	0.5	1.7	2.2	2.6	3.3	4.0	5.0	6.1	7.0	7.3	7.8	8.0	8.3	8.6	8.8	9.0	9.3	9.6	9.8	10.2	10.6	10.7	10.8	10.9	11.2			
MAINTENANCE PURCHASE																													
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	1.4	1.7	3.3	5.1	6.8	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0			
FOSNIL																													
	32.8	28.6	27.2	26.8	26.8	24.3	25.1	21.0	20.8	44.6	39.0	43.4	48.4	54.0	52.5	42.9	37.0	37.4	38.2	38.6	38.2	38.1	38.1	35.6	11.2	6.9			
NUCLEAR																													
	72.6	81.2	87.6	90.8	94.3	97.8	98.8	104.1	98.8	96.8	104.5	104.6	104.7	99.1	105.6	116.6	120.5	126.1	128.3	127.9	130.1	130.1	134.1	134.1	134.1	134.1			
TOTAL PRODUCTION																													
	141.4	145.9	152.2	159.3	165.4	171.1	173.7	178.6	181.5	185.8	190.7	195.8	204.1	209.5	212.6	215.2	216.5	219.9	221.2	223.6	224.9	227.3	229.6	230.9	232.3	234.6			

DEMAND / SUPPLY BALANCE - ANNUAL ENERGY (TWH) FORT PLAN 15

LOWER LOAD FORECAST		1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
YEAR		1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
BASE LOAD FORECAST		132.0	133.0	135.0	137.0	138.0	139.0	141.0	141.0	143.0	144.0	148.0	153.0	159.0	163.0	164.0	167.0	168.0	171.0	174.0	178.0	181.0	185.0	188.0	191.0	194.0	197.0
ELECTR. EFFIC. IMPROVE.		0.1	0.2	0.3	0.5	0.7	1.3	2.0	3.2	4.4	5.6	6.8	8.0	8.3	8.6	8.9	9.2	9.6	9.9	10.2	10.6	10.8	11.1	11.4	11.7	12.1	12.4
LOAD SHIFTING		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
LOAD DISPLACEMENT KW09		0.5	0.8	1.4	1.9	2.4	2.8	3.2	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.8	3.8	3.8	3.8	3.9	3.9	3.9	3.9	3.9	3.9
PRIMAUM LOAD FORECAST		131.4	132.0	133.3	134.6	134.9	135.1	136.3	136.1	138.9	137.7	139.5	142.3	148.0	151.7	154.4	155.0	155.7	158.3	161.0	164.7	167.3	171.0	173.6	176.3	179.0	181.6
HYDRAULIC		35.6	35.6	35.6	35.6	35.7	35.7	35.8	36.4	37.1	37.1	38.5	38.5	38.6	39.0	39.3	39.5	39.8	39.8	39.8	39.8	40.0	40.3	40.6	40.6	40.8	40.8
PURCHASE KW09		0.2	0.5	1.7	2.2	2.8	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.3	3.6	3.8	4.3	4.6	4.9	5.2	5.3	5.5	5.8	5.7	5.8
MAINTENANCE PURCHASE		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	1.4	1.7	3.3	5.1	6.8	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0
FOSFIL		23.3	18.3	11.6	9.9	7.2	6.3	6.7	3.7	4.6	6.7	2.7	3.4	4.9	6.1	6.6	8.8	8.3	9.0	10.8	18.5	20.3	18.4	22.2	21.7	13.1	10.3
NUCLEAR		72.3	79.4	84.5	88.6	89.1	90.1	90.8	92.0	91.3	90.7	93.9	95.8	98.0	93.6	94.4	99.3	99.6	99.3	98.8	94.5	94.7	99.9	94.4	101.4	112.6	117.7
TOTAL PRODUCTION		131.4	132.0	133.3	134.6	134.9	135.1	136.3	136.1	138.9	137.7	139.5	142.3	148.0	151.7	154.4	155.0	155.7	158.3	161.0	164.7	167.3	171.0	173.6	176.3	179.0	181.6

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DEMAND / SUPPLY BALANCE - ANNUAL ENERGY (TWN FOR PLAN 22)

MEDIAN LOAD FORECAST		1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
YEAR		1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
BASIC LOAD FORECAST		137.0	140.0	143.0	151.0	155.0	160.0	163.0	165.0	168.0	174.0	178.0	184.0	182.0	184.0	201.0	202.0	205.0	214.0	211.0	214.0	217.0	220.0	224.0	227.0	230.0	234.0
ELECT. EFFIC. IMPROVE.		0.1	0.2	0.4	0.6	0.9	1.8	2.5	4.0	5.8	7.0	8.8	10.0	10.5	11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.5	15.0	15.5	16.0	16.5	17.0
LOAD SHIFTING		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
LOAD DISPLACEMENT NUCOS		0.1	0.8	1.3	1.8	2.3	2.5	2.7	2.8	2.8	2.8	2.8	2.8	3.0	3.0	3.1	3.1	3.2	3.2	3.2	3.2	3.2	3.3	3.3	3.3	3.3	3.4
LOAD DISPLACEMENT NUCOS		0.1	0.8	1.3	1.8	2.3	2.5	2.7	2.8	2.8	2.8	2.8	2.8	3.0	3.0	3.1	3.1	3.2	3.2	3.2	3.2	3.2	3.3	3.3	3.3	3.3	3.4
PRIORITY LOAD FORECAST		136.8	130.0	143.3	148.6	151.8	165.0	157.8	160.2	160.7	164.1	168.6	171.0	178.5	182.0	186.4	186.9	189.4	191.9	194.3	196.8	199.3	201.7	205.2	207.7	210.2	213.6
HYDRAULIC		35.8	35.6	35.6	35.6	35.7	35.7	35.6	34.4	37.1	37.1	34.5	34.5	34.8	35.0	39.3	39.5	39.6	39.6	39.6	39.6	40.0	40.3	40.6	40.6	40.6	40.8
PURCHASE NUCOS		0.3	0.4	1.7	2.3	2.9	3.4	3.8	4.3	4.8	5.3	5.8	6.4	6.7	7.1	7.4	7.7	8.0	8.4	8.7	9.0	9.3	9.6	9.8	10.0	10.2	10.3
MANITOBA PURCHASE		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	1.4	1.7	3.3	5.1	6.6	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0
FOSSIL		24.3	22.1	19.3	20.9	20.0	19.8	20.8	15.6	21.1	25.5	17.6	21.0	25.8	29.0	22.7	12.2	8.7	13.2	10.2	11.4	8.8	8.8	9.0	8.7	6.4	5.4
NUCLEAR		72.6	80.7	64.6	69.7	69.2	64.3	67.4	101.9	91.7	96.0	103.0	103.4	103.9	104.8	110.3	120.6	124.8	123.5	128.7	129.6	134.4	136.1	138.9	141.4	144.0	150.0
TOTAL PRODUCTION		136.8	130.0	143.3	148.6	151.8	165.0	157.8	160.2	160.7	164.1	168.6	171.0	178.5	182.0	186.4	186.9	189.4	191.9	194.3	196.8	199.3	201.7	205.2	207.7	210.2	213.6

DEMAND / SUPPLY BALANCE - ANNUAL ENERGY (TWN FOR PLAN 22)

UPPER LOAD FORECAST		1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
YEAR		1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
BASIC LOAD FORECAST		142.0	147.0	154.0	162.0	168.0	176.0	180.0	185.0	192.0	198.0	205.0	212.0	221.0	227.0	231.0	234.0	236.0	240.0	242.0	245.0	247.0	250.0	252.0	255.0	257.0	260.0
ELECT. EFFIC. IMPROVE.		0.1	0.3	0.5	0.8	1.1	2.0	3.1	5.0	6.9	8.7	10.6	12.6	13.1	13.7	14.4	15.0	15.6	16.2	16.9	17.5	18.1	18.7	19.4	20.0	20.6	21.2
LOAD SHIFTING		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
LOAD DISPLACEMENT NUCOS		0.5	0.8	1.4	1.9	2.4	2.9	3.2	3.5	3.6	3.7	3.7	3.7	3.7	3.8	3.8	3.8	3.8	3.8	3.8	3.8	4.0	4.0	4.0	4.1	4.1	4.1
PRIORITY LOAD FORECAST		141.4	145.9	152.2	159.3	165.4	171.1	173.7	178.6	181.5	185.6	190.7	195.6	204.1	209.5	212.6	215.2	216.5	219.9	221.2	223.6	224.9	227.3	228.6	230.9	232.3	234.6
HYDRAULIC		35.6	35.6	35.6	35.6	35.7	35.7	35.6	34.4	37.1	37.1	34.5	34.5	34.8	35.0	39.3	39.5	39.6	39.6	39.6	40.0	40.3	40.6	40.6	40.6	40.8	40.8
PURCHASE NUCOS		0.2	0.6	1.7	2.2	2.8	3.3	4.0	8.0	6.1	7.0	7.3	7.8	8.0	8.3	8.6	9.0	9.3	9.6	9.8	10.2	10.6	10.7	10.8	10.9	11.1	11.2
MANITOBA PURCHASE		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	1.4	1.7	3.3	5.1	6.8	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0
FOSSIL		32.8	28.6	27.3	30.6	32.6	34.3	35.1	31.0	39.8	41.6	39.0	43.4	48.4	51.5	46.8	34.2	30.8	31.2	26.2	27.1	18.6	14.6	13.3	11.1	8.0	5.8
NUCLEAR		72.6	81.2	67.6	69.8	69.3	67.8	68.6	104.1	98.9	94.6	104.8	104.6	104.7	105.6	111.3	123.4	129.5	132.3	134.3	136.4	150.5	154.6	154.9	161.3	165.7	169.8
TOTAL PRODUCTION		141.4	145.9	152.2	159.3	165.4	171.1	173.7	178.6	181.5	185.6	190.7	195.6	204.1	209.5	212.6	215.2	216.5	219.9	221.2	223.6	224.9	227.3	228.6	230.9	232.3	234.6

DEMAND / SUPPLY BALANCE - ANNUAL ENERGY (TWN FOR PLAN 22)

LOWER LOAD FORECAST		1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
YEAR		1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
BASIC LOAD FORECAST		132.0	133.0	135.0	137.0	138.0	139.0	141.0	141.0	143.0	144.0	146.0	153.0	150.0	153.0	164.0	167.0	168.0	171.0	174.0	176.0	181.0	185.0	184.0	181.0	184.0	187.0
ELECT. EFFIC. IMPROVE.		0.1	0.2	0.3	0.5	0.7	1.3	2.0	3.2	4.4	5.6	6.8	8.0	8.3	8.8	9.2	9.6	9.9	10.2	10.5	10.8	11.1	11.4	11.7	12.1	12.4	12.8
LOAD SHIFTING		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
LOAD DISPLACEMENT NUCOS		0.5	0.8	1.4	1.9	2.4	2.9	3.2	3.5	3.6	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8
PRIMARY LOAD FORECAST		131.4	132.0	133.3	134.6	134.9	135.1	136.3	135.1	135.9	137.7	139.5	142.3	148.0	151.7	154.4	156.0	156.7	158.3	161.0	164.7	167.3	171.0	173.6	176.3	179.0	181.6
HYDRAULIC		35.6	35.6	35.6	35.6	35.7	35.7	35.6	34.4	37.1	37.1	34.5	34.5	34.8	35.0	39.3	39.5	39.6	39.6	39.6	40.0	40.3	40.6	40.6	40.6	40.8	40.8
PURCHASE NUCOS		0.2	0.5	1.7	2.2	2.8	3.3	3.8	4.3	4.8	5.3	5.8	6.4	6.7	7.1	7.4	7.7	8.0	8.4	8.7	9.0	9.3	9.6	9.8	10.0	10.2	10.3
MANITOBA PURCHASE		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	1.4	1.7	3.3	5.1	6.6	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0
FOSSIL		23.3	18.5	11.6	8.9	7.2	4.3	6.7	3.7	4.8	8.7	2.7	3.3	4.8	8.1	8.6	5.6	5.3	6.0	10.8	13.0	10.3	8.8	7.5	7.4	8.1	3.5
NUCLEAR		72.3	79.4	64.5	66.8	69.1	60.1	60.6	92.0	81.3	90.7	94.0	93.8	94.0	95.6	94.4	94.3	90.8	94.3	98.8	100.0	104.7	109.3	113.1	115.7	120.3	124.3
TOTAL PRODUCTION		131.4	132.0	133.3	134.6	134.9	135.1	136.3	135.1	135.9	137.7	139.5	142.3	148.0	151.7	154.4	156.0	156.7	158.3	161.0	164.7	167.3	171.0	173.6	176.3	179.0	181.6

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DEMAND / SUPPLY BALANCE - ANNUAL ENERGY (TWh) FOR PLAN 24

MEDIAN LOAD FORECAST

YEAR	1999	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	
BASIC LOAD FORECAST	137.0	140.0	143.0	151.0	155.0	159.0	163.0	165.0	169.0	174.0	178.0	184.0	182.0	186.0	191.0	201.0	202.0	205.0	208.0	211.0	214.0	217.0	220.0	224.0	227.0	230.0	234.0
ELECT. EFFIC. IMPROVE.	0.1	0.2	0.4	0.6	0.9	1.4	2.5	4.0	8.5	7.0	8.8	10.0	10.5	11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.5	15.0	15.5	16.0	16.5	17.0	
LOAD SHIFTING	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
LOAD DISPLACEMENT MUOS	0.1	0.8	1.3	1.8	2.3	2.8	2.7	2.8	2.8	2.9	2.9	3.0	3.0	3.0	3.1	3.1	3.1	3.2	3.2	3.2	3.2	3.3	3.3	3.3	3.3	3.4	
PRIMARY LOAD FORECAST	136.8	139.0	143.3	148.6	151.8	155.0	157.8	158.2	160.7	164.1	166.6	171.0	178.5	182.0	186.4	186.9	189.4	191.9	194.3	196.8	199.3	201.7	205.2	207.7	210.2	213.6	
HYDRAULIC	35.6	35.6	35.6	35.6	35.7	35.7	35.6	36.4	37.1	37.1	38.5	38.5	38.8	39.0	39.3	39.5	39.8	39.8	39.8	39.8	40.0	40.3	40.6	40.6	40.6	40.8	
PURCHASE MUOS	0.3	0.8	1.7	2.3	2.9	3.4	3.8	4.3	4.8	5.3	5.9	6.4	6.7	7.1	7.4	7.7	8.0	8.4	8.7	9.0	9.3	9.8	9.8	10.0	10.2	10.3	
MANITOBA PURCHASE	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	1.4	1.7	3.3	5.1	6.8	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	
FOSSIL	24.3	22.1	19.3	20.9	20.0	19.6	20.8	15.6	21.1	25.5	17.8	21.0	25.4	32.0	34.1	22.6	19.3	18.5	15.2	21.4	22.4	25.0	34.6	40.7	36.7	34.1	
NUCLEAR	72.6	80.7	84.6	89.7	93.2	94.3	97.4	101.9	97.7	96.0	103.0	103.4	103.9	94.8	98.9	110.2	115.3	118.2	123.7	119.6	120.3	119.8	113.1	109.4	115.7	121.3	
TOTAL PRODUCTION	136.8	139.0	143.3	148.6	151.8	155.0	157.8	158.2	160.7	164.1	166.6	171.0	178.5	182.0	186.4	186.9	189.4	191.9	194.3	196.8	199.3	201.7	205.2	207.7	210.2	213.6	

DEMAND / SUPPLY BALANCE - ANNUAL ENERGY (TWh) FOR PLAN 24

UPPER LOAD FORECAST

YEAR	1999	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
BASIC LOAD FORECAST	142.0	147.0	154.0	162.0	169.0	176.0	180.0	185.0	192.0	198.0	205.0	212.0	221.0	227.0	231.0	234.0	236.0	240.0	242.0	245.0	247.0	250.0	252.0	256.0	257.0	260.0
ELECT. EFFIC. IMPROVE.	0.1	0.3	0.5	0.8	1.1	2.0	3.1	5.0	6.9	8.7	10.6	12.8	13.1	13.7	14.4	15.0	15.6	16.2	16.9	17.5	18.1	18.7	19.4	20.0	20.6	21.2
LOAD SHIFTING	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
LOAD DISPLACEMENT MUOS	0.5	0.8	1.4	1.9	2.4	2.9	3.2	3.5	3.8	3.7	3.7	3.7	3.7	3.8	3.8	3.8	3.9	3.9	3.9	3.9	4.0	4.0	4.0	4.1	4.1	4.1
PRIMARY LOAD FORECAST	141.4	145.9	152.2	159.3	165.4	171.1	173.7	178.6	181.5	185.6	190.7	195.8	204.1	209.5	212.8	215.2	216.5	219.9	221.2	223.6	224.9	227.3	228.6	230.9	232.3	234.6
HYDRAULIC	35.6	35.6	35.6	35.6	35.7	35.7	35.6	36.4	37.1	37.1	38.5	38.5	38.8	39.0	39.3	39.5	39.8	39.8	39.8	39.8	40.0	40.3	40.6	40.6	40.6	40.8
PURCHASE MUOS	0.2	0.5	1.7	2.2	2.8	3.3	4.0	5.0	6.1	7.0	7.3	7.8	8.0	8.5	8.6	9.0	9.3	9.6	9.9	10.2	10.6	10.7	10.6	10.9	11.1	11.2
MANITOBA PURCHASE	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	1.4	1.7	3.3	5.1	6.8	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0
FOSSIL	32.6	28.6	27.3	30.6	32.6	34.3	35.1	31.0	39.6	44.9	39.0	43.4	49.4	54.0	52.5	42.9	37.0	37.4	38.2	44.8	39.6	34.5	36.1	37.8	32.8	28.7
NUCLEAR	72.8	81.2	87.6	90.8	94.3	97.8	98.8	104.1	98.9	96.8	104.5	104.6	104.7	99.1	105.6	116.8	123.5	126.1	126.3	121.7	127.7	132.7	132.1	134.6	140.9	144.9
TOTAL PRODUCTION	141.4	145.9	152.2	159.3	165.4	171.1	173.7	178.6	181.5	185.6	190.7	195.8	204.1	209.5	212.8	215.2	216.5	219.9	221.2	223.6	224.9	227.3	228.6	230.9	232.3	234.6

DEMAND / SUPPLY BALANCE - ANNUAL ENERGY (TWh) FOR PLAN 24

LOWER LOAD FORECAST

YEAR	1999	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
BASIC LOAD FORECAST	132.0	133.0	135.0	137.0	138.0	139.0	141.0	141.0	143.0	146.0	149.0	153.0	159.0	163.0	164.0	167.0	168.0	171.0	174.0	178.0	181.0	185.0	186.0	191.0	194.0	197.0
ELECT. EFFIC. IMPROVE.	0.1	0.2	0.3	0.5	0.7	1.3	2.0	3.2	4.4	5.8	6.8	8.0	8.3	8.8	8.9	9.2	9.6	9.9	10.2	10.5	10.8	11.1	11.4	11.7	12.1	12.4
LOAD SHIFTING	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
LOAD DISPLACEMENT MUOS	0.8	0.8	1.4	1.9	2.4	2.8	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.8	2.8	2.8	2.8	2.9	2.9	2.9	3.0	3.0	3.0
PRIMARY LOAD FORECAST	131.4	132.0	133.3	134.6	134.9	135.1	136.3	135.1	135.9	137.7	139.8	142.3	148.0	151.7	154.4	155.0	155.7	158.3	161.0	164.7	167.3	171.0	173.6	176.3	179.0	181.6
HYDRAULIC	35.6	35.6	35.6	35.6	35.7	35.7	35.6	36.4	37.1	37.1	38.5	38.5	38.8	39.0	39.3	39.5	39.8	39.8	39.8	39.8	40.0	40.3	40.6	40.6	40.6	40.8
PURCHASE MUOS	0.2	0.5	1.7	2.2	2.8	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.3	3.6	3.9	4.3	4.6	4.9	5.2	5.3	5.5	5.6	5.7	5.8
MANITOBA PURCHASE	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	1.4	1.7	3.3	5.1	6.8	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0
FOSSIL	23.3	19.5	11.6	9.9	7.2	6.3	6.7	3.7	4.8	6.7	2.7	3.4	4.9	9.1	8.6	5.6	5.3	9.0	10.6	18.5	20.3	18.4	22.2	21.7	18.4	20.1
NUCLEAR	72.3	79.4	84.5	88.8	89.1	90.1	90.8	92.0	91.3	90.7	93.9	95.6	98.0	95.6	96.4	99.3	99.6	98.3	96.8	94.5	94.7	99.9	96.4	101.4	107.3	107.8
TOTAL PRODUCTION	131.4	132.0	133.3	134.6	134.9	135.1	136.3	135.1	135.9	137.7	139.8	142.3	148.0	151.7	154.4	155.0	155.7	158.3	161.0	164.7	167.3	171.0	173.6	176.3	179.0	181.6

5. TRANSMISSION

5.0 INTRODUCTION

5.1 BACKGROUND

5.2 CRITICAL TRANSMISSION INTERFACES

5.3 TRANSMISSION REQUIREMENTS - CANDIDATE SITES

5.4 TRANSMISSION REQUIREMENTS - CANDIDATE PLANS

5.5 REVIEW

5.0 INTRODUCTION

This chapter discusses the transmission aspects of the major supply plans. In particular, it outlines the transmission requirements to incorporate the fossil and nuclear options being considered. The transmission required to incorporate the Non-Utility Generation (NUG) developments, the Hydraulic Program and the 1000 MW Manitoba Purchase are not covered in this chapter.

5.1 BACKGROUND

Transmission Purposes

The bulk electricity transmission system (BES) is the integrated system of transmission lines and stations by which electric power is delivered from major generating stations to and between load centers and to and from interconnections with neighbouring utilities.

The purpose of the bulk transmission system is:

- to deliver power to meet forecast growth in customer demand, recognizing regional variations in rates of growth;
- to incorporate new sources of power generation or purchases into the integrated transmission network to permit economic and reliable use of such generation or purchases;
- to integrate the Hydro BES with neighbouring utilities through interconnections with these utilities to permit economic and reliability enhancements; and
- to optimize the use of available generation and purchases in accordance with changing customer demands and environmental restrictions.

The primary reasons for developing such an integrated transmission system are to permit the most economical use of resources and to maintain adequate reliability of supply to area loads in the event of anticipated station and transmission component failures.

Planning Criteria

Transmission additions to the BES are based on the System Planning procedures for design of the Bulk Transmission System, first introduced over 20 years ago and updated regularly. These procedures take into account the more probable station and transmission component failures for which the system must remain stable with acceptable post disturbance voltage and loading levels. The procedures are based upon the Northeast Power Coordinating Council (NPCC) design and operation criteria for interconnected power systems.

Transmission System in Year 2000

The planned development of the transmission system up to the year 2000 is contained in the System Planning Report 679SP, entitled "1989 Bulk Electricity Transmission Report" dated October 1989. The most significant component of the transmission plan is the Southwestern Ontario transmission reinforcement, which will enable the incorporation of the Bruce generation complex, and will increase the power transfer capability into the London area. Other major transmission projects include 500 kilovolt (kV) transmission from Hamilton to Toronto, Kingston and Ottawa. By the late 1990's, four 500 kV circuits will be in-service between Hamilton and Kingston.

The major transmission facilities listed in Figure 5.1 and shown in Figure 5.2, provide a strong base system for incorporating the demand and supply options under consideration in the Demand/Supply Plan Report. However, additional bulk transmission facilities will be required beyond the year 2000, to meet growth in customer demand and to incorporate new supply options, including the hydroelectric program, NUG developments, major purchases and new thermal generating stations. Both the nature and timing of these transmission facilities will be influenced by the timing, sequencing, location and choice of option of generating stations, and by the rate and magnitude of load growth.

Transmission Classification

The transmission required to incorporate a new Ontario Hydro generating station will include radial transmission necessary to connect the site to the existing and planned BES. It may also include inter-area transmission necessary to maintain an integrated BES. The need for radial transmission is driven solely by the choice of site and its proximity to a suitable existing or planned transmission station in the integrated system. The need for inter-area transmission can also be driven by choice of sites, but is also concerned with many other factors such as security and reliability of load supply, geographic balancing of load and generation, cost and availability of fuel, and operational flexibility and economics. In summary, this inter-area transmission is governed by area load growth and existing capacity considerations in addition to the siting of new generation.

Figure 5.1

Base Case Bulk Transmission System in 2000

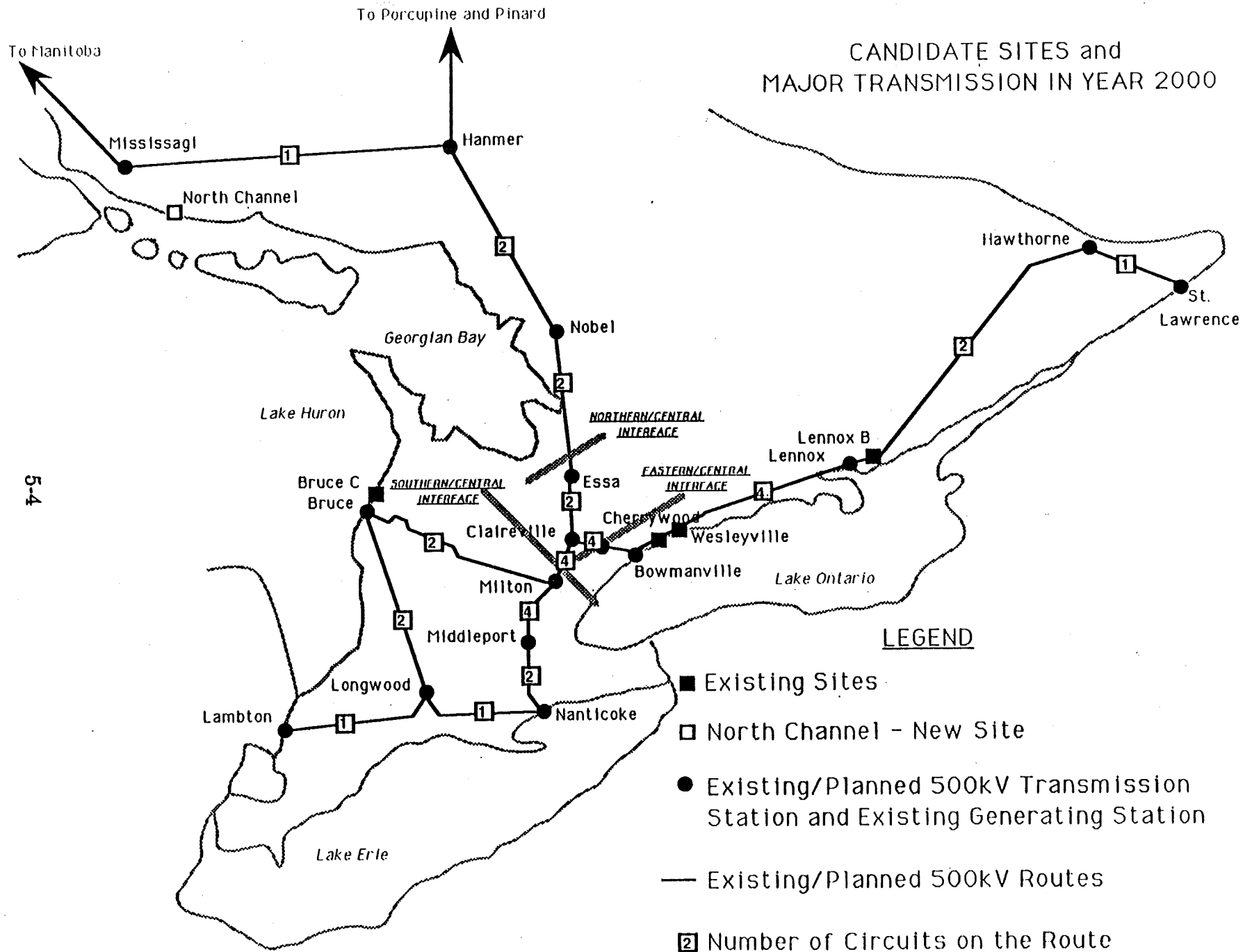
The existing system as of December 31, 1989 plus the following major additions

500 kV Transmission:

1	x	1	cct	-	Milton to Nanticoke	(1992)
1	x	1	cct	-	Lennox to Hawthorne	(1992)
1	x	2	cct	-	Bruce to Longwood	(1990)
1	x	2	cct	-	Claireville to Cherrywood	(1993)
1	x	2	cct	-	Cherrywood to Bowmanville	(1991)
1	x	1	cct	-	Nanticoke to Longwood	(1991)
1	x	2	cct	-	Lennox to Bowmanville	(1994)
1	x	2	cct	-	Milton to Middleport	(1999)
1	x	1	cct	-	Longwood to Lambton	(1996)
1	x	2	cct	-	Milton to Trafalgar	(1996)
1	x	1	cct	-	St.Lawrence to Hawthorne	(1998)

FIGURE 5.2

CANDIDATE SITES and
MAJOR TRANSMISSION IN YEAR 2000



5.2 CRITICAL TRANSMISSION INTERFACES

In the study of large power systems, it has become necessary to identify various "critical interfaces" which define the ability of the system to deliver power from one geographic area to another. Typically, an interface consists of two or more transmission circuits which acting together, transmit power from the area on one side of the interface to the area on the other side. For the purposes of assessing the impact of the major supply plans on the need for bulk transmission reinforcements, three critical interfaces have been defined. These are:

- | | |
|------------------------------|---|
| * Eastern/Central Interface | Flow into Claireville Transformer Station (TS) on the 500 kV circuits from the east |
| * Northern/Central Interface | Flow into Essa TS on the 500 kV circuits from the north |
| * Southern/Central Interface | Flow into Claireville TS on the 500 kV circuits from the southwest |

These interfaces are shown in Figure 5.2.

The following sections outline major factors which influence the loading of the critical interfaces. They also describe the impact the choice of siting and sequencing of the supply options of the Demand/Supply Plan have on the need for inter-area transmission to reinforce these interfaces.

Eastern/Central Interface

Most of the greater Toronto area load is currently supplied radially from Cherrywood TS and Richview TS, and from stations tapped off the six 230 kV circuits crossing the city on the Finch right-of-way. These circuits are also used to carry bulk power transfers across Toronto in parallel with the 500 kV circuits on the Parkway Belt right-of-way. The high rate and magnitude of load growth in the greater Toronto area has greatly increased the loading on the 230 kV circuits on the Finch right-of-way. This is beginning to restrict Hydro's overall ability to transfer power across Toronto. In the near future, it will likely be necessary to open the 230 kV circuits on the Finch right-of-way and use these circuits only for radial load supply. This measure is a logical step in the development of the BES and was applied several years ago to the 115 kV system. Keeping the 230 kV circuits permanently open will increase the loading on the 500 kV transmission on the Parkway Belt between Cherrywood TS and Claireville TS; and, more critically render it the sole transmission path around Toronto.

Hydro plans to increase the transfer capability of the bulk transmission around Toronto by building a second 500 kV line on the existing Parkway Belt right-of-way. This transmission will be in service in 1993. Recent studies have shown that even with this reinforcement, the power transfer capability of the 500 kV transmission across Toronto would be inadequate beyond the year 2000 to fully incorporate the range of demand and supply options being evaluated for the Demand/Supply Plan.

Ontario Hydro has several sites that are available for expansion or do not presently have a station on the site. Most of these sites are on Lake Ontario, east of Toronto. Development of these sites will necessitate the transfer of large amounts of power on the existing 500 kV transmission system around Toronto. These power transfers will vary as a result of daily, weekly and monthly changes in load and generation patterns. The maximum power transfer is expected to approach 40% of the coincident system load with the establishment of just one new major generating station east of Toronto. Under these conditions a large number of customers would be exposed to total interruption of supply for prolonged periods, following a contingency resulting in the loss of all circuits on a right-of-way. A second 500 kV corridor would provide a firm transmission ring around Toronto and ensure an adequate reliability of supply. The timing of this new corridor would not only be influenced by the next new thermal generating station, if it is located east of Toronto, but also by a large purchase from Quebec. Any additional power resources or significant demand management east of Toronto, beyond either of these options, could not be incorporated without this second corridor.

The short circuit current levels on the BES, particularly in the Toronto area, have been steadily increasing as new generation and transmission have been added. The short circuit current levels can be defined as the maximum current that a circuit breaker must interrupt in order to isolate a faulted transmission line or station component from the rest of the BES. This current is many times normal load current. These levels are now approaching the point where they are among the highest experienced by any utility worldwide. The situation will be seriously aggravated by the addition of a new thermal generating station near the greater Toronto area. These very high short circuit levels have placed Ontario Hydro outside the international market provided for by most high voltage circuit breaker manufacturers. Currently, to keep the short circuit levels within the capability of available station equipment, it has been necessary to operate some of our 230 kV stations as two separate stations. Studies show that this measure, or other measures including the use of bus-tie reactors, will need to be extended to most of the BES stations in the Toronto area beyond the year 2000. While operation of a few stations in this manner poses no major problems, the widespread adoption of split station operation is a major concern. It increases operating complexities and could reduce system security and increase production costs. Additional transmission around Toronto and increased transmission redundancy will likely be required to ensure adequate security of the greater Toronto load.

Customer loads in the Regional Municipalities of York and Durham have increased by an average of 7 to 15% annually over the past five years and are expected to exceed the load meeting capability of the existing supply facilities in the area by the mid 1990s. Major transmission reinforcements will be required to maintain a reliable supply to customers in these areas. These reinforcements could be incorporated into a staged development of the proposed bulk transmission reinforcement around Toronto.

Thus, it will be necessary to reinforce the eastern/central interface to increase the reliability of load supply, to ensure security of the power system, and to permit economic utilization of system resources. One approach to this reinforcement is to build a double circuit 500 kV line on a new right-of-way from the Bowmanville SS in Newcastle Township to a new 500 kV transformer station, "Site A" TS, to be established on the existing 500 kV right-of-way between Claireville TS and Essa TS.

Northern/Central Interface

The existing two single circuit 500 kV transmission lines between Hanmer TS and Claireville TS, via Essa TS, provide the capability to transfer power from generation in the north to supply loads in the south, particularly during peak load and generation conditions. At other times, when northern hydraulic generation is not available, these lines provide the capability to supply loads in the north from thermal generation in the south. Hydro plans to increase the flow north and flow south transfer capability of this interface in the mid 1990s by the establishment of a switching station at Nobel near Parry Sound, and by uprating of the existing Essa to Claireville 500 kV lines. The Hanmer to Essa 500 kV lines may also need to be uprated to provide adequate transfer capability in the summer.

Even with these developments, the capability of the northern/central transmission interface will permit incorporation of no more than 2800 MW of new resources in the north. This transfer limit will be exceeded by the following northern resource developments proposed in the Demand/Supply Plan: 1000 MW firm purchase from Manitoba, with provision for an additional 500 MW economy power purchase, 1443 MW of hydraulic developments by 2004, and about 960 MW of non-utility generation developments. Additional transfer capability will be required between the Sudbury area and the Toronto area to incorporate these developments.

One of the candidate sites for the next major new thermal generating station is the North Channel area of Lake Huron. The output of this station, added to the above range of resource developments proposed for northern Ontario, would raise the level of power transfer to supply loads to the south of the northern/central interface to nearly 6000 MW. The existing and planned transmission in place by the turn of the century will not be capable of incorporating the North Channel generating station (GS). Both radial transmission to connect the generating station site to Mississagi

TS and Hanmer TS, and inter-area transmission to reinforce the northern/central interface, will be required to incorporate the new station, whether or not other developments materialize.

One approach to this inter-area transmission reinforcement is to build two single circuit 500 kV lines on a new right-of-way from Hanmer TS to "Site A", a new 500 kV transformer station to be established on the existing 500 kV right-of-way between Claireville TS and Essa TS. Also, build a single circuit 500 kV line on an existing right-of-way from "Site A" TS to Claireville TS.

Southern/Central Interface

The existing and planned transmission reinforcements in southern Ontario will form a strong electrical network for load supply and economic power transactions. Transmission facilities to connect Bruce GS into the London area and reinforcing the transmission between the London and Nanticoke areas will enable the incorporation of the Bruce GS into the Ontario Hydro system. Even after these new facilities are placed in service, a special protection system will still be required at Bruce GS to reject up to two generators during those times when transmission elements in southern Ontario are not available. With the present generation resource allocation in southern Ontario, the capability of the bulk transmission system in the London, Milton and Bruce triangle will be fully utilized by the turn of the century. Hence, radial and inter-area transmission will be required to incorporate additional major generation resources in this triangle prior to the retirement of the existing base load generation resources. With the present load and generation balance in this part of the Ontario Hydro system, new major generation resources are not expected to be added here until after 2008.

5.3 TRANSMISSION REQUIREMENTS - CANDIDATE SITES

The purpose of this section is to provide representative transmission plans for incorporation of the selected fossil and nuclear options in the Plans. Existing and identified sites are considered for illustrative purposes to ensure that cost estimates are realistic and comprehensive.

Site Categories

There are five site categories used in the development of major supply plans. The site categories are:

- a) Existing Station/Sites - Available for Expansion
- b) Existing Sites - Without Station

- c) Existing Station/Sites - Available for Redevelopment
- d) New Identified Sites
- e) New Unidentified Sites

Candidate sites have been used for future fossil and nuclear generating facilities. The intent is not to propose actual, specific sites for generation options, but rather to illustrate that it is technically and economically feasible to site the selected options within the province. Figure 5.2 shows the geographic location of the candidate sites. Figure 5.3 indicates whether new radial and inter-area transmission are needed to incorporate each candidate site within the five site categories.

Transmission Incorporation Requirements

The incorporation of a generating station into the BES could require both radial and inter-area transmission facilities. The following outlines an alternative of the radial and inter-area transmission facilities required to incorporate each of the 12 identified sites and 3 new sites into the Bulk Transmission System for each supply option being considered. These are included for illustrative purposes. The precise configuration of the new transmission, including an assessment of viable alternatives and routing options, will be considered in the respective project specific environmental assessments. The facilities listed assume the candidate site is the first major supply option to be added to the Ontario Hydro system after the incorporation of Darlington 'A' nuclear generating station in 1992. The inter-area transmission facilities should not be used as building blocks for sequencing of stations. The inter-area transmission requirements of the major supply plans depend on many factors other than siting, such as timing, sequencing of siting, load growth and retirements of existing facilities. These factors are dealt with in the formulation of the transmission requirements of each major supply plan in section 5.4.

Figure 5.3
Transmission Requirements for Sites/Options

Site	Generation Option	Transmission Requirements			
		Radial		Inter-area	
		Yes	No	Yes	No
		(1)	(2)	(1)	(2)
Darlington 'B'	CANDU	x		x	
Lambton	CTU/NC (Expansion)		x		x
	CSC (Redevelopment)		x		x
	IGCC (Redevelopment)		x		x
Bruce 'C'	CANDU	x		x	
Hearn	CTU/CC (Expansion)		x		x
	CTU/CC (Redevelopment)		x		x
Keith	CTU/CC (Expansion)		x		x
	CTU/IGCC (Redevelopment) (3)		x		x
Nanticoke	CTU/NC (Expansion)		x		x
Lennox 'A'	CTU/NC (Expansion)		x		x
Lennox 'B'	CSC (Expansion)	x		x	
	IGCC (Expansion)	x		x	
Wesleyville 'A'	CANDU	x		x	
	CSC	x		x	
	IGCC	x		x	
Wesleyville 'B'	CANDU	x		x	
	CSC	x		x	
	IGCC	x		x	
Lakeview	CTU/NC (Expansion) (3)		x		x
	CSC (Redevelopment) (3)		x		x
	IGCC (Redevelopment)		x		x
North Channel	CANDU	x		x	
	CSC	x		x	
	IGCC	x		x	
New Sites	CANDU	x		x	
	CSC	x		x	
	IGCC	x		x	

Notes

- 1 Yes - New lines and/or rights of way are required.
- 2 No - No new lines and/or rights of way are required.
But some upgrading of existing lines and station facilities may be required.
- 3 Site and transmission limitations may restrict the size or number of units for these options

a) **Existing Stations/Sites - Available for Expansion**

Darlington B (4 x 881 MW CANDU)

- Radial - An alternative is to build two double circuit 500 kV lines (less than 1 km) on an existing right-of-way to connect the generating station into the BES at Bowmanville SS. As a minimum, it would also be necessary to build the third double circuit 500 kV line (46 km) between Bowmanville SS and Cherrywood TS on an existing right-of-way and upgrade existing facilities. This alternative would result in some energy being "locked-in" at Darlington under certain conditions.
- Inter-area - New inter-area transmission, as an alternative to the third Bowmanville to Cherrywood line, would enable incorporation of this station with no locked-in energy. For example, a double circuit 500 kV line (175 km) could be built on a new right-of-way from the Bowmanville SS to a new 500 kV transformer station to be established at "Site A" on the existing 500 kV right-of-way between Claireville TS and Essa TS. As this is the preferred alternative for the incorporation of this station, it has been included in the Plan evaluations. A second major station east of Toronto could not be incorporated without this inter-area transmission.

Bruce C (4 x 881 MW CANDU)

- Radial - An alternative is to build two double circuit 500 kV lines (less than 2 km) on a new right-of-way to connect the generating station into the Bruce A & B stations. Also, build a double circuit 500 kV line (150 km) on a new right-of-way to connect the generating station to "Site A" TS, a new 500 kV transformer station on the existing 500 kV right-of-way between Claireville TS and Essa TS.
- Inter-area - New inter-area transmission may also be required. An alternative is to build a double circuit 500 kV line (200 km) on a new right-of-way from Longwood TS to "Site A" TS, a new 500 kV transformer station on the existing 500 kV right-of-way between Claireville TS and Essa TS.

Lambton (up to 4 x 150 MW CTU)

- Radial - Some upgrading of existing 230 kV and 115 kV transmission and station equipment may be required.
- Inter-area - No new inter-area transmission will be required.

Hearn (up to 4 x 150 MW CTU/CC)

- Radial - Some uprating of existing 115 kV transmission and station equipment will be required.
- Inter-area - No new inter-area transmission will be required.

Keith (up to 4 x 150 MW CTU)

- Radial - No new radial transmission will be required.
- Inter-area - No new inter-area transmission will be required.

Nanticoke (up to 4 x 150 MW CTU)

- Radial - No new radial transmission will be required.
- Inter-area - No new inter-area transmission will be required.

Lennox A (up to 4 x 150 MW CTU)

- Radial - No new radial transmission will be required.
- Inter-area - No new inter-area transmission will be required.

Lennox B (4 x 800 MW US Coal CSC or 4 x 660 MW IGCC)

- Radial - An alternative is to build two short double circuit 500 kV lines on an existing right-of-way to connect the generating station into the local existing and planned 500 kV system.
- Inter-area - Inter-area transmission will also be required. An alternative of this transmission is to build the third double circuit 500 kV line (46 km) between Bowmanville SS and Cherrywood TS on an existing right-of-way.

b) Existing Sites - Without Station

Wesleyville A or B (4 x 881 MW CANDU or 4 x 800 MW CSC)

- Radial - An alternative is to build two double circuit 500 kV lines (less than 1 km) on an existing right-of-way to connect the generating station into the 500 kV lines between Bowmanville SS and Lennox TS and build a switching station at the site.
- Inter-area - New inter-area transmission will also be required. The preferred alternative to incorporate the 4 x 881 MW CANDU station is to build a double circuit 500 kV line (175 km) on a new right-of-way from Bowmanville SS to "Site A" TS, a new 500 kV transformer station to be established on the existing 500 kV right-of-way between Claireville TS and Essa TS. However, the first new station east of Toronto could be incorporated by the third double circuit 500 kV line (46 km) between Bowmanville SS and

Cherrywood TS on an existing right-of-way and upgrading of existing facilities. This alternative would result in some locked-in energy at Wesleyville under certain conditions. If either Wesleyville A or B is the second major station east of Toronto, then the preferred inter-area transmission alternative is a definite requirement.

c) Existing Stations/Sites - Available for Redevelopment

Hearn (4 x 150 MW CTU/CC)

- Radial - Some uprating of existing 115 kV transmission and station equipment will be required.
- Inter-area - No new inter-area transmission will be required.

Lambton (4 x 800 MW CSC Coal or 4 x 660 MW IGCC)

- Radial - Some uprating of existing 230 kV transmission and station equipment will be required.
- Inter-area - No new inter-area transmission will be required.

Lakeview (4 x 660 MW IGCC)

- Radial - Some uprating of existing 230 kV transmission and station equipment will be required.
- Inter-area - No new inter-area transmission will be required.

d) New Identified Sites

North Channel (4 x 881 MW CANDU or 4 x 800 MW CSC)

- Radial - An alternative is to build two single circuit 500 kV lines (50 km) on a new right-of-way from the new site to the existing Mississagi TS (near Sault Ste. Marie) and two single circuit 500 kV lines (225 km) on a new right-of-way from the new site to the existing Hanmer TS at Sudbury.
- Inter-area - Inter-area transmission will also be required. An alternative scheme is to build a new 500 kV single circuit line (210 km) on an existing right-of-way from Sault Ste. Marie to Sudbury and two single circuit 500 kV lines (400 km) on a new right-of-way from Hanmer TS to "Site A", a new 500 kV transformer station to be established on the existing 500 kV right-of-way between Claireville TS and Essa TS. Also, build a single circuit 500 kV line (45 km) on an existing right-of-way from "Site A" TS to Claireville TS.

e) New Unidentified Sites in Southwestern Ontario

New Sites (4 x 881 MW CANDU or 4 x 800 MW CSC)

- Radial - An alternative is to build two double circuit 500 kV lines (up to 50 km) on a new right-of-way to connect the generating station into an existing or planned transformer station.
- Inter-area - New inter-area transmission will also be required. An alternative is to build a double circuit 500 kV line (200 km) on a new right-of-way from Longwood TS to "Site A", a new transformer station on the existing 500 kV right-of-way between Claireville TS and Essa TS.

5.4 TRANSMISSION REQUIREMENTS - CANDIDATE PLANS

Criteria for design and evaluation of the Plans are identified in the Demand/Supply Planning Strategy Report. Major supply plans are formulated to satisfy the requirements for peak power and energy established in Chapter 13 of the Demand/Supply Plan Report. The sequence in which sites are developed influences transmission requirements.

Maintaining a regional balance between load and generation reduces, but does not eliminate, the requirement for inter-area transmission facilities. Such balance may exist at peak load times. At other times, large transfers of power in or out of the area may be required as a result of daily, weekly and monthly changes in load and generation patterns. These power transfers may stress critical transmission interfaces and require inter-area transmission reinforcements to ensure security of supply. The timing and sequencing of inter-area transmission will therefore depend on the demand and supply option chosen and its siting. The transmission facilities proposed will allow optimal use of available generation and purchases to permit economic and reliable operation of the Ontario Hydro system.

The transmission requirements for the five candidate plans are based on four transmission schemes, outlined in Figure 5.4. These transmission requirements are provided in Figure 5.5 to 5.9, using the four transmission schemes as building blocks. Figures 5.10 and 5.11 compliment this series of figures by illustrating the two siting sequences considered in developing the transmission requirements, and later, the economic evaluation of demand and supply plans. The transmission schemes are only one alternative and are provided to ensure that transmission costs are captured in the plan evaluation. The capital cost estimates have been developed using typical unit costs for new transmission and include property acquisition, engineering, overheads and contingencies. Interest charges are excluded. In all cases a typical four year cash flow is assumed to apply.

Figure 5.4
Transmission Requirements for Incorporation of Major GS's
(Station Requirements Not Included)

Scheme ID	Description
I	<u>Incorporation of GS at North Channel site:</u> Transmission Facilities Required: - Hanmer TS x Mississagi TS: Build the second 1-cct 500 kV line, approximately 210 km long, on an existing right-of-way - North Channel GS x Mississagi TS: Build two 1-cct 500 kV lines, each about 50 km long, on a new right-of-way - North Channel GS x Sudbury area: Build two 1-cct 500 kV lines, approximately 225 km long, on a new right-of-way - Sudbury area x Toronto area (Site A): Build two 1-cct 500 kV lines, approximately 400 km long, on a new right-of-way. - Toronto area (Site A) x Claireville TS: Build one 1-cct 500 kV line, approximately 45 km long, on an existing right-of-way.
II	<u>Incorporation of GS east of Toronto</u> Transmission Facilities Required:
IIA	- Bowmanville SS x North-west of Toronto (Site A) Build one 2-cct 500 kV line, approximately 175 km long, on a new right-of-way. Each circuit is to be provided with 50% series compensation.
IIB	- Bowmanville SS x Cherrywood TS: Build 3rd 2-cct 500 kV line, approximately 46 km, on an existing approved right-of-way.
Note:	Where the first site developed after Darlington 'A' is east of Toronto, the preferred method of incorporation for a 4x881 MW nuclear GS is by means of Scheme IIA. However, this site could be incorporated by means of the 3rd Bowmanville SS x Cherrywood TS 2-cct 500 kV line and upgrading of existing facilities with some locked-in energy.
III	<u>Incorporation of GS in Southwestern Ontario</u> <u>Site on Lake Erie</u> Transmission Facilities Required: - New GS x Existing 500 kV Station in SWO: Build two 2-cct 500 kV lines, up to 100 km long, on a new right-of-way
IV	<u>Manitoba Purchase</u> Transmission Facilities Required: - Manitoba Border x Sudbury Area: Build one 1-cct 500 kV line, approximately 1000 km long, on a new right-of-way
Note:	This work covers only the facilities required in Ontario. New 500 kV stations will be established at Dryden, Lakehead and midpoint between Lakehead and Mississagi stations. The proposed facilities will displace indefinitely the following planned transmission projects in Northern Ontario: - Birch X Marmion Lake - Marmion Lake x Dryden - Hanmer x Mississagi, 2nd line - Northern Ontario Interconnection Stages I & II

Figure 5.5

Case 15

08/02/90

Transmission Facilities	Costs in 1988 \$M		Lower	In-service Year		Branch Upper	Upper
	Line	Station		Branch Lower	Median		
=====	=====	=====	=====	=====	=====	=====	=====
A) First Site - Darlington 'B'							
Scheme I	688	58	2013	2012	2010	2008	2008
	463	76	2015	2014	2012	2010	2010
Scheme IIA	270	171	2010	2004	2004	2004	2003
Scheme IIB	71	42	2012	2011	2009	2003	2001
Scheme III	308	30					2009
Scheme IV **	576	208	2001	2001	2001	2001	2001
B) First Site - North Channel							
Scheme I	688	58	2010	2004	2004	2004	2003
	463	144	2012	2006	2006	2006	2005
Scheme IIA	270	103	2013	2012	2010	2008	2008
Scheme IIB	71	42	2012	2011	2009	2003	2001
Scheme III	308	30					2009
Scheme IV **	576	208	2001	2001	2001	2001	2001

** Those costs do not include the costs of deferred facilities. See Figure 5.12

Figure 5.6

Case 22

08/02/90

Transmission Facilities	Costs in 1988 \$M		Lower	In-service Year		Branch Upper	Upper
	Line	Station		Branch Lower	Median		
=====	=====	=====	=====	=====	=====	=====	=====
A) First Site - Darlington 'B'							
Scheme I	688	58	2011	2011	2007	2007	2006
	463	76	2013	2013	2009	2009	2008
Scheme IIA	270	171	2008	2002	2002	2002	2002
Scheme IIB	71	42		2013	2011	2011	2001
Scheme III	308	30				2008	2009
Scheme IV **	576	208	2001	2001	2001	2001	2001
B) First Site - North Channel							
Scheme I	688	58	2008	2002	2002	2002	2002
	463	144	2010	2004	2004	2004	2004
Scheme IIA	270	103	2011	2011	2007	2007	2006
Scheme IIB	71	42		2013	2011	2011	2001
Scheme III	308	30				2008	2009
Scheme IV **	576	208	2001	2001	2001	2001	2001

** These costs do not include the costs of deferred facilities. See Figure 5.12.

Figure 5.7

Case 23

08/02/90

Transmission Facilities	Costs in 1988 \$M		Lower	In-service Year			Branch Upper	Upper
	Line	Station		Branch Lower	Median			
=====	=====	=====	=====	=====	=====		=====	=====
A) First Site - Darlington 'B'								
Scheme I	688	58	2011	2003	2003		2003	2003
	463	76	2013	2005	2005		2005	2005
Scheme IIA	270	171	2000	2000	2000		2000	2000
Scheme IIB	71	42	2013	2012	2010		2008	2008
Scheme III	308	30		2013	2011	2009/2013		2009
Scheme IV **	576	208	2001	2001	2001		2001	2001
B) First Site - North Channel								
Scheme I	688	58	2000	2000	2000		2000	2000
	463	144	2002	2002	2002		2002	2002
Scheme IIA	270	103	2011	2003	2003		2003	2003
Scheme IIB	71	42	2013	2012	2010		2008	2008
Scheme III	308	30		2013	2011	2009/2013		2009
Scheme IV **	576	208	2001	2001	2001		2001	2001

** These costs do not include the costs of deferred facilities. See Figure 5.12.

Figure 5.8

Case 24

08/02/90

Transmission Facilities	Costs in 1988 \$M		In-service Year				
	Line	Station	Lower	Branch Lower	Median	Branch Upper	Upper
=====	=====	=====	=====	=====	=====	=====	=====
A) First Site - Darlington 'B'							
Scheme I	688	58	2013	2012	2010	2008	2008
	463	76	2015	2014	2012	2010	2010
Scheme IIA	270	171	2010	2004	2004	2004	2003
Scheme IIB	71	42	2012	2010	2009	2003	2001
Scheme III	308	30				2010	2009
Scheme IV **	576	208	2001	2001	2001	2001	2001
B) First Site - North Channel							
Scheme I	688	58	2010	2004	2004	2004	2003
	463	144	2012	2006	2006	2006	2005
Scheme IIA	270	103			2013	2010	2009
Scheme IIB	71	42	2013	2012	2010	2003	2001
Scheme III	308	30					2013
Scheme IV **	576	208	2001	2001	2001	2001	2001

** These costs do not include the costs of deferred facilities. See Figure 5.12.

Figure 5.9

Case 26

08/02/90

Transmission Facilities	Costs in 1988 \$M		Lower	In-service Year			Upper
	Line	Station		Branch Lower	Medlan	Branch Upper	
=====	=====	=====	=====	=====	=====	=====	=====
A) First Site - Darlington 'B'							
Scheme I	688	58	2013	2012	2010	2008	2008
	463	76	2015 *	2014 *	2012	2010	2010
Scheme IIA	270	171			2009	2004	2003
Scheme IIB	71	42	2010	2011	2004	2003	2001
Scheme III	308	30				2010	2009
Scheme IV **	576	208	2001	2001	2001	2001	2001
B) First Site - North Channel							
Scheme I	688	58	2010	2004	2004	2004	2003
	463	144	2012	2006	2006	2006	2005
Scheme IIA	270	103			2013	2010	2008
Scheme IIB	71	42	2012	2011	2009	2003	2001
Scheme III	308	30					2009
Scheme IV **	576	208	2001	2001	2001	2001	2001

* add \$60 M for station work at southern terminal

** These costs do not include the costs of deferred facilities. See Figure 5.12.

ILLUSTRATIVE SITING AND TIMING OF OPTIONS

SITE	LOAD FORECAST CONDITION	CASE 23		CASE 22		CASE 15		CASE 24		CASE 25	
		Option	In- Service	Option	In- Service	Option	In- Service	Option	In- Service	Option	In- Service
Darlington B	Lower	CANDU A	1999	CANDU A	2007	CANDU A	2009	CANDU A	2009		
	Branch Lower	CANDU A	1999	CANDU A	2001	CANDU A	2003	CANDU A	2003		
	Median	CANDU A	1999	CANDU A	2001	CANDU A	2003	CANDU A	2003		
	Branch Upper	CANDU A	1999	CANDU A	2001	CANDU A	2003	CANDU A	2003		
	Upper	CANDU A	1999	CANDU A	2001	CANDU A	2002	CANDU A	2002		
Hearn	Lower					CTU/CC A	2008	CTU/CC A	2008	CTU/CC A	2008
	Branch Lower			CTU/CC A	2009	CTU/CC A	2009	CTU/CC A	2008	CTU/CC A	2008
	Median			CTU/CC A	2008	CTU/CC A	2001	CTU/CC A	2001	CTU/CC A	2001
	Branch Upper			CTU/CC A	2000	CTU/CC A	2000	CTU/CC A	2000	CTU/CC A	2000
	Upper			CTU/CC B	2003	CTU/CC B	2002	CTU/CC B	2003	CTU/CC B	2003
Keith	Lower										
	Branch Lower										
	Median										
	Branch Upper					CTU/CC B	2002	CTU/CC B	2002	CTU/CC B	2007
	Upper			CTU/CC A	2002	CTU/CC C	2001	CTU/CC A	2002	CTU/CC A	2002
Lakeview	Lower	CTU/IGCC A	2012	CTU/IGCC A	2012	CTU/IGCC B	2012	CTU/IGCC B	2012	CTU/IGCC B	2012
	Branch Lower			CTU/IGCC B	2012	CTU/IGCC B	2012	CTU/IGCC B	2010	CTU/IGCC B	2010
	Median			CTU/IGCC B	2012	CTU/IGCC B	2009	CTU/IGCC B	2008	CTU/IGCC B	2008
	Branch Upper	CTU/IGCC A	2012	CTU/IGCC B	2011	CTU/IGCC B	2008	CTU/IGCC B	2007	CTU/IGCC C	2008
	Upper			CTU/IGCC B	2012	CTU/IGCC B	2012	CTU/IGCC C	2006	CTU/IGCC C	2007
Lambton	Lower										
	Branch Lower										CTU/IGCC C 2012
	Median					CTU/IGCC C	2012	CTU/IGCC C	2010	CTU/IGCC C	2010
	Branch Upper			CTU/IGCC C	2012	CTU/IGCC C	2012	CTU/IGCC C	2012	CTU/IGCC D	2012
	Upper	CTU/NC A	1993	CTU/NC A	1993	CTU/NC A	1993	CTU/NC A	1993	CTU/NC A	1993
Lennox A	Lower										
	Branch Lower										
	Median										
	Branch Upper										
	Upper					CTU/NC C	2001				
Lennox B	Lower										
	Branch Lower										
	Median										
	Branch Upper										
	Upper							CTU/IGCC B	2001	CTU/IGCC B	2002
Nanticoke	Lower										
	Branch Lower										
	Median										
	Branch Upper										
	Upper	CTU/NC B	1994	CTU/NC B	1994	CTU/NC B	1994	CTU/NC B	1994	CTU/NC B	1994

FIGURE 5.10 (CON'T)

ILLUSTRATIVE SITING AND TIMING OF OPTIONS

Darlington B/Wesleyville B Sites Used First for CANDU/CSC Coal

SITE	LOAD FORECAST CONDITION	CASE 23		CASE 22		CASE 15		CASE 24		CASE 26	
		Option	In- Service	Option	In- Service	Option	In- Service	Option	In- Service	Option	In- Service
New Site 1	Lower	CANDU C	2012								
	Branch Lower	CANDU C	2011								
	Median	CANDU C	2009	CANDU C	2010	CANDU C	2012	CANDU B	2012	CSC COAL C	2012
	Branch Upper	CANDU C	2007	CANDU C	2007	CANDU C	2009	CANDU B	2009	CSC COAL C	2009
	Upper	CANDU C	2007	CANDU C	2008	CANDU C	2008	CANDU B	2008	CSC COAL C	2008
New Site 2	Lower										
	Branch Lower	CANDU D	2012								
	Median	CANDU D	2010								
	Branch Upper	CANDU D	2008	CANDU D	2013						
New Site 3	Lower										
	Branch Lower										
	Median										
	Branch Upper	CANDU E	2012								
New Site 4	Lower										
	Branch Lower										
	Median										
	Branch Upper	CANDU F	2012								
North Channel	Lower	CANDU B	2010	CANDU B	2010	CANDU B	2012	CSC COAL A	2012	CSC COAL B	2012
	Branch Lower	CANDU B	2002	CANDU B	2010	CANDU B	2011	CSC COAL A	2011	CSC COAL B	2011
	Median	CANDU B	2002	CANDU B	2006	CANDU B	2009	CSC COAL A	2009	CSC COAL B	2009
	Branch Upper	CANDU B	2002	CANDU B	2006	CANDU B	2007	CSC COAL A	2007	CSC COAL B	2007
	Upper	CANDU B	2002	CANDU B	2005	CANDU B	2007	CSC COAL A	2007	CSC COAL B	2007
Wesleyville A	Lower					CTU/IGCC A	2009	CTU/IGCC A	2009	CTU/IGCC A	2009
	Branch Lower			CTU/IGCC A	2009	CTU/IGCC A	2009	CTU/IGCC A	2009	CTU/IGCC A	2009
	Median			CTU/IGCC A	2009	CTU/IGCC A	2002	CTU/IGCC A	2002	CTU/IGCC A	2002
	Branch Upper			CTU/IGCC A	2002	CTU/IGCC A	2001	CTU/IGCC A	2001	CTU/IGCC A	2001
	Upper	CTU/IGCC A	1997	CTU/IGCC A	1997	CTU/IGCC A	1997	CTU/IGCC A	1997	CTU/IGCC A	1997
Wesleyville B	Lower									CSC COAL A	2009
	Branch Lower									CSC COAL A	2003
	Median									CSC COAL A	2003
	Branch Upper									CSC COAL A	2003
	Upper									CSC COAL A	2002

FIGURE 5.11

ILLUSTRATIVE SITING AND TIMING OF OPTIONS

North Channel Area Site Used First for CANDU/CSC Coal

SITE	LOAD FORECAST CONDITION	CASE 23		CASE 22		CASE 15		CASE 24		CASE 26	
		Option	In- Service	Option	In- Service	Option	In- Service	Option	In- Service	Option	In- Service
Darlington B	Lower	CANDU B	2010	CANDU B	2010	CANDU B	2012				
	Branch Lower	CANDU B	2002	CANDU B	2010	CANDU B	2011				
	Median	CANDU B	2002	CANDU B	2006	CANDU B	2009	CANDU B	2012		
	Branch Upper	CANDU B	2002	CANDU B	2006	CANDU B	2007	CANDU B	2009		
	Upper	CANDU B	2002	CANDU B	2005	CANDU B	2007	CANDU B	2008		
Hearn	Lower					CTU/CC A	2008	CTU/CC A	2008	CTU/CC A	2008
	Branch Lower			CTU/CC A	2009	CTU/CC A	2009	CTU/CC A	2008	CTU/CC A	2008
	Median			CTU/CC A	2008	CTU/CC A	2001	CTU/CC A	2001	CTU/CC A	2001
	Branch Upper			CTU/CC A	2000	CTU/CC A	2000	CTU/CC A	2000	CTU/CC A	2000
	Upper			CTU/CC B	2003	CTU/CC B	2002	CTU/CC B	2003	CTU/CC B	2003
Keith	Lower										
	Branch Lower										
	Median										
	Branch Upper					CTU/CC B	2002	CTU/CC B	2002	CTU/CC B	2007
Lakeview	Upper			CTU/CC A	2002	CTU/CC C	2001	CTU/CC A	2002	CTU/CC A	2002
	Lower	CTU/IGCC A	2012	CTU/IGCC A	2012	CTU/IGCC B	2012	CTU/IGCC B	2012	CTU/IGCC B	2012
	Branch Lower			CTU/IGCC B	2012	CTU/IGCC B	2012	CTU/IGCC B	2010	CTU/IGCC B	2010
	Median			CTU/IGCC B	2012	CTU/IGCC B	2009	CTU/IGCC B	2008	CTU/IGCC B	2008
	Branch Upper	CTU/IGCC A	2012	CTU/IGCC B	2011	CTU/IGCC B	2008	CTU/IGCC B	2007	CTU/IGCC C	2008
Lambton	Upper			CTU/IGCC B	2012	CTU/IGCC B	2012	CTU/IGCC C	2006	CTU/IGCC C	2007
	Lower										
	Branch Lower									CTU/IGCC C	2012
	Median					CTU/IGCC C	2012	CTU/IGCC C	2010	CTU/IGCC C	2010
	Branch Upper			CTU/IGCC C	2012	CTU/IGCC C	2012	CTU/IGCC C	2012	CTU/IGCC D	2012
Lennox A	Upper	CTU/NC A	1993	CTU/NC A	1993	CTU/NC A	1993	CTU/NC A	1993	CTU/NC A	1993
	Lower										
	Branch Lower										
	Median										
	Branch Upper										
Lennox B	Upper					CTU/NC C	2001				
	Lower										
	Branch Lower										
	Median										
	Branch Upper										
Nanticoke	Upper							CTU/IGCC B	2001	CTU/IGCC B	2002
	Lower									CTU/IGCC B	2001
	Branch Lower										
	Median										
	Branch Upper										
Nanticoke	Upper	CTU/NC B	1994	CTU/NC B	1994	CTU/NC B	1994	CTU/NC B	1994	CTU/NC B	1994
	Lower										

FIGURE 5.11 (CON'T)

ILLUSTRATIVE SITING AND TIMING OF OPTIONS

North Channel Area Site Used First for CANDU/CSC Coal

SITE	LOAD FORECAST CONDITION	CASE 23		CASE 22		CASE 15		CASE 24		CASE 26	
		Option	In- Service	Option	In- Service	Option	In- Service	Option	In- Service	Option	In- Service
New Site 1	Lower	CANDU C	2012								
	Branch Lower	CANDU C	2011								
	Median	CANDU C	2009	CANDU C	2010	CANDU C	2012			CSC COAL C	2012
	Branch Upper	CANDU C	2007	CANDU C	2007	CANDU C	2009			CSC COAL C	2009
	Upper	CANDU C	2007	CANDU C	2008	CANDU C	2008	CANDU C	2012	CSC COAL C	2008
New Site 2	Lower										
	Branch Lower	CANDU D	2012								
	Median	CANDU D	2010								
	Branch Upper	CANDU D	2008	CANDU D	2013						
New Site 3	Lower										
	Branch Lower										
	Median										
	Branch Upper	CANDU E	2012								
New Site 4	Lower										
	Branch Lower										
	Median										
	Branch Upper	CANDU F	2012								
North Channel	Lower	CANDU A	1999	CANDU A	2007	CANDU A	2009	CANDU A	2009	CSC COAL A	2009
	Branch Lower	CANDU A	1999	CANDU A	2001	CANDU A	2003	CANDU A	2003	CSC COAL A	2003
	Median	CANDU A	1999	CANDU A	2001	CANDU A	2003	CANDU A	2003	CSC COAL A	2003
	Branch Upper	CANDU A	1999	CANDU A	2001	CANDU A	2003	CANDU A	2003	CSC COAL A	2003
	Upper	CANDU A	1999	CANDU A	2001	CANDU A	2002	CANDU A	2002	CSC COAL A	2002
Wesleyville A	Lower					CTU/IGCC A	2009	CTU/IGCC A	2009	CTU/IGCC A	2009
	Branch Lower			CTU/IGCC A	2009	CTU/IGCC A	2009	CTU/IGCC A	2009	CTU/IGCC A	2009
	Median			CTU/IGCC A	2009	CTU/IGCC A	2002	CTU/IGCC A	2002	CTU/IGCC A	2002
	Branch Upper			CTU/IGCC A	2002	CTU/IGCC A	2001	CTU/IGCC A	2001	CTU/IGCC A	2001
	Upper	CTU/IGCC A	1997	CTU/IGCC A	1997	CTU/IGCC A	1997	CTU/IGCC A	1997	CTU/IGCC A	1997
Wesleyville B	Lower							CSC COAL A	2012	CSC COAL B	2012
	Branch Lower							CSC COAL A	2011	CSC COAL B	2011
	Median							CSC COAL A	2009	CSC COAL B	2009
	Branch Upper							CSC COAL A	2007	CSC COAL B	2007
	Upper							CSC COAL A	2007	CSC COAL B	2007

All Plans include the purchase of electricity from Manitoba. The present purchase arrangements start in 1998 at 200 MW, grow to 1000 MW by 2002, continue at that level until 2018, and conclude in 2022. The transmission required to incorporate the 1000 MW Manitoba Purchase into the Plan is included in all cases. The proposed transmission scheme to incorporate the Manitoba Purchase indefinitely delays several planned load supply transmission projects in northwestern Ontario, as well as planned inter-area transmission between northwestern and northeastern Ontario. These facilities are outlined in Figure 5.12. The net effect of the deferral of these transmission facilities is factored into the Manitoba Purchase as a benefit to Ontario Hydro.

All Plans include the same Hydraulic Program and NUG developments. The transmission required to incorporate these resources will include radial transmission to connect individual stations into the BES and inter-area transmission to ensure security and reliability of power supply, operational flexibility and economic utilization of these resources. The cost of the radial transmission is included in the cost of individual hydraulic station projects. However, the costs of the inter-area transmission have not been included. As these costs are common to all plans their exclusion does not alter the economic comparison between plans.

The four transmission schemes are common to all the candidate plans. Their in-service dates are influenced however by load growth, choice of option, geographic location and sequencing of siting. All of these influencing factors must be viewed collectively when assessing the transmission developments required by each candidate Plan.

Load Growth

Each Major Supply Case was tested against the bandwidth forecast, consisting of five load paths.

Under the lower load growth options, where in-service dates of major supply options are farther out in the planning time frame, transmission facilities that are freed up because of retirement of existing generating resources can be utilized to incorporate the new supply options.

Under the high load growth options, the existing and proposed transmission reinforcements are fully utilized. To incorporate the additional options required under the upper load growth, new unidentified generation sites and incorporating transmission are required. Sites to the southwest and northwest of Toronto are preferred for these upper load growth options. Incorporation of these sites would require reinforcing of the southern/central transmission interface. Because of the uncertainties associated with the siting within this geographic area and the already strained state of this transmission system, a representative transmission

Figure 5.12

Cost and Timing of Facilities in Northern Ontario
Deferred Indefinitely by Manitoba Purchase

08/02/90

Facility	Costs in 1988 \$M		In-service Year without Manitoba Purchase				
	Line Costs	Station Costs	Lower	Branch Lower	Median	Branch Upper	Upper
2nd Hanmer x Mississagi 500 kV	94	4	2013	2009	2005	2002	1999
Birch x Marmion Lake	101	9	2005	2000	2000	2000	1997
Marmion Lake x Dryden	89	5	2011	2009	2005	2003	2001
Northern Ontario Int. St I	318	78	2015	2012	2006	2003	2000
Northern Ontario Int. St II	299	10	2023	2023	2015	2005	2005

reinforcement was specified for the planning studies. Since sites to the southwest and northwest of Toronto are not proposed to be utilized until late in the 25-year planning time frame, the transmission reinforcements specified take into account the unloading of the transmission system that would result from the retirement of existing generation resources.

Choice of Option

The set of illustrative sites for each Case represents a feasible choice and meets the planning requirement for a geographic balance between electricity demand and supply. Darlington 'B' and North Channel are used as reference sites for CANDU stations. Wesleyville 'B' is used as a reference site for a CSC coal station. In those Cases where North Channel is not used for a nuclear station, it is a reference site for a CSC coal station. Wesleyville 'A' and Lennox 'B' are reference sites for CTU/IGCC.

Siting - Geographic Location/Sequencing

To achieve geographic balance between load and generation, the major supply options are initially sited in eastern and northern Ontario. The inter-area transmission reinforcements triggered by this choice of site would be eastern/central and northern/central, respectively. To investigate the impact of choice of site on these inter-area transmission links, two options for the siting of the first base load station in each of the five selected Cases were chosen:

- Darlington/Wesleyville
- North Channel.

For the eastern/central reinforcement, the option chosen for the first site developed east of metro Toronto has an impact on the extent of the transmission reinforcements required, and ultimately, on the costs. The eastern/central reinforcements are designed to achieve many system goals, including the incorporation of the demand and supply options. Economical use of available resources is one of these system goals. An assessment of the resources available to the system and those options outlined in the five Cases, shows that to achieve the operational and economic objectives for the BES, the following guidelines are appropriate in determining the eastern/central transmission interface reinforcements.

Option	Additional Generation East of metro Toronto	Transmission Reinforcements
fossil	less than 1500 MW	nil
fossil	up to 5000 MW	Scheme IIB
fossil	5000 MW to 7500 MW	Scheme IIA & IIB
nuclear	up to 5000 MW	Scheme IIA
nuclear	5000 MW to 7500 MW	Scheme IIA & IIB

Additional generation east of Toronto beyond 7500 MW will require further reinforcement of the eastern/central interface and possible reinforcement of the southern/central interface.

For the northern/central transmission reinforcement, the impacts of the hydraulic program, non-utility generation and the Manitoba Purchase have to be considered collectively to determine the incorporation requirements for the selected option. The following resource additions in northern Ontario are expected over the 25-year planning time frame:

Resource Addition	Installed Capability
Hydraulic Program	2300 MW (by 2014)
Non-utility generation	1340 MW (by 2014)
Manitoba Purchase	1000 MW (2002 to 2018)

Taking into account the proposed transmission reinforcements, upgrades to existing facilities and stability enhancing devices, the northern/central interface will permit only one major supply option to be incorporated at the North Channel site. For this reason, it was decided to limit the North Channel site to the base load options (nuclear, CSC coal or IGCC).

The development of a transformer station at "Site A", to terminate the northern/central and eastern/central reinforcements in the existing 500 kV right-of-way between Claireville TS and Essa TS, is common to both of these reinforcements and is allocated for costing purposes to the first reinforcement placed in-service.

Comparison of Cases

Case 15 - Proposed Plan

The choice of the initial base load site, whether in eastern or northern Ontario, does not alter the total transmission reinforcements required over the 25-year planning time frame. However, the choice of first site does affect total transmission costs, due to the relative costs of the northern/central and eastern/central inter-area transmission reinforcements, the extensive radial transmission for the North Channel site and the time value of money. Under the upper load growth path, an additional site and associated incorporating transmission are required in southern Ontario.

Case 22

The choice of initial siting does not impact the total transmission reinforcements required. Under the lower load growth path, one less inter-area transmission link is required than under the same conditions for Case 15. However, an additional site in southern Ontario and associated transmission is required under the branch upper load growth path as well as the upper load growth path.

Case 23

The choice of initial siting does not impact the total transmission reinforcements required. An additional site in southern Ontario and associated transmission is required under all load growth paths except the lower load growth. Two additional sites are required in southern Ontario under the branch upper load growth path.

Case 24

Under the branch upper load growth path, an additional site is required in southern Ontario when the first site utilized is in eastern Ontario. When the first site is in northern Ontario, the major transmission reinforcements between eastern and central Ontario are not required for the lower and branch lower load growth paths.

Case 26

The major transmission reinforcements between eastern and central Ontario are not required for the lower and branch lower load growth paths. Under the branch upper load growth path, an additional site is required in southern Ontario, when the first site utilized is in eastern Ontario.

Summary

A major factor in determining the siting for the base load plants is the geographic balance between load and generation. To achieve this, it is preferable to limit base load expansion east of Toronto to one station at the beginning of the 25-year planning period. It is preferable to limit the North Channel development to one base load station, because of load distribution and transmission considerations. Prior to retirements of base load plants east of Toronto (2011), locations for base load stations southwest and northwest of Toronto would also be required under the upper load growth path for all Cases.

The transmission requirements to incorporate the North Channel site into the BES are approximately four times as costly as those for sites east of metro Toronto. While unit transmission costs are expected to be greatest in and around the greater Toronto area, the shorter distances and the common transmission reinforcements between the northern/central and eastern/central reinforcements more than offset the higher unit costs of the eastern/central transmission reinforcements. The lower total cost for the eastern/central transmission reinforcements is of particular significance, when comparing the impact of siting of the first base load option between eastern and northern Ontario.

5.5 REVIEW

The siting of generation has an impact on the nature, timing and sequence of transmission system reinforcements. The transmission required to incorporate a new Ontario Hydro generating station will include radial transmission necessary to connect the site to the existing and planned Bulk Electricity System (BES). It may also include inter-area transmission necessary to maintain an integrated BES. The inter-area transmission facilities described in this chapter are those influenced by the demand and supply options and are not meant to be a comprehensive list of the Bulk Transmission System additions required over the 25-year life of the Demand/Supply Plan.

Illustrative transmission for the incorporation of generating stations at the candidate sites is provided to ensure that transmission costs are captured in the plan evaluation. The precise configuration of the new transmission, including an assessment of viable alternatives, will be considered in the project specific environmental assessments.

Approvals sought in the Demand/Supply Plan Report include the need for radial transmission. Specific routes for this radial transmission will be assessed as part of the project specific environmental assessment for each generation development. Approvals for inter-area transmission reinforcements will be sought in separate parallel environmental assessment processes.

Consolidation of the eastern/central and northern/central inter-area transmission reinforcements into a single environmental assessment meets the incorporation requirements of the candidate plans, and offers significant advantages for the development of the integrated bulk electricity system:

- It provides the flexibility to disperse additional generation across the province (Demand/Supply Planning Strategy Element 5.4). More particularly, it enables the next new generating station to be located either on the North Channel or east of Toronto.
- It provides the opportunity for a staged development since, the in-service dates for the two transmission reinforcements are interdependent, and part of the right-of-way and facilities for the two inter-area transmission reinforcements could be common.
- It enables approvals under the Environmental Assessment Act to be sought for a total transmission development plan which is consistent with the Demand/Supply Plan.

6. ENERGY PRODUCTION

6.0 INTRODUCTION

6.1 OPERATING STRATEGY

6.2 FUEL CONSUMPTION

6.3 ENERGY PRODUCTION RESULTS

6.4 ENERGY DIVERSITY BY SOURCE AND FUEL

6.5 REVIEW

6.0 INTRODUCTION

To assess the economic and environmental impacts of demand/supply plans, it is necessary to consider:

1. energy production, and the amount of fuel required to produce that energy;
2. energy acquired through purchases from US and Canadian utilities, and non-utility generators; and
3. regulatory limits on acid gas emissions, which apply to the generating system as a whole. These limits influence the application of emission control technologies and the choice of fossil fuels, such as bituminous coal, lignite, natural gas and oil.

As noted in Chapter 4, five Cases were formulated. All five Cases require new major supply facilities.

The timing and nature of new supply additions (hydraulic, nuclear, fossil, purchases) influence the way the entire system can be operated. Hence, the pattern of energy production and fuel consumption changes between Cases.

6.1 OPERATING STRATEGY

Ontario Hydro generating stations are fuelled with one of five energy sources: uranium, coal, oil, gas and falling water. Each station's production is driven by the system operating strategy, which is to minimize the total cost of providing electricity to customers. This is done, whenever possible, by using the lowest cost energy sources first, provided environmental requirements and standards are met. Cost in this instance includes the variable costs of fuel and of operations. Capital costs and financing charges already incurred are not included, as they do not influence how a station is operated.

The order of generation, by least operating cost, is hydraulic, nuclear and fossil. Based on past experience and current economic considerations, it is generally best to match demand needs and generating options as follows:

1. Base load - nuclear units and hydraulic units that have limited storage capabilities,
2. Intermediate load - coal-fired units, and
3. Peak load - oil-fired, natural gas-fired and hydraulic units with storage capabilities. Hydraulic peaking stations have extra value because of their quick response to changing demand.

Electricity purchases and non-utility generation are also contracted to meet base load or intermediate load and, on some occasions, to maintain adequate operating reserves.

6.2 FUEL CONSUMPTION

The calculation of fuel consumption is performed with computer modelling. The model takes into account available supply facilities and their characteristics, and the characteristics of the load, as explained in Chapter 2.

Load characteristics include the effects of demand management and load displacement non-utility generation.

The model of available supply facilities includes purchases from utilities and non-utility generators, the existing system and new supply additions. Supply characteristics that influence operation include:

1. Performance of operating units such as generator outage rates,
2. Natural constraints such as water availability, and
3. Environmental constraints such as acid gas emission regulations.

By determining time of use and fuel employed, the model calculates fuel costs and emissions for every station in the plan. If the results are poor in one or both areas -- for example, acid gas emissions above regulatory limits -- the nature of the plan is revised as described in Chapter 4.

Fuel cost and emission data are used in a number of additional evaluations. Fuel consumption figures are employed to examine fuel supply implications, range of costs, electricity rates, provincial economy impact and environmental impacts (wastes, water use, mining activity, etc.). Emissions are a starting point for the environmental review.

6.3 ENERGY PRODUCTION RESULTS

Calculations of energy production and fuel consumption have been made for all five Cases under each of the five load forecast paths. The lower, branch lower, median, branch upper and upper load paths are discussed for each energy source: utility purchases, non-utility generation, hydraulic, nuclear and fossil.

6.3.1 Energy From Utility Purchases

Figure 6-1 shows the annual energy purchased from other utilities. This is assumed in all Cases and load paths.

All five Cases feature the purchase of electricity from Manitoba. The present purchase arrangements start in 1998 at 200 MW, grow to 1000 MW by 2002, continue at that level until 2018, and conclude in 2022.

The purchase begins in November 1998. However, because of the time periods used in the model, it is assumed to begin in 1999. Energy from the Manitoba Purchase reaches about 7 TW.h per year by 2003, and continues at that level to the end of the planning period.

6.3.2 Energy From Non-utility Generation Purchases

Figure 6-2 shows the annual energy supplied by non-utility generation purchases in all five Cases under the five load forecast paths. The estimates represent net energy purchased by Ontario Hydro. There are some non-utility generators which generate electricity to supply part or all of their own load without any net sale of power to Ontario Hydro. Because electricity produced by these "load displacement" projects has been accounted for in the primary load forecast, it is not included here.

Energy from non-utility generators increases steadily to about 3 TW.h per year by 1994 under all load paths. Thereafter, under median load forecast, energy production continues to climb, reaching about 11 TW.h per year by 2014.

Under lower load forecast, energy production levels off at about 3 TW.h per year for several years, until about 2003. Thereafter, energy production increases steadily, reaching about 7 TW.h per year by 2014.

Energy production under upper load forecast is slightly higher than under median load forecast after 1994, by about 1 TW.h per year.

After 2000, energy purchased from non-utility generators under branch lower and branch upper load forecasts begins to differ from the median load forecast. Energy under the branch lower load path levels off at about 6 TW.h per year until 2009, then rises to over 7 TW.h per year by 2014. Energy under the branch upper load path is higher than under the median load path after 2000, and reaches the same level as under the upper load path by 2005.

FIGURE 6-1
ENERGY FROM UTILITY PURCHASES
(FOR ALL CASES & LOAD FORECASTS)

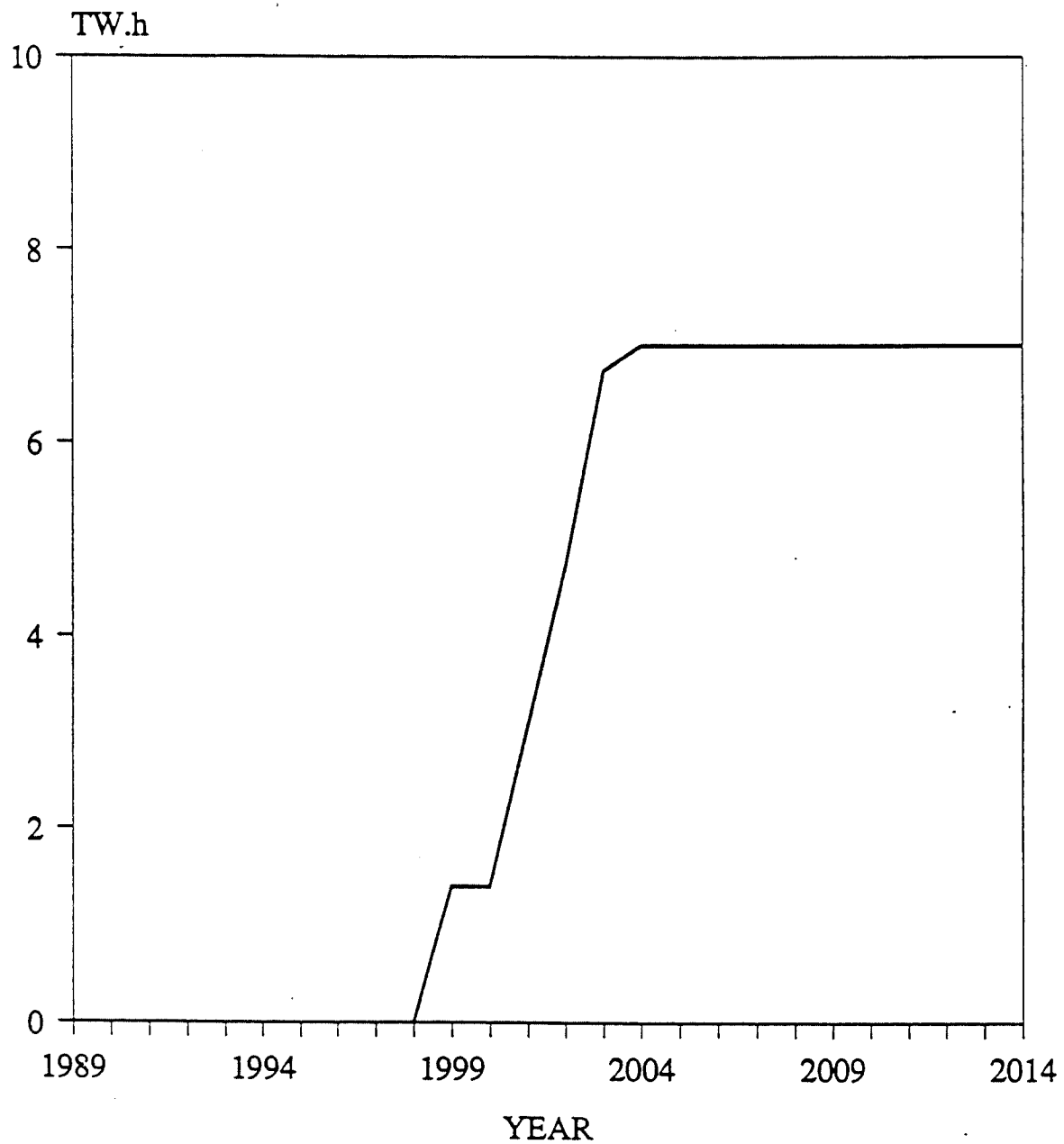
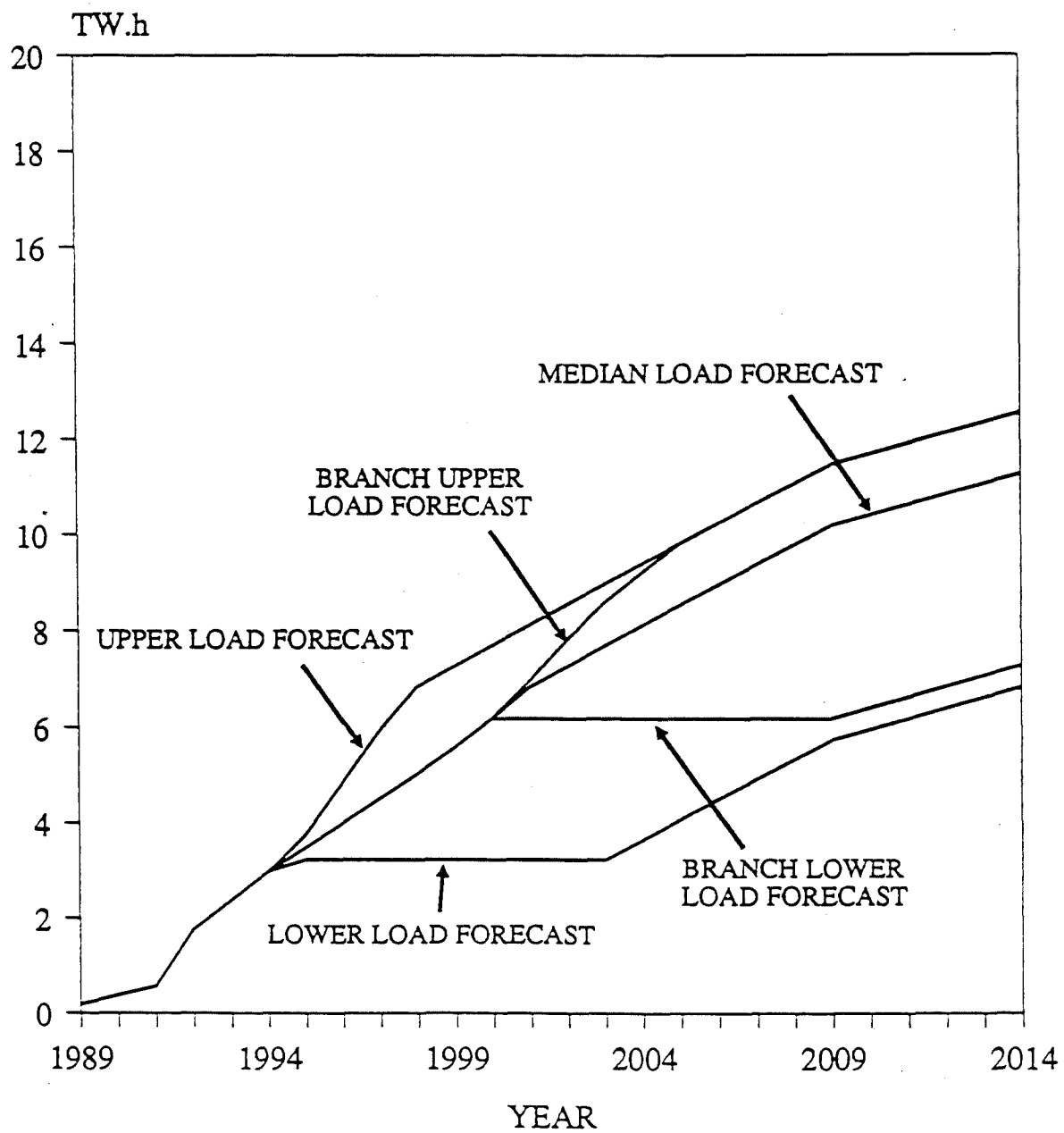


FIGURE 6-2
ENERGY FROM NON-UTILITY GENERATION
(FOR ALL CASES)



6.3.3 Hydraulic Energy Production

Figure 6-3 shows the annual hydraulic energy production. The hydraulic development program, and the energy production it contributes, is the same for all five Cases and load forecast paths.

Annual energy production from hydraulic generation grows steadily from 36 TW.h in 1989 to about 41 TW.h per year by 2014. Under all load conditions, Ontario Hydro's operating strategy is to maximize the use of this renewable resource.

6.3.4 Nuclear Energy Production

Figures 6-4(a) through 6-4(e) show the annual nuclear production for the five Cases under all five load paths.

The variation between Cases under each load path is mostly due to the in-service dates for new nuclear facilities. Since nuclear stations are operated as often as possible under any load condition, all Cases have the same amount of nuclear energy production up until 1999, when Case 23 is the first to have a new nuclear facility placed in-service.

Nuclear energy production under the five load forecast paths exhibits similar patterns, but the quantity of energy produced differs. From 1989 to 1996, energy production rises as Darlington comes into service and existing nuclear units, unavailable during retubing, are returned to service.

The dips in energy production are a result of retubing one or two generating units at times and retirement of Pickering GS A units beginning in 2011. In some instances, the effects of retubing and retirements are masked by new nuclear generation coming into service.

Median Load Forecast

Under median load forecast, Cases 15, 22 and 23 produce about 140 to 160 TW.h of nuclear energy per year by 2014. Case 24 has a conventional steam cycle coal station coming into service from 2009. Nuclear production in Case 24 is therefore lower than in the other three Cases, reaching about 120 TW.h per year by 2014. Case 26 has no new nuclear generation added. Nuclear energy production gradually falls from about 100 TW.h per year in 2007 to present day levels of about 80 TW.h per year by 2014, mostly because of retirements of Pickering GS A units.

FIGURE 6-3
HYDRAULIC ENERGY PRODUCTION
(FOR ALL CASES & LOAD FORECASTS)

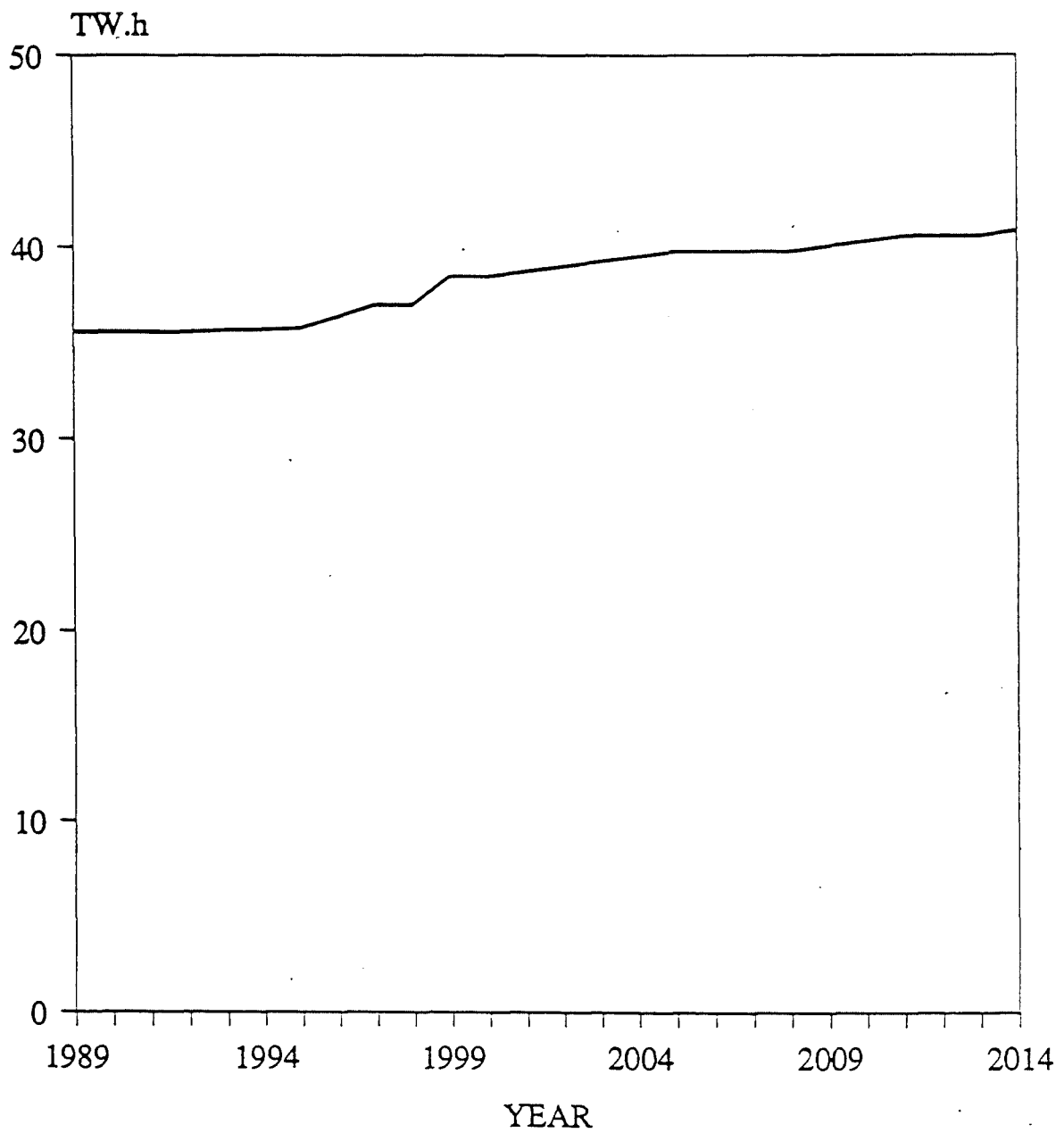


FIGURE 6-4(a)
NUCLEAR ENERGY PRODUCTION
(LOWER LOAD FORECAST)

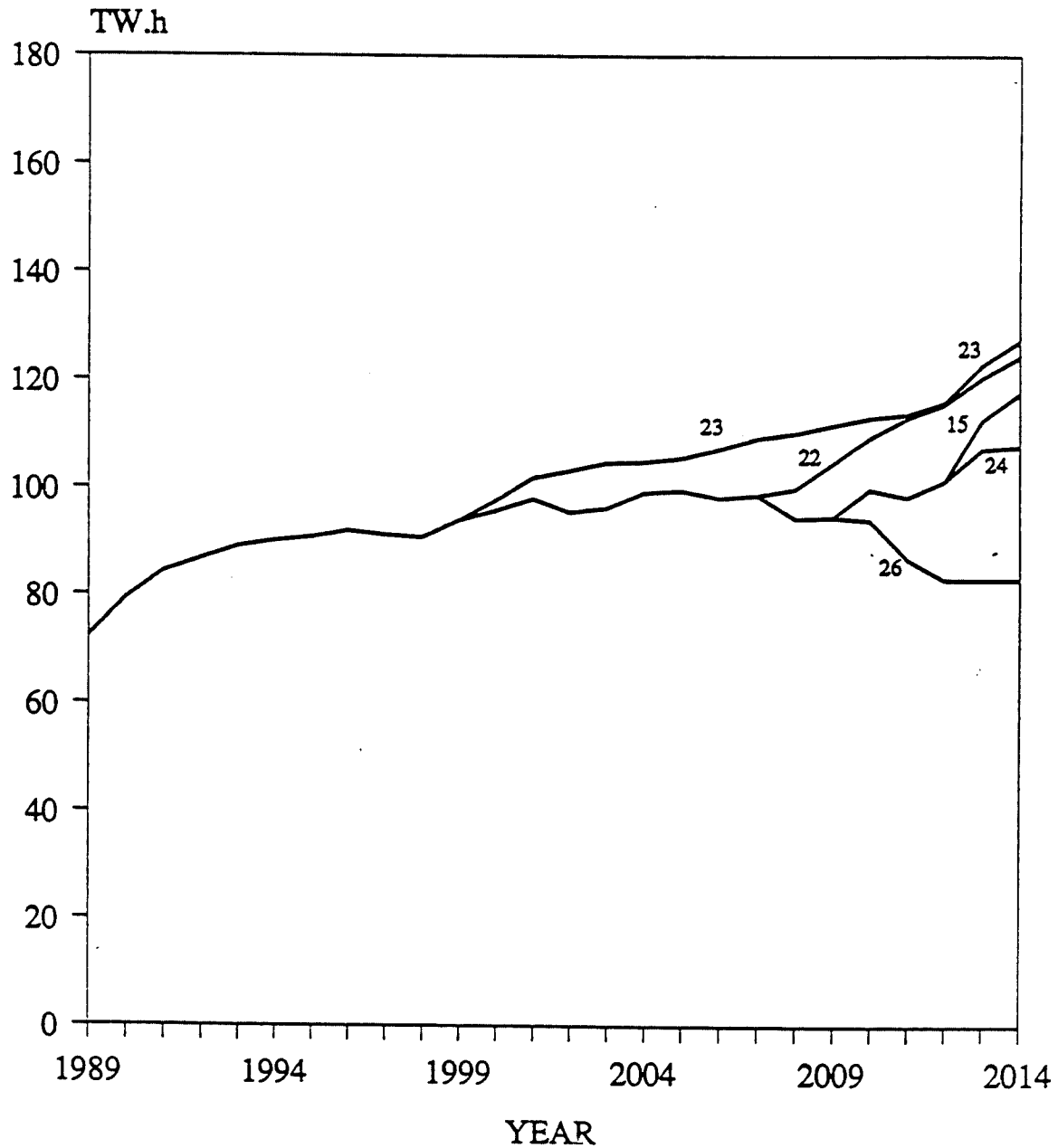


FIGURE 6-4(b)
NUCLEAR ENERGY PRODUCTION
(BRANCH LOWER LOAD FORECAST)

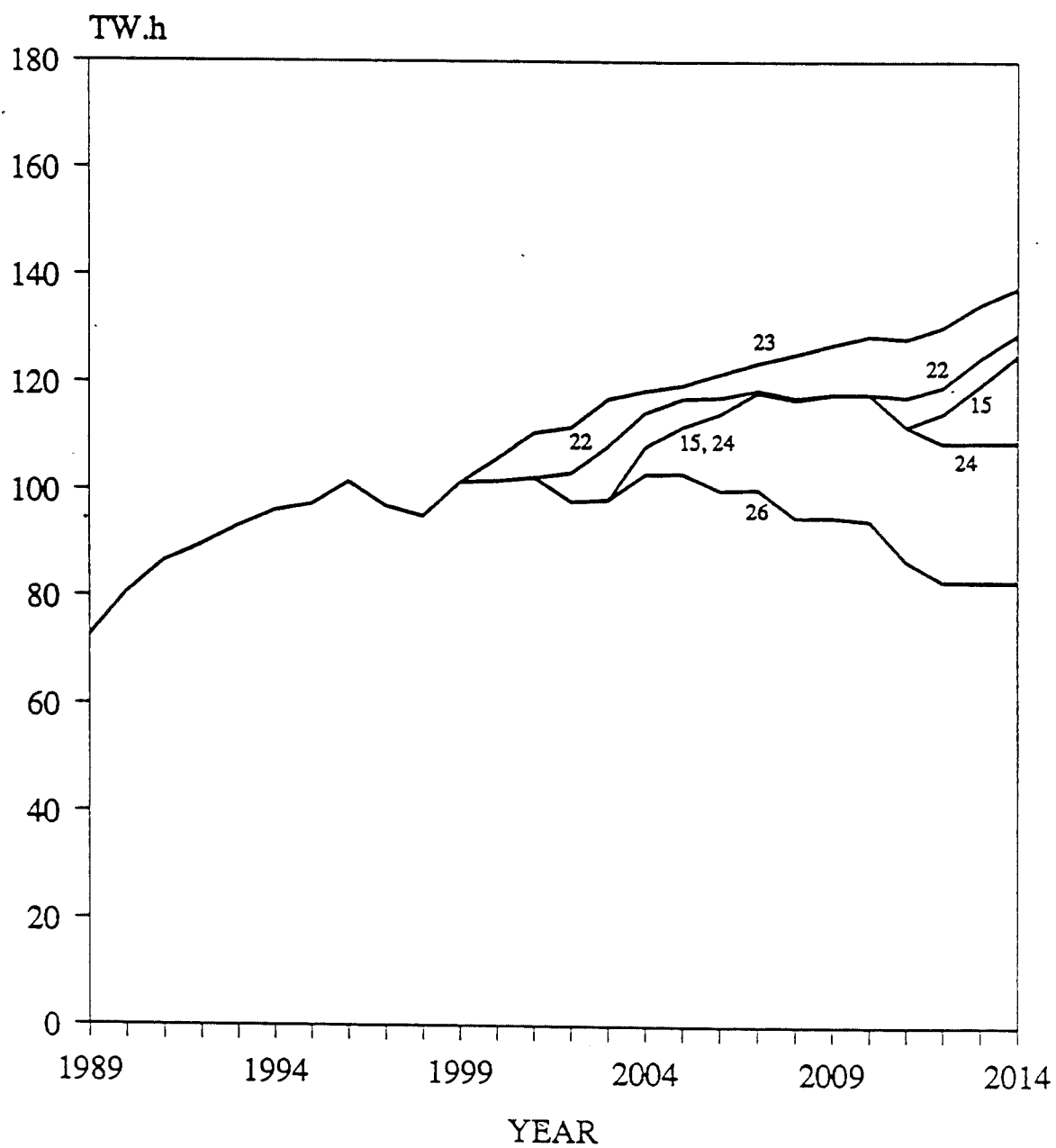


FIGURE 6-4(c)
NUCLEAR ENERGY PRODUCTION
(MEDIAN LOAD FORECAST)

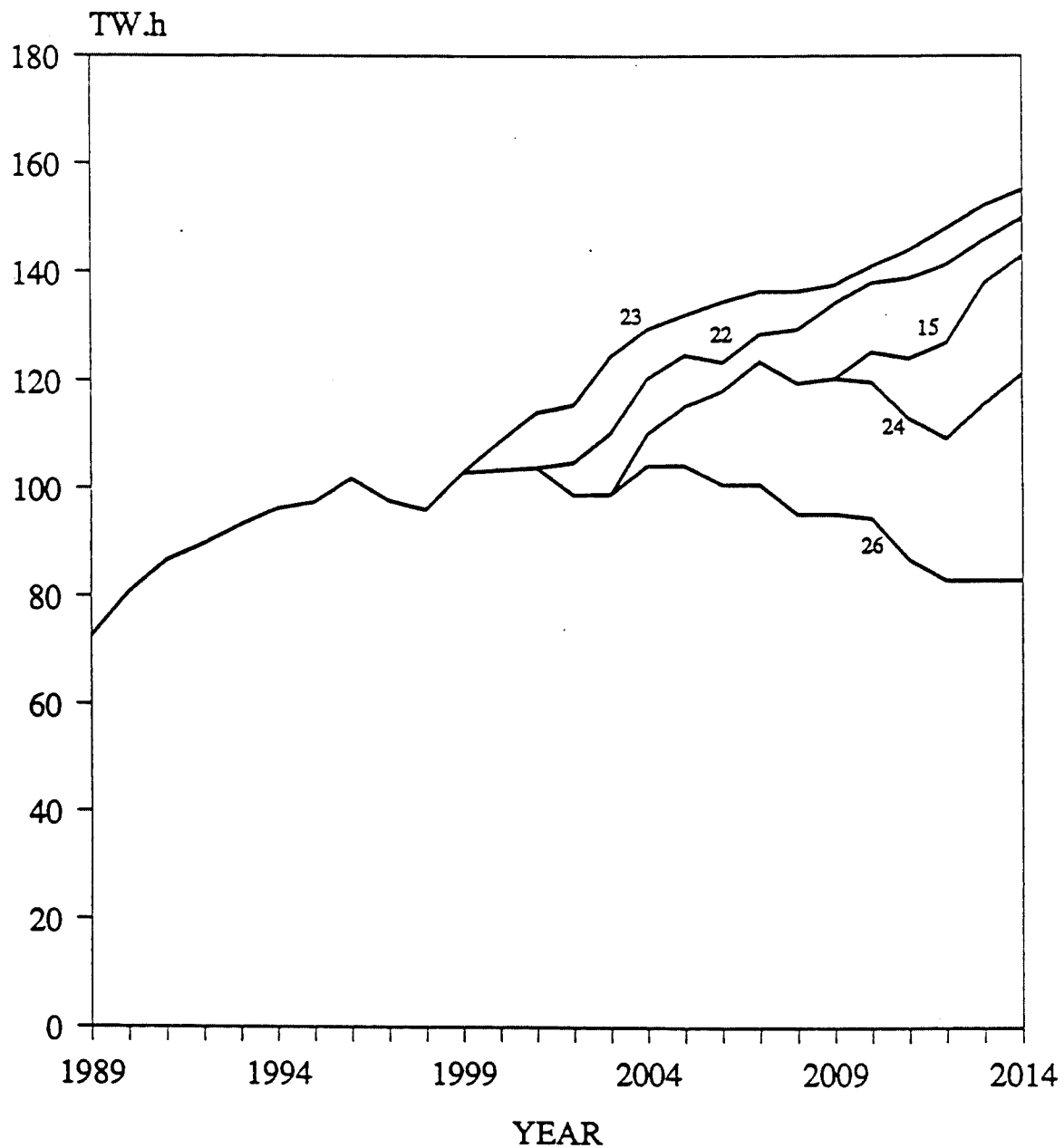


FIGURE 6-4(d)
NUCLEAR ENERGY PRODUCTION
(BRANCH UPPER LOAD FORECAST)

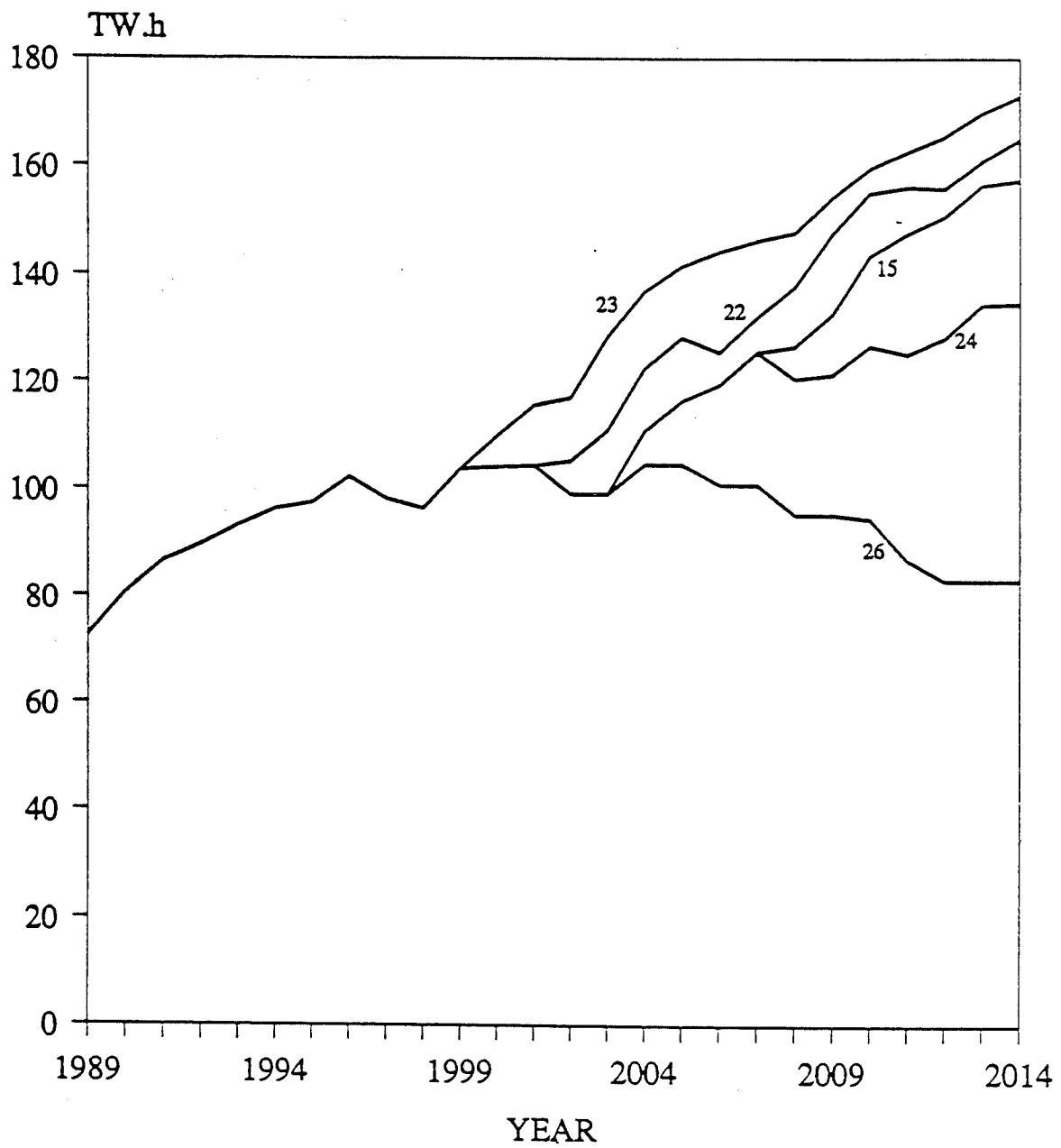
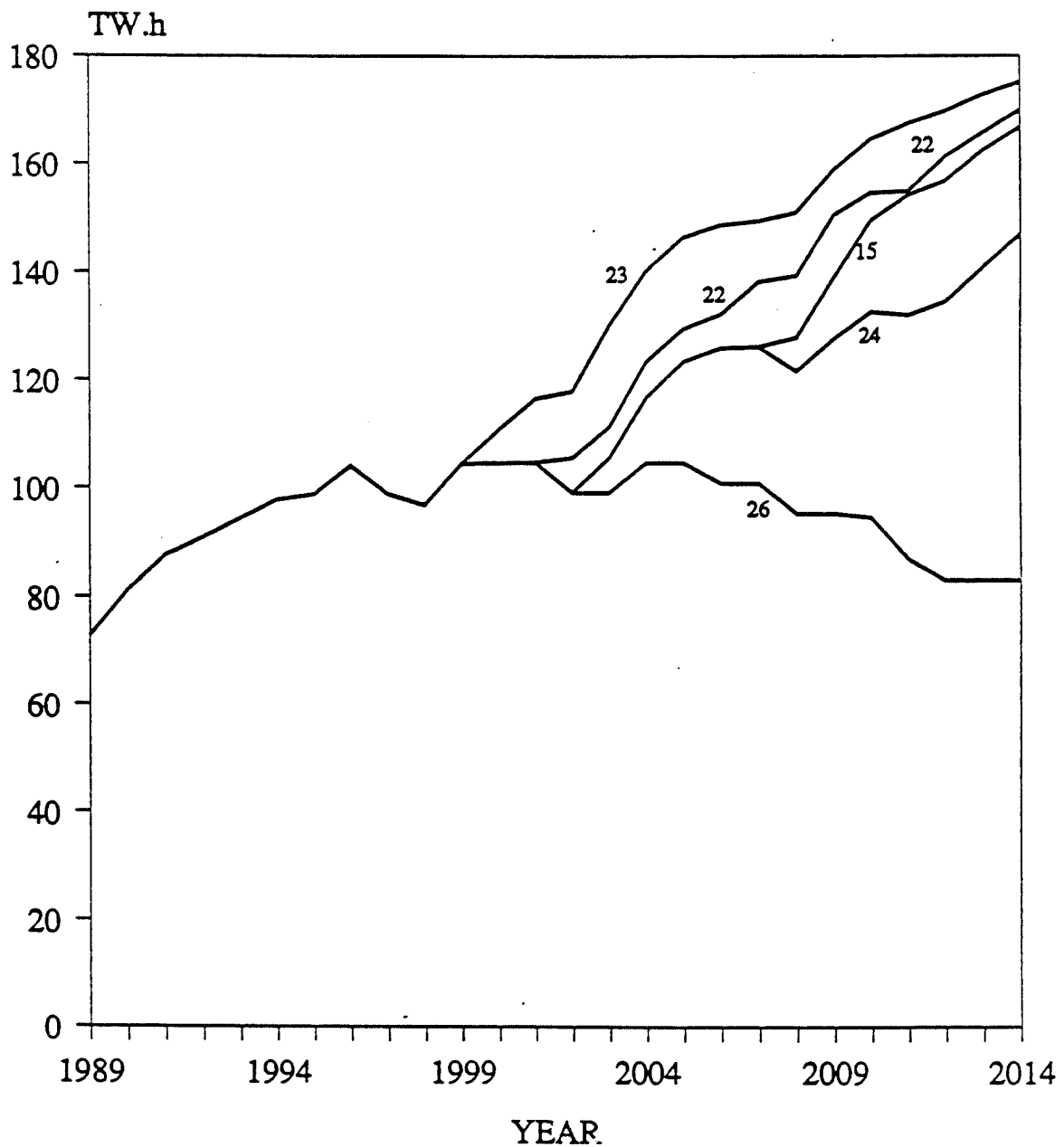


FIGURE 6-4(e)
NUCLEAR ENERGY PRODUCTION
(UPPER LOAD FORECAST)



Lower Load Forecast

Under lower load forecast, nuclear energy production rises as Darlington comes into service. Compared to other load paths, there are fewer dips in energy production because nuclear capability is not quite fully utilized in the 1990s, which masks the unavailability of units out of service for retubing.

By 2014, Cases 15, 22 and 23 produce about 120 TW.h of nuclear energy per year. Case 24 lags by 10 TW.h, reaching about 110 TW.h per year by 2014. Case 26 is the same as under the median load forecast, producing about 80 TW.h per year by 2014.

Branch Lower Load Forecast

Under branch lower load forecast, Cases 15, 22 and 23 produce about 130 TW.h of nuclear energy per year by 2014. In Case 24, energy production is 20 TW.h lower at about 110 TW.h per year. Case 26 produces the same 80 TW.h of nuclear energy per year by 2014.

Branch Upper Load Forecast

Under branch upper load forecast, Cases 15, 22 and 23 produce about 160 TW.h of nuclear energy per year by 2014. Energy production in Case 24 rises to about 130 TW.h per year and Case 26 produces the same 80 TW.h of nuclear energy per year by 2014.

Upper Load Forecast

Under upper load forecast, Cases 15, 22 and 23 produce about 170 TW.h of nuclear energy per year by 2014. Case 24 reaches about 150 TW.h per year by 2014. Case 26 remains the same as under other load forecasts, generating about 80 TW.h of nuclear energy per year by 2014.

6.3.5 Fossil Energy Production

Fossil energy is derived from a number of fuels: US bituminous coal, Western Canadian bituminous and lignite coal, natural gas and oil. In this section, the total fossil fuel consumption is shown. Later, in the discussion of acid gas control measures in Chapter 7, the breakdown of fossil fuel use is presented.

Fossil energy production varies more widely than the other supply options. This is because fossil generation is generally used to meet demands after contracted utility and non-utility purchases, hydraulic and nuclear generation are fully utilized. Figures 6-5(a) through 6-5(e) illustrate the annual fossil energy production for the five Cases under the five load paths.

Primarily, fossil energy production fluctuates with nuclear production -- rising during nuclear retubing, falling when nuclear comes into service. The variation in fossil energy production between Cases is due to the timing and type of supply additions. The pattern of the variation between Cases is generally similar across all load paths. The main difference under different load forecasts is the level of energy production.

Median Load Forecast

Under median load forecast, fossil energy production in all five Cases starts at about 28 TW.h per year in 1989, then drops to the 20 TW.h per year level as Darlington comes into service in the early 1990s. During the late 1990s, annual fossil energy production ranges from 16 TW.h to 26 TW.h. After 1999, the five Cases begin to exhibit different fossil production.

Case 26 has the highest fossil energy production, increasing steadily from a low of about 19 TW.h per year in 1999 to about 73 TW.h per year by 2014.

Cases 15 and 24 show similar fossil production up to 2009. Fossil energy production rises from about 19 TW.h per year in 1999 to about 34 TW.h per year by 2003. The new nuclear station coming into service in 2003 reduces fossil energy production to about 23 TW.h per year by 2009. After 2009, the two Cases diverge in their fossil production. In Case 15, a second nuclear station is added and fossil energy production falls to about 13 TW.h per year by 2014. Case 24 has a new conventional steam cycle coal station coming into service in 2009. Fossil energy production peaks at about 41 TW.h per year in 2012, then dips to 35 TW.h per year by 2014 as the second nuclear station is added.

In Case 22, fossil energy production increases from about 19 TW.h per year in 1999 to a peak of about 27 TW.h per year in 2002. As new nuclear facilities are added, fossil energy production falls to about 6 TW.h per year by 2014.

Case 23 has the lowest amount of fossil generation. The two new nuclear stations starting in 1999 and in 2002 reduce fossil production in the 2000s. Fossil energy production declines steadily from about 19 TW.h per year in 1999 to less than 1 TW.h per year by 2014.

FIGURE 6-5(a)
FOSSIL ENERGY PRODUCTION
(LOWER LOAD FORECAST)

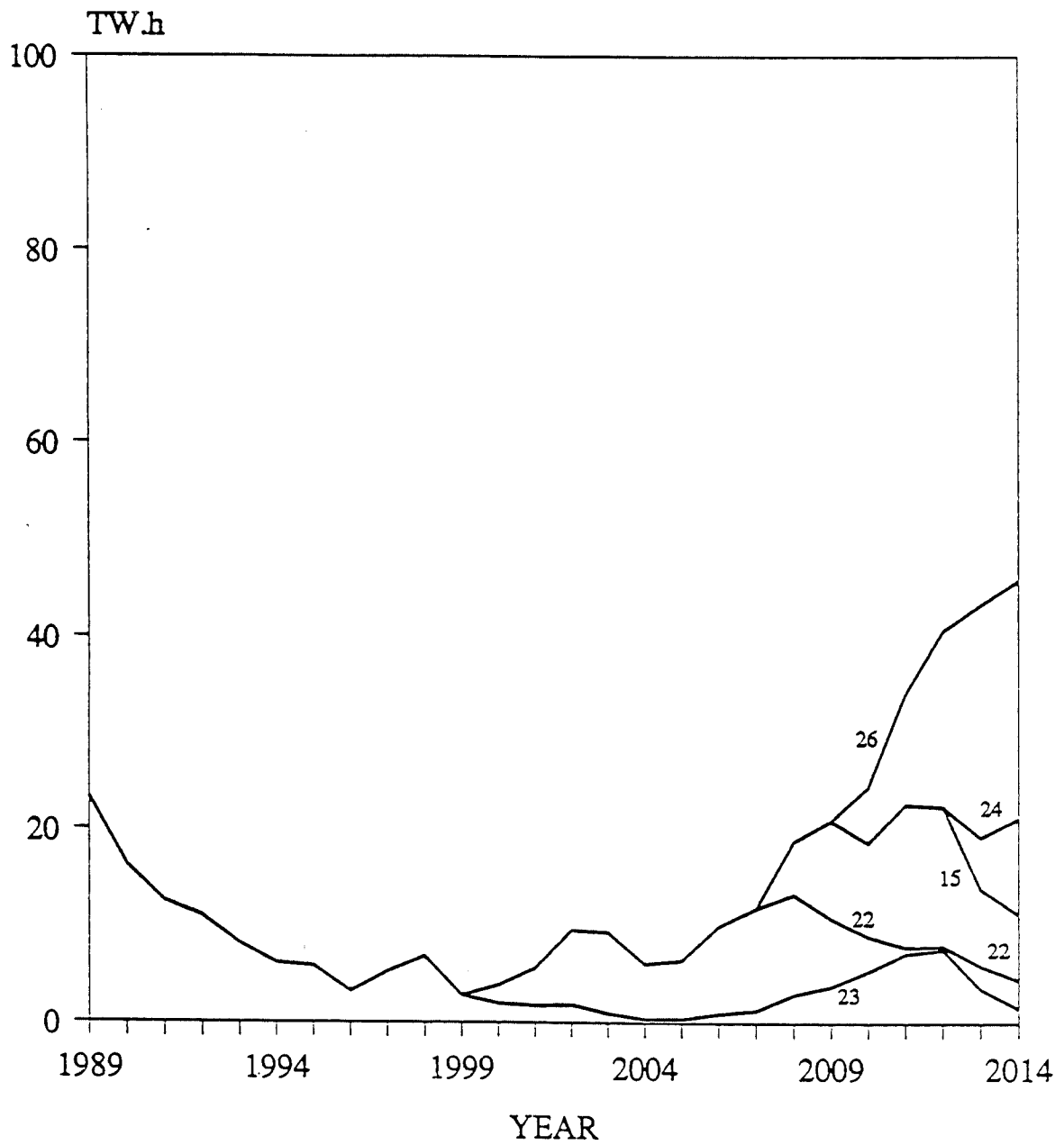


FIGURE 6-5(b)
FOSSIL ENERGY PRODUCTION
(BRANCH LOWER LOAD FORECAST)

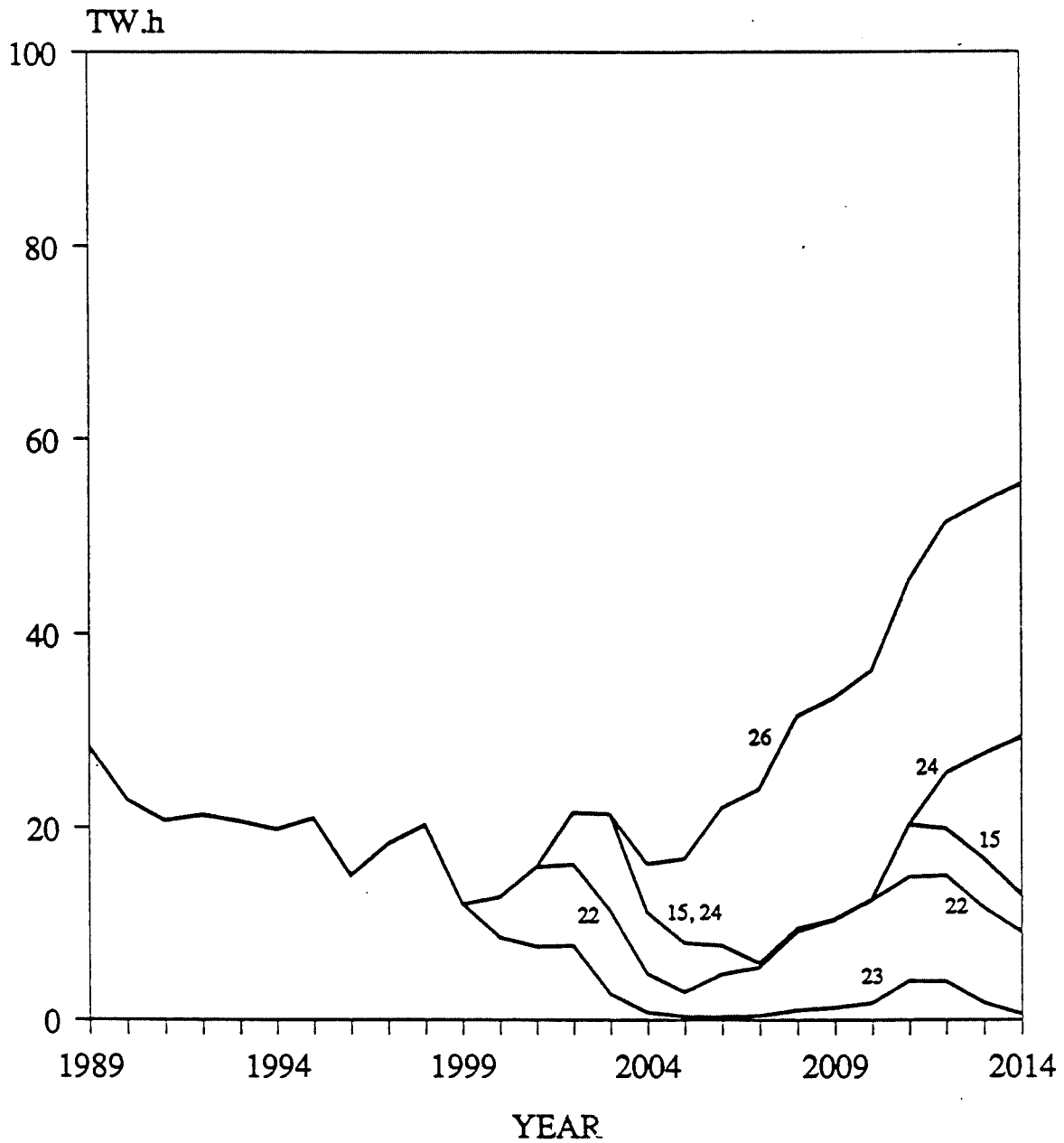


FIGURE 6-5(c)
FOSSIL ENERGY PRODUCTION
(MEDIAN LOAD FORECAST)

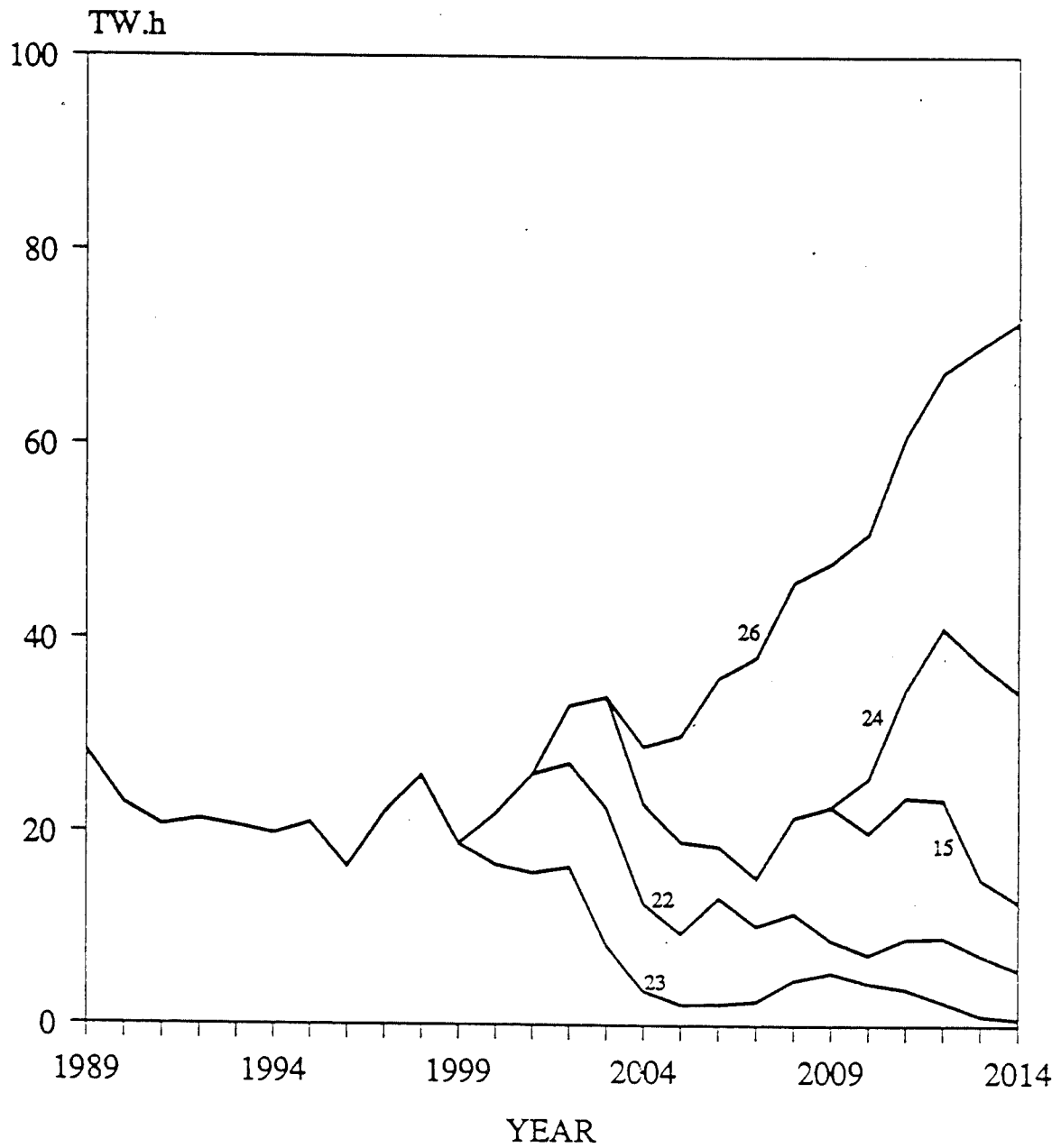


FIGURE 6-5(d)
FOSSIL ENERGY PRODUCTION
(BRANCH UPPER LOAD FORECAST)

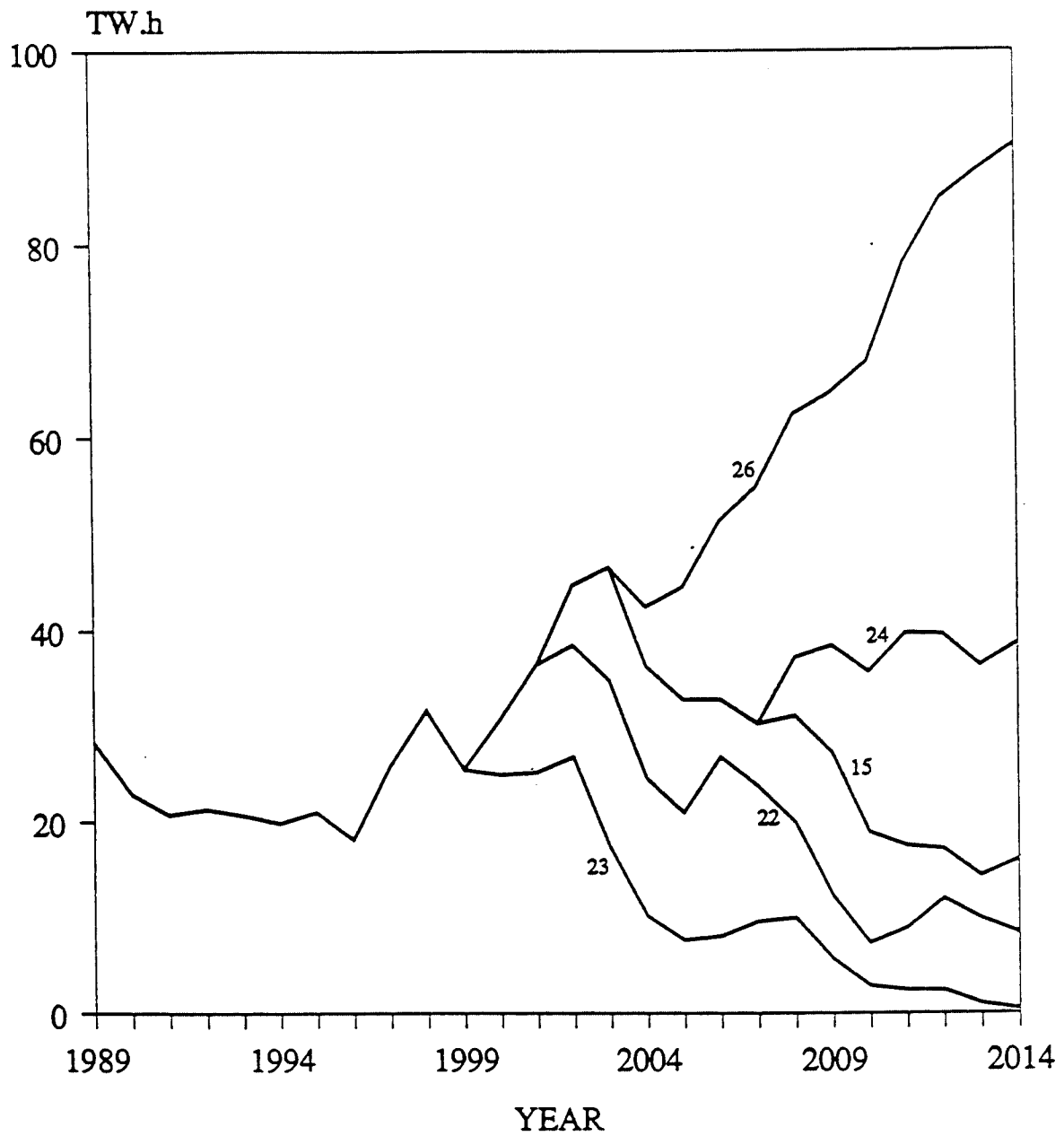
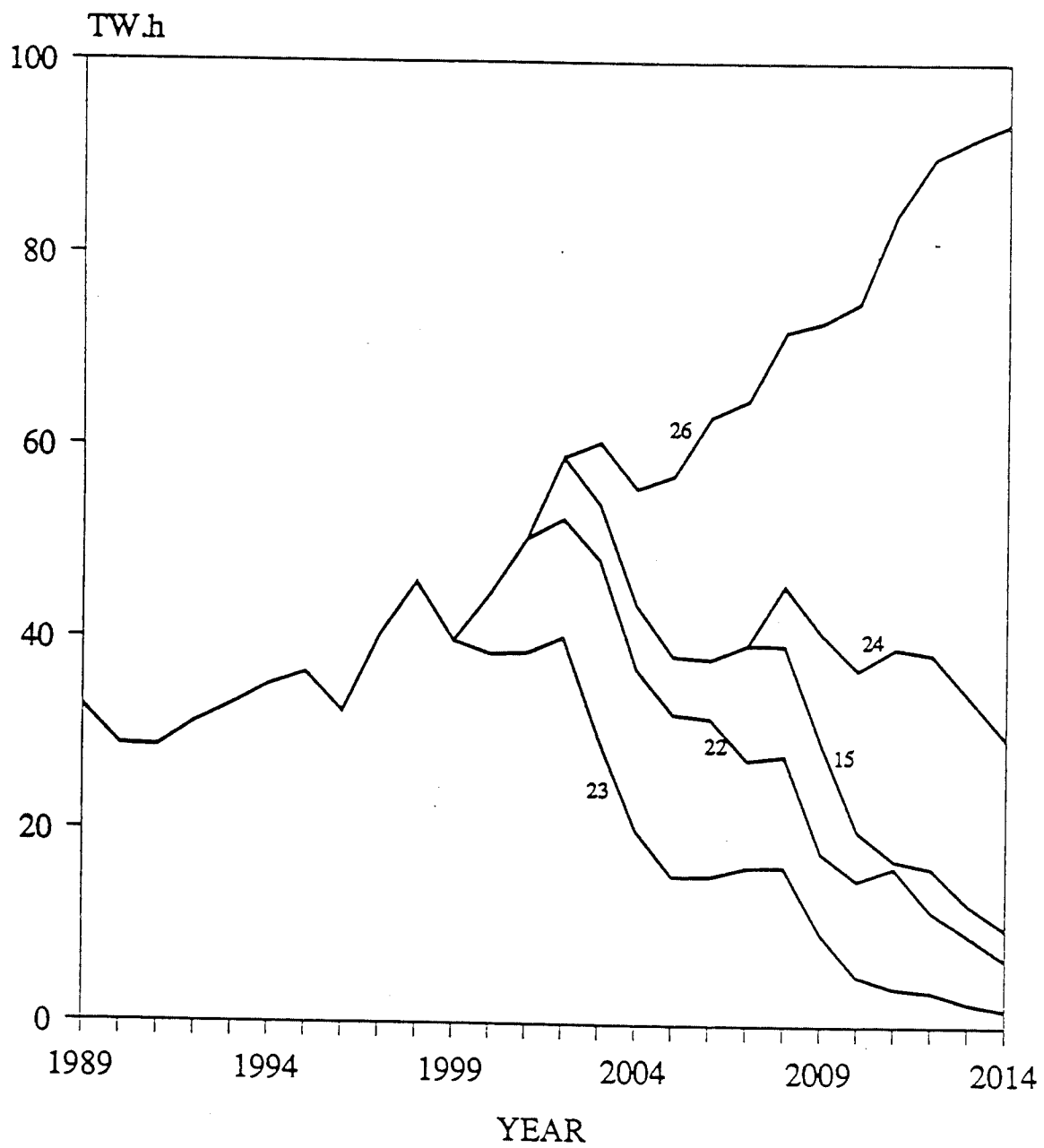


FIGURE 6-5(e)
FOSSIL ENERGY PRODUCTION
(UPPER LOAD FORECAST)



Lower Load Forecast

Under lower load forecast, fossil energy production in all five Cases starts at about 23 TW.h per year, then gradually declines to about 3 TW.h per year by 1999.

In Cases 15, 24 and 26, fossil energy production rises from about 3 TW.h in 1999 to about 21 TW.h per year by 2009. Thereafter, with the addition of major fossil generation to meet load growth and retirement needs, fossil energy production in Case 26 continues to rise to about 46 TW.h per year by 2014. In Case 24, fossil energy production is held at the 21 TW.h per year level to 2014 by the addition of new nuclear facilities. In Case 15, fossil energy production peaks at about 23 TW.h per year in 2011, then declines to about 11 TW.h per year by 2014.

In Case 22, fossil energy production increases from about 3 TW.h per year in 1999 to a peak of about 13 TW.h per year in 2008. Thereafter, new nuclear facilities are added and fossil energy production decreases to about 4 TW.h per year by 2014.

In Case 23, new nuclear facilities are added to meet load growth and retirement needs. The first new nuclear station starts in 1999, the second station in 2009 and the third station in 2011. Fossil energy production falls from about 3 TW.h per year in 1999 to a low of about 0.4 TW.h in 2004. Thereafter, fossil energy production rises gradually to about .8 TW.h per year by 2012, then falls to under 2 TW.h per year by 2014.

Branch Lower Load Forecast

Under branch lower load forecast, fossil energy production in all five Cases starts at about 28 TW.h per year and declines to about 12 TW.h per year by 1999.

In Cases 15, 24 and 26, fossil energy production rises from the low of 12 TW.h in 1999 to about 21 TW.h per year by 2003. Thereafter, fossil energy production in Case 26 rises to about 55 TW.h per year by 2014. In Cases 15 and 24, fossil energy production drops to a low of about 6 TW.h per year in 2007. Case 24 then rises to produce about 29 TW.h of fossil energy per year by 2014, while Case 15 produces about 13 TW.h per year.

In Case 22, fossil energy production falls to a low of 3 TW.h per year in 2005, and reaches about 9 TW.h per year by 2014.

In Case 23, fossil energy production declines steadily from about 12 TW.h per year in 1999 to under 1 TW.h per year by 2014.

Branch Upper Load Forecast

Under branch upper load forecast, fossil energy production also starts at about 28 TW.h per year, declines to about 18 TW.h per year by 1996, then rises to about 25 TW.h per year by 1999.

Thereafter, fossil energy production in Case 26 rises steadily, reaching over 90 TW.h per year by 2014.

In Cases 15 and 24, fossil energy production rises to a peak of 47 TW.h per year in 2003. In Case 24, fossil energy production is held steady at the 30 TW.h to 40 TW.h range, ending at about 39 TW.h per year by 2014. In Case 15, fossil energy production gradually declines to about 16 TW.h by 2014.

In Case 22, fossil energy production rises from about 25 TW.h per year in 1999 to a peak of about 38 TW.h per year in 2002, then declines to about 8 TW.h per year by 2014.

In Case 23, fossil energy production declines steadily from 25 TW.h per year in 1999 to under 1 TW.h per year by 2014.

Upper Load Forecast

Under upper load forecast, fossil energy production in all five Cases starts at about 33 TW.h per year. Fossil generation decreases for two years as the Darlington generating units are brought into service. After 1991, load growth needs dominate and fossil generation increases to about 40 TW.h per year by 1999. Thereafter, fossil energy production begins to differ among the Cases.

In Case 26, fossil energy production continues to rise from 40 TW.h per year in 1999 to about 94 TW.h per year by 2014, the highest level among all the Cases.

Fossil energy production in Cases 15 and 24 is the same as Case 26 up to 2002, when it peaks at about 59 TW.h per year. Fossil generation then declines as new nuclear facilities are brought into service between 2002 and 2014. By 2014, fossil energy production reaches about 10 TW.h per year in Case 15 and about 30 TW.h per year in Case 24.

In Case 22, fossil energy production rises from about 40 TW.h per year in 1999 to about 53 TW.h per year in 2002. Thereafter, as new nuclear generation is brought into service, fossil generation declines to about 7 TW.h per year by 2014.

In Case 23, fossil energy production decreases steadily from about 40 TW.h per year in 1999 to under 2 TW.h per year by 2014.

6.4 ENERGY DIVERSITY BY SOURCE AND FUEL

The portions of energy acquired from utility and non-utility purchases and hydraulic, nuclear and fossil generation are shown in Figures 6-6(a) through 6-10(e) for the five Cases under each of the five load forecast paths. The portions are expressed as a percentage of the total energy produced per year.

6.4.1 Common Features - Hydraulic, Non-utility Generation And Utility Purchases

There are several common features among the five Cases.

Non-utility generation purchases rise from a very small fraction of total energy in 1989 to about 5% of total energy by 2014. Non-utility generation purchases are just under 4% of total energy under the branch lower and lower load paths.

The 1000 MW Manitoba Purchase provides a small fraction of total energy production, contributing about 3% per year by 2014. Under the branch lower and lower load paths, utility purchases provide slightly under 4% of total energy.

Despite growth in the absolute quantity of hydraulic energy produced under each load path, there is not sufficient hydraulic potential to keep pace with the development of other options. Therefore, the portion of hydraulic energy production decreases with time. Hydraulic generation produces about 25% to 27% of energy needs in 1989, depending upon load forecast, and decreases to about 17% to 22% of total energy by 2014.

Together, utility and non-utility purchases and hydraulic production provide a reasonably level portion of energy across all Cases; about 27% under median load forecast, about 30% under branch lower and lower load forecasts, and about 25% under branch upper and upper load forecasts.

This leaves nuclear and fossil generation to make up the remaining portion of energy needs. The proportions of each option vary over time and between Cases.

FIGURE 6-6(a)
ENERGY DIVERSITY - CASE 23
(LOWER LOAD FORECAST)

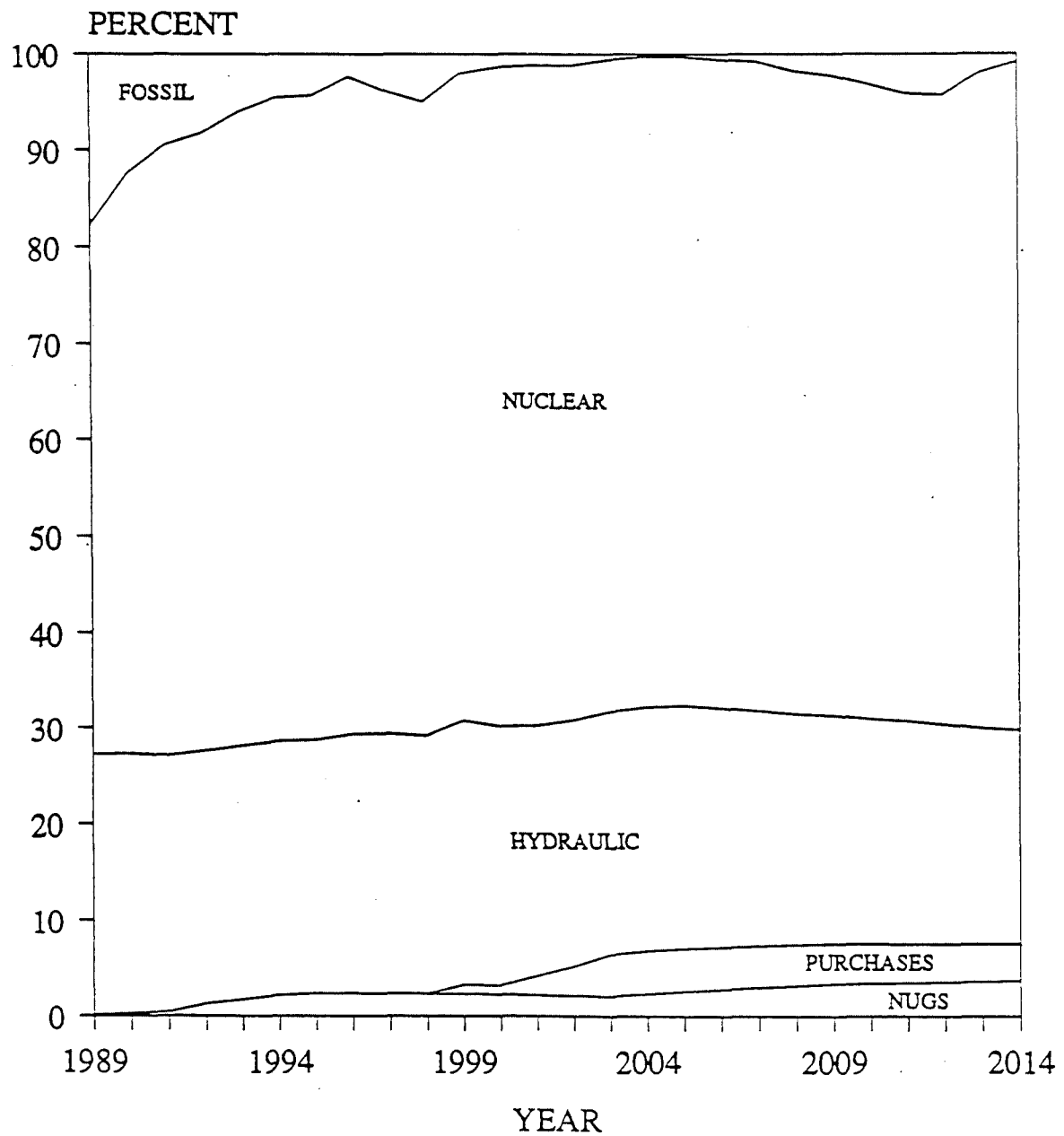


FIGURE 6-6(b)
ENERGY DIVERSITY - CASE 23
(BRANCH LOWER LOAD FORECAST)

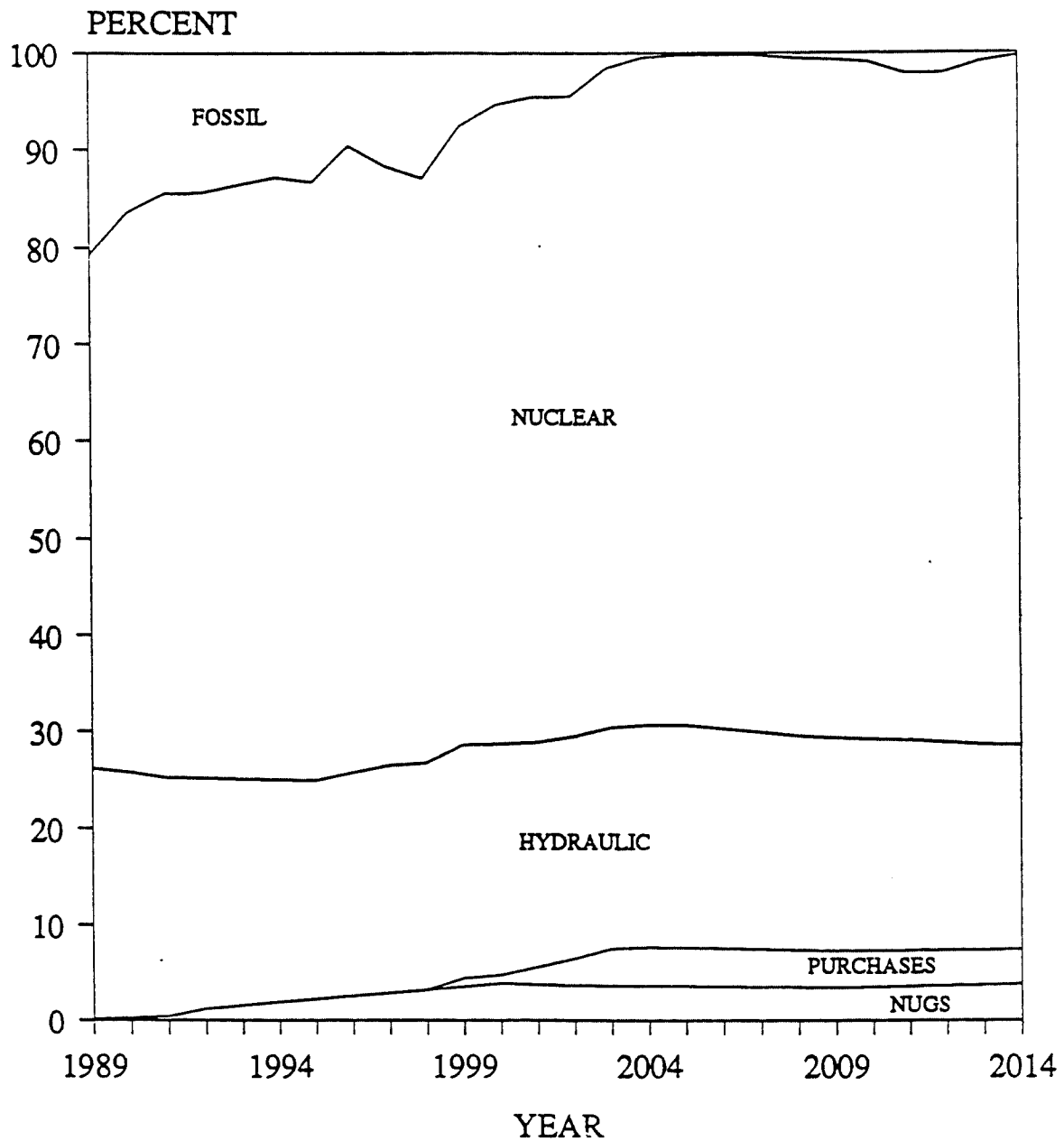


FIGURE 6-6(c)
ENERGY DIVERSITY - CASE 23
(MEDIAN LOAD FORECAST)

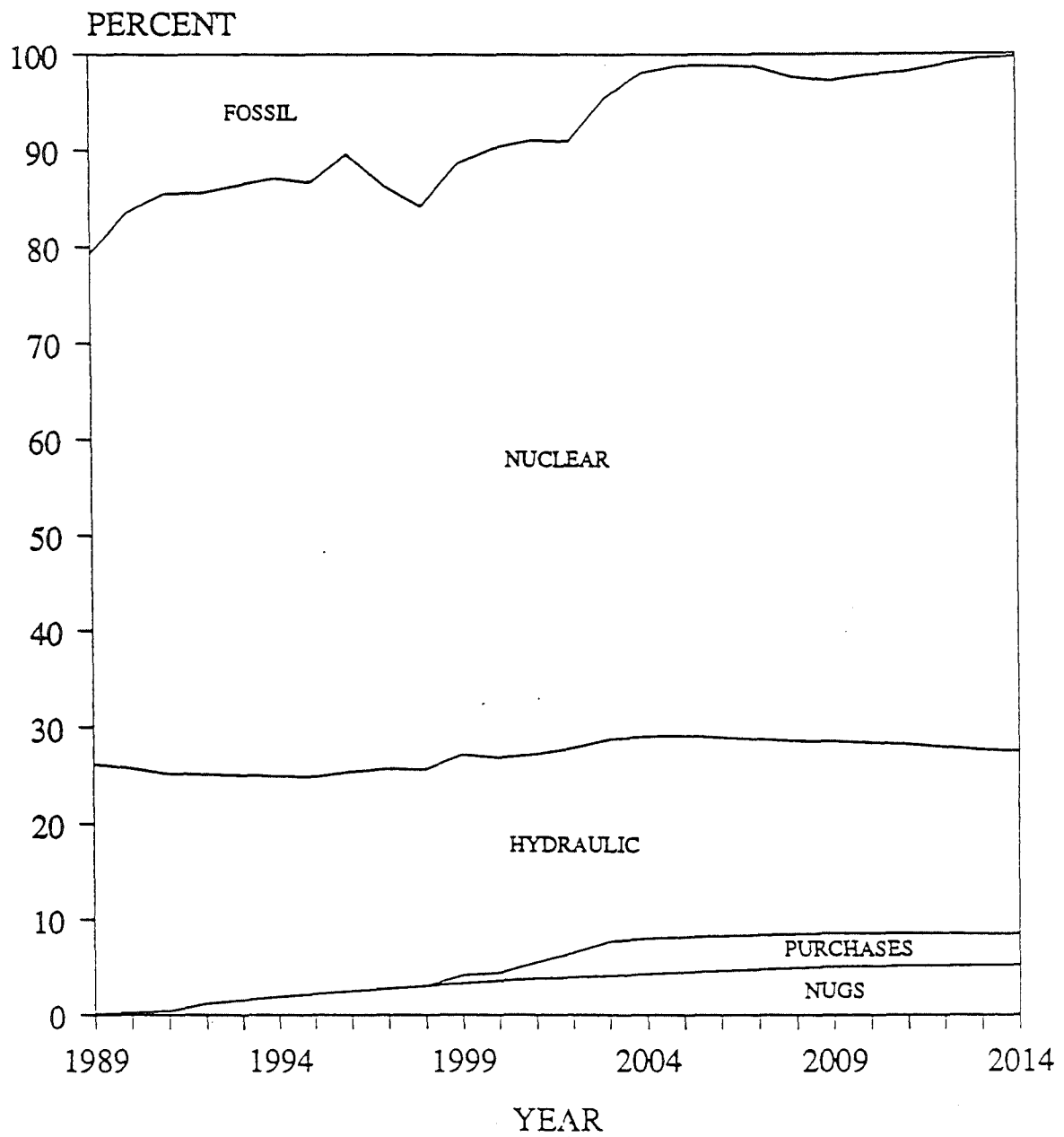


FIGURE 6-6(d)
ENERGY DIVERSITY - CASE 23
(BRANCH UPPER LOAD FORECAST)

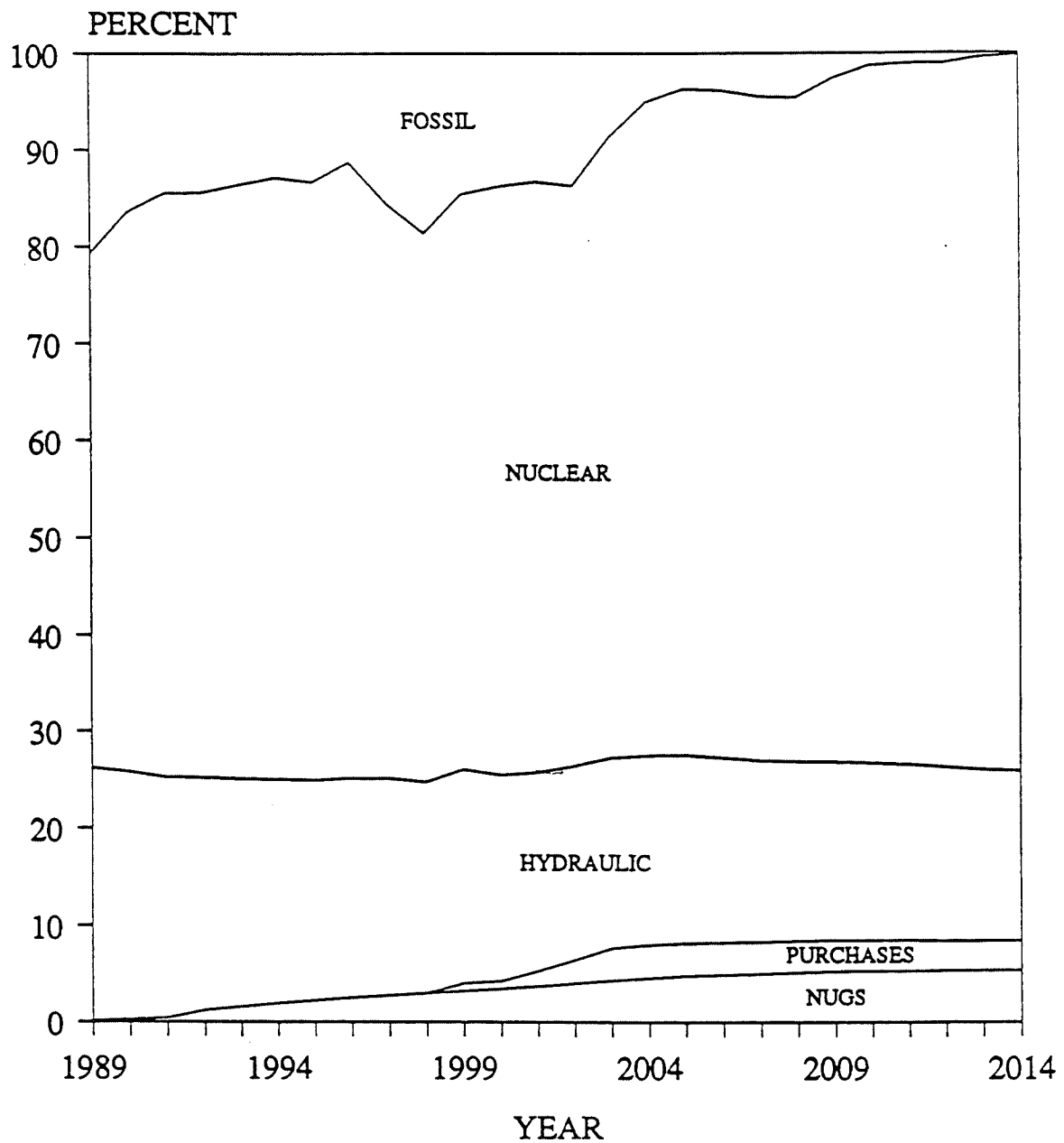


FIGURE 6-6(e)
ENERGY DIVERSITY - CASE 23
(UPPER LOAD FORECAST)

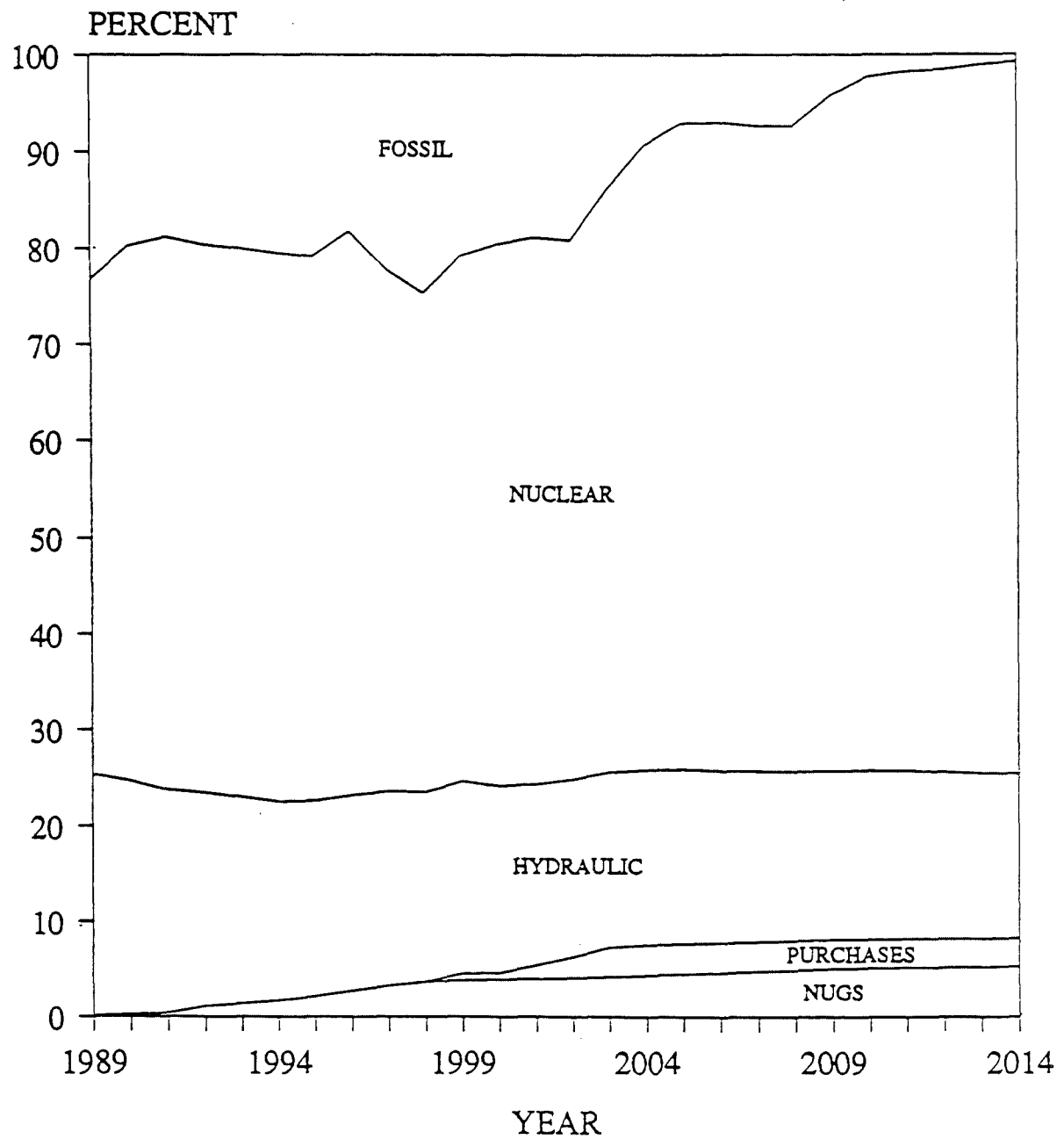


FIGURE 6-7(a)
ENERGY DIVERSITY - CASE 22
(LOWER LOAD FORECAST)

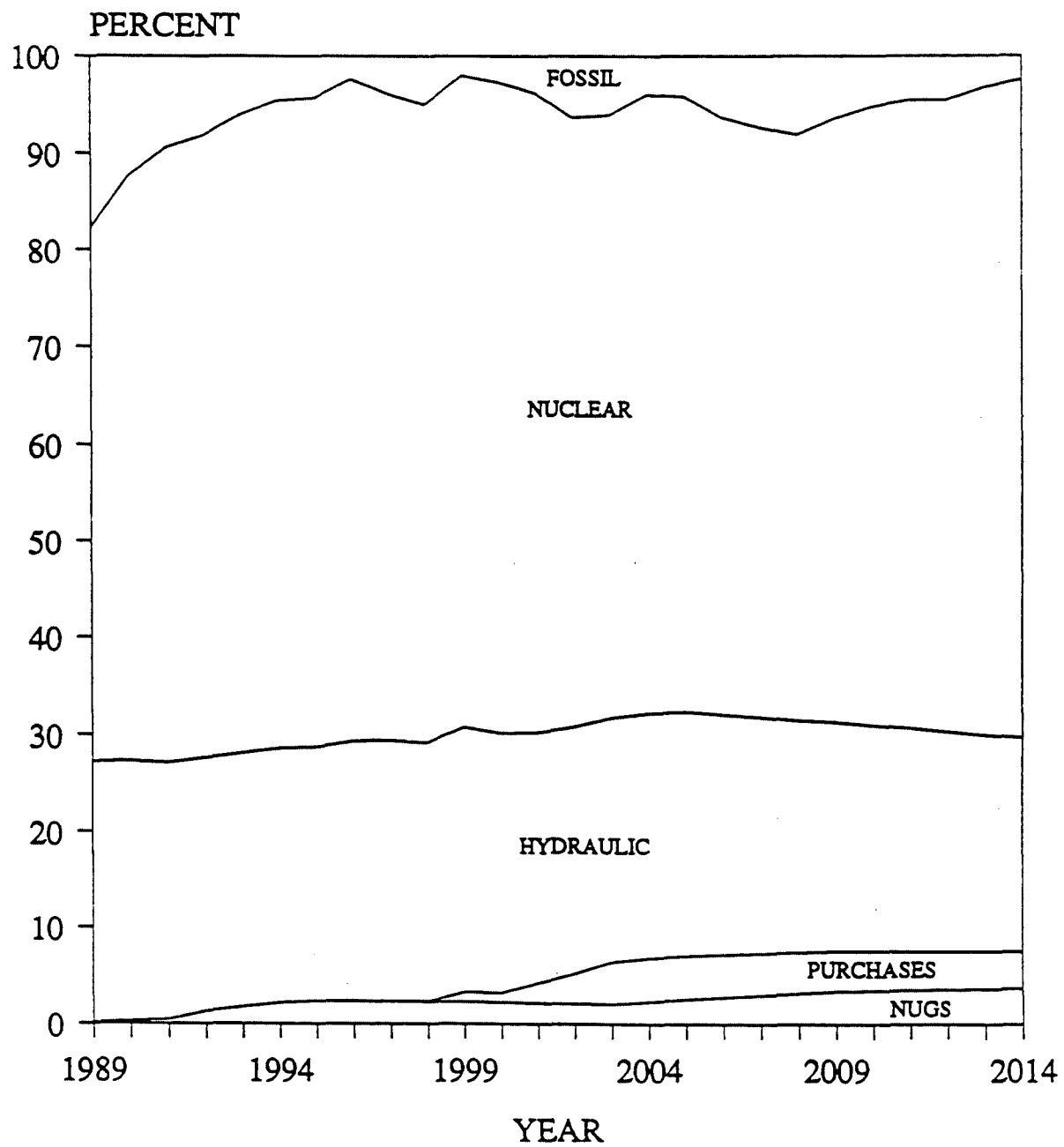


FIGURE 6-7(b)
ENERGY DIVERSITY - CASE 22
(BRANCH LOWER LOAD FORECAST)

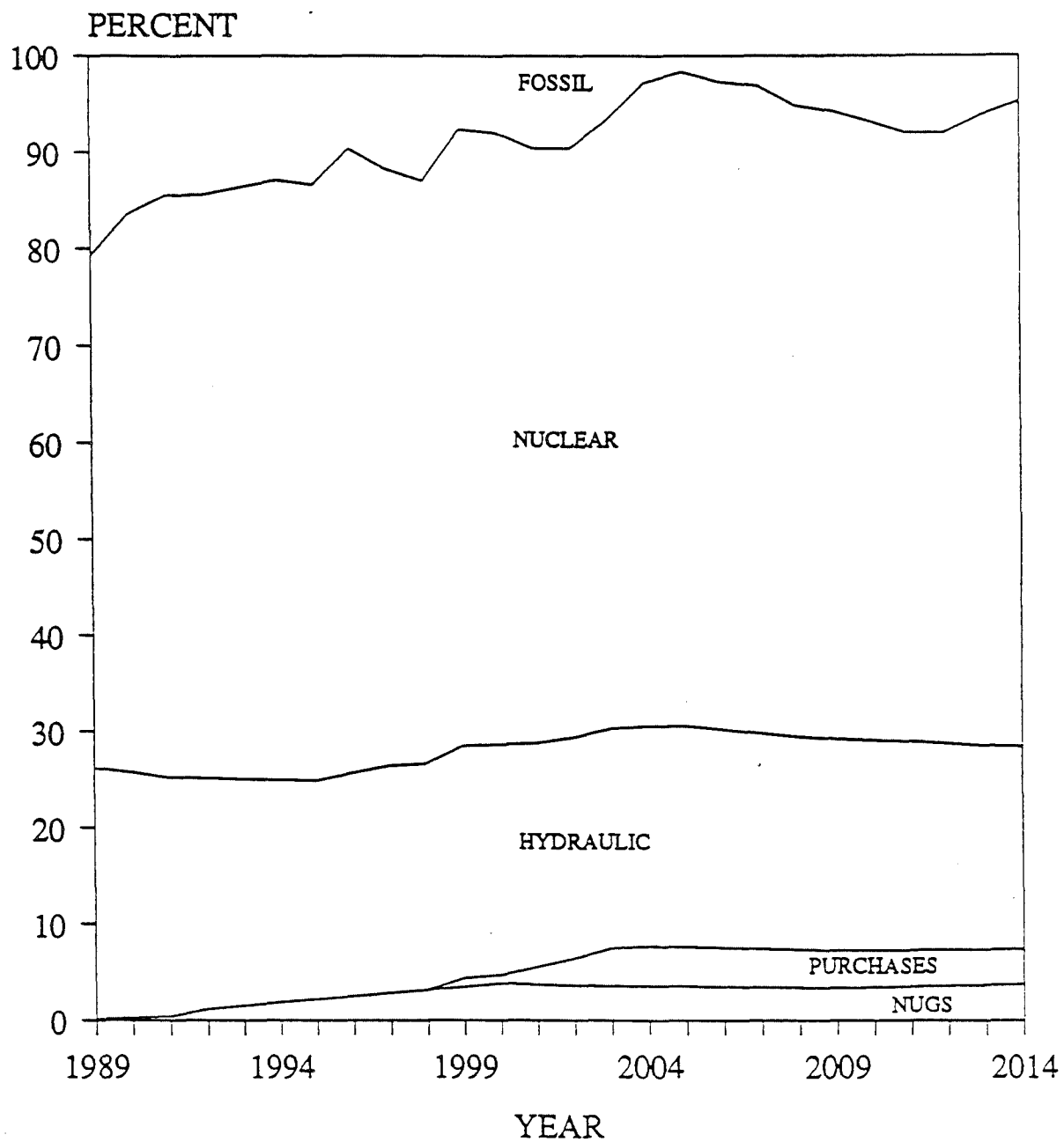


FIGURE 6-7(c)
ENERGY DIVERSITY - CASE 22
(MEDIAN LOAD FORECAST)

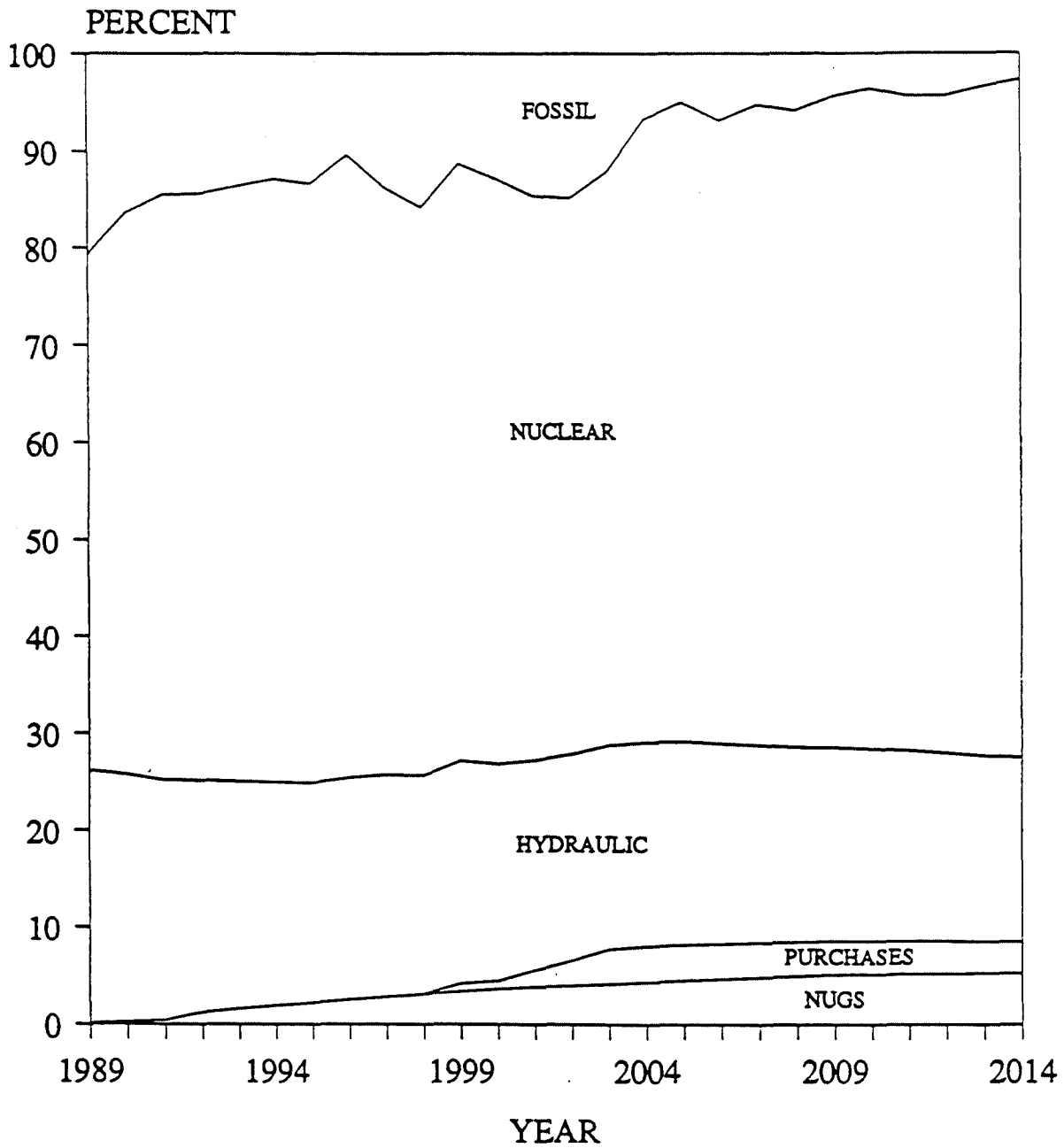


FIGURE 6-7(d)
ENERGY DIVERSITY - CASE 22
(BRANCH UPPER LOAD FORECAST)

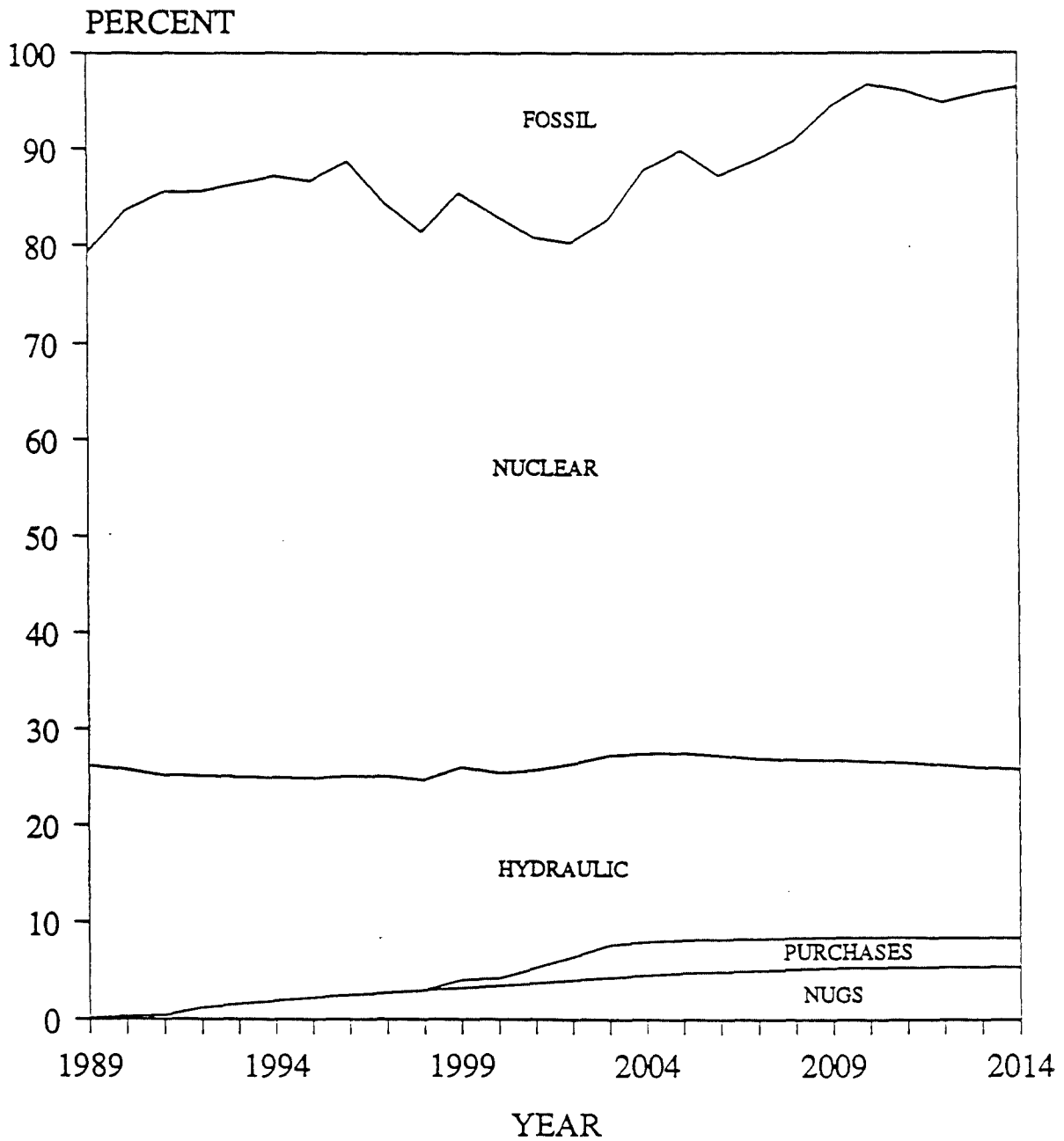


FIGURE 6-7(e)
ENERGY DIVERSITY - CASE 22
(UPPER LOAD FORECAST)

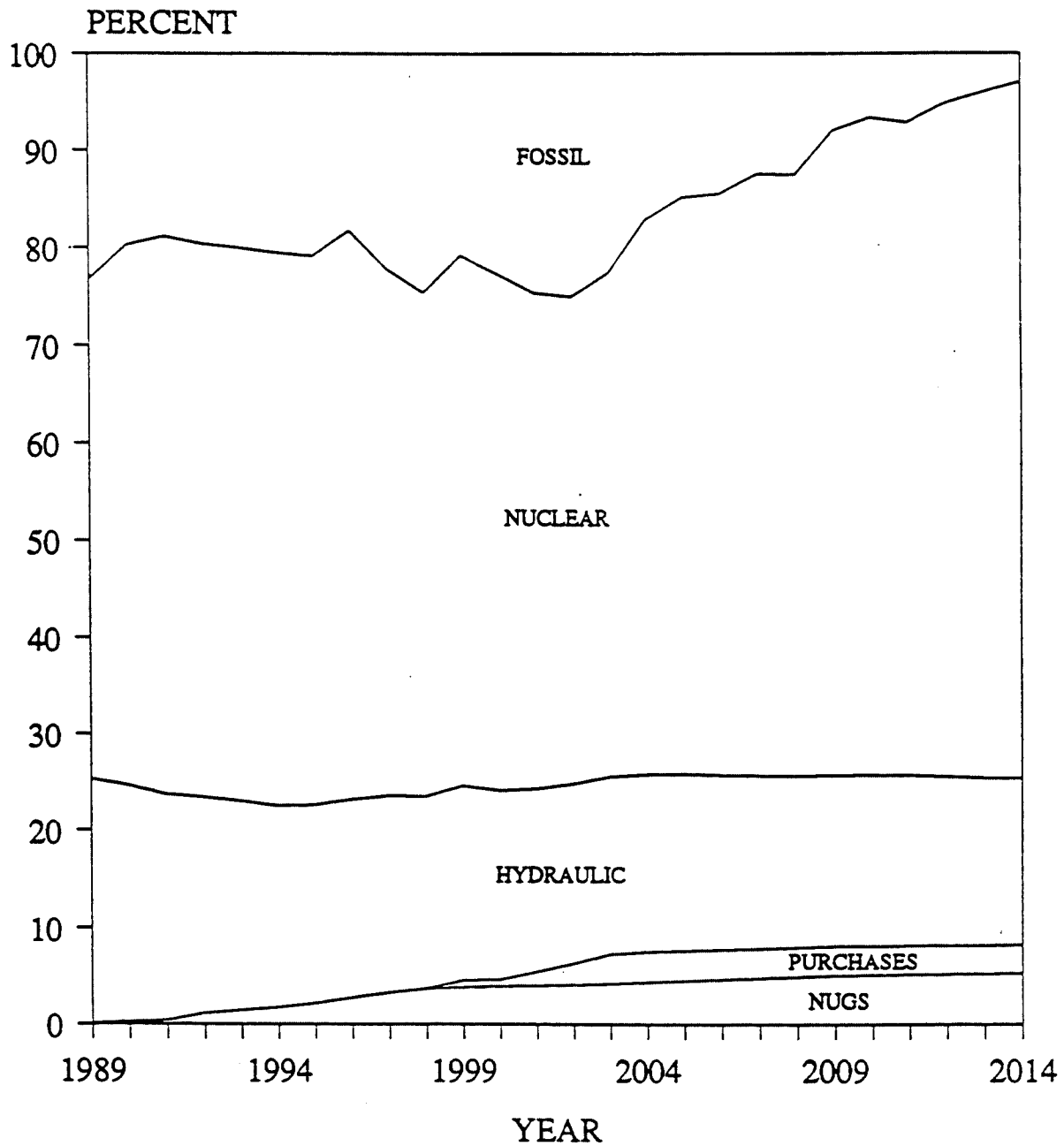


FIGURE 6-8(a)
ENERGY DIVERSITY - CASE 15
(LOWER LOAD FORECAST)

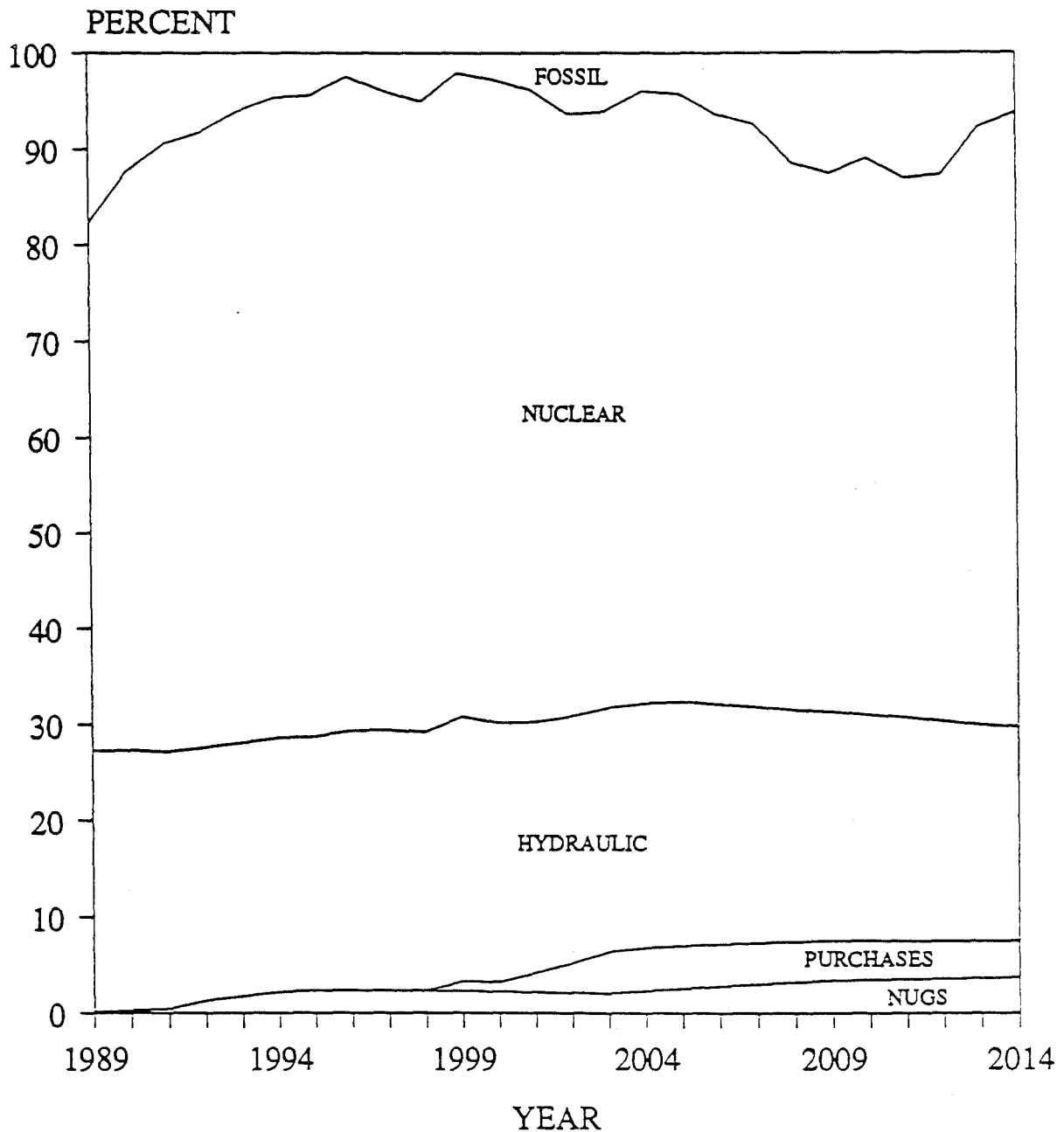


FIGURE 6-8(b)
ENERGY DIVERSITY - CASE 15
(BRANCH LOWER LOAD FORECAST)

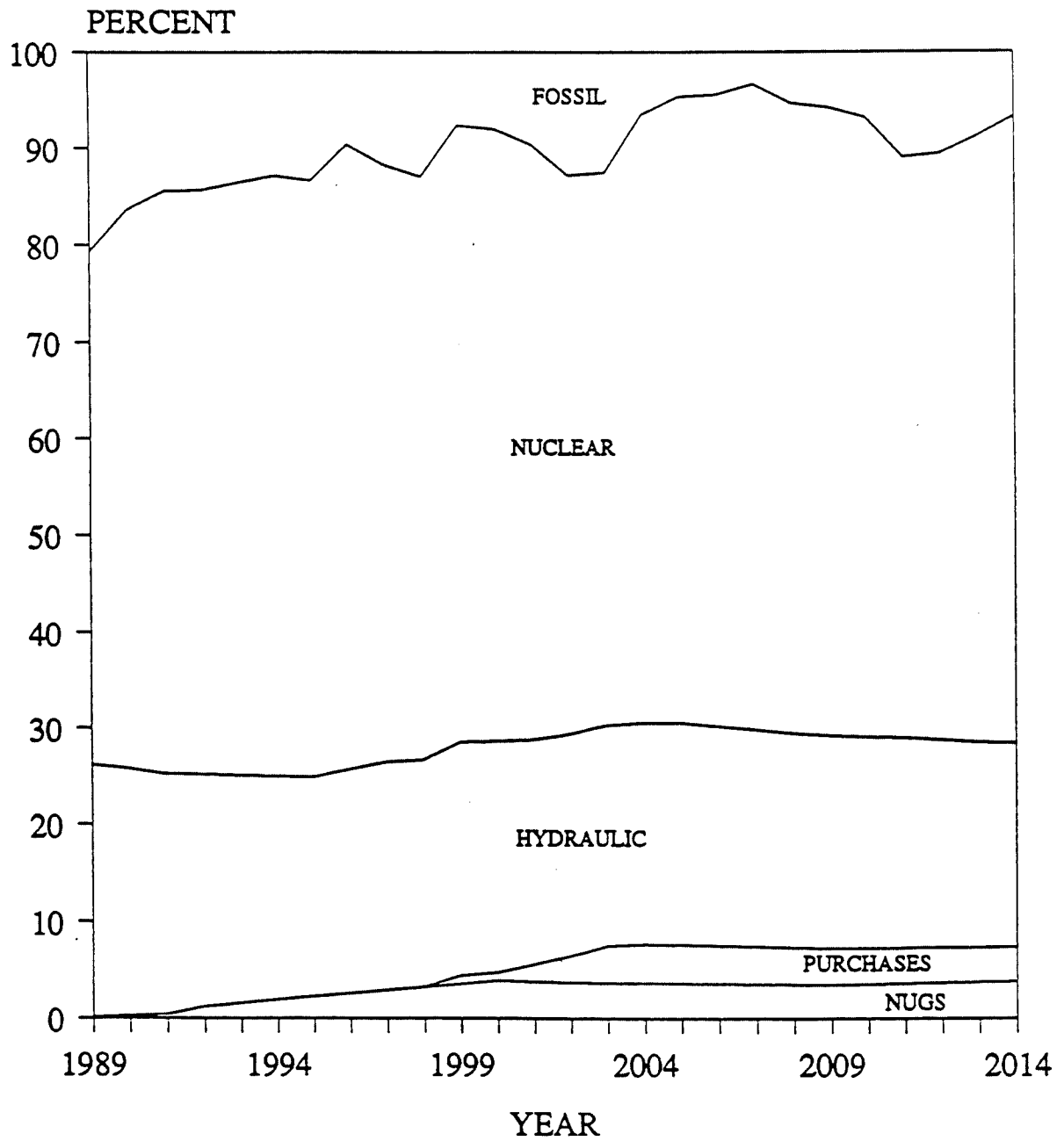


FIGURE 6-8(c)
ENERGY DIVERSITY - CASE 15
(MEDIAN LOAD FORECAST)

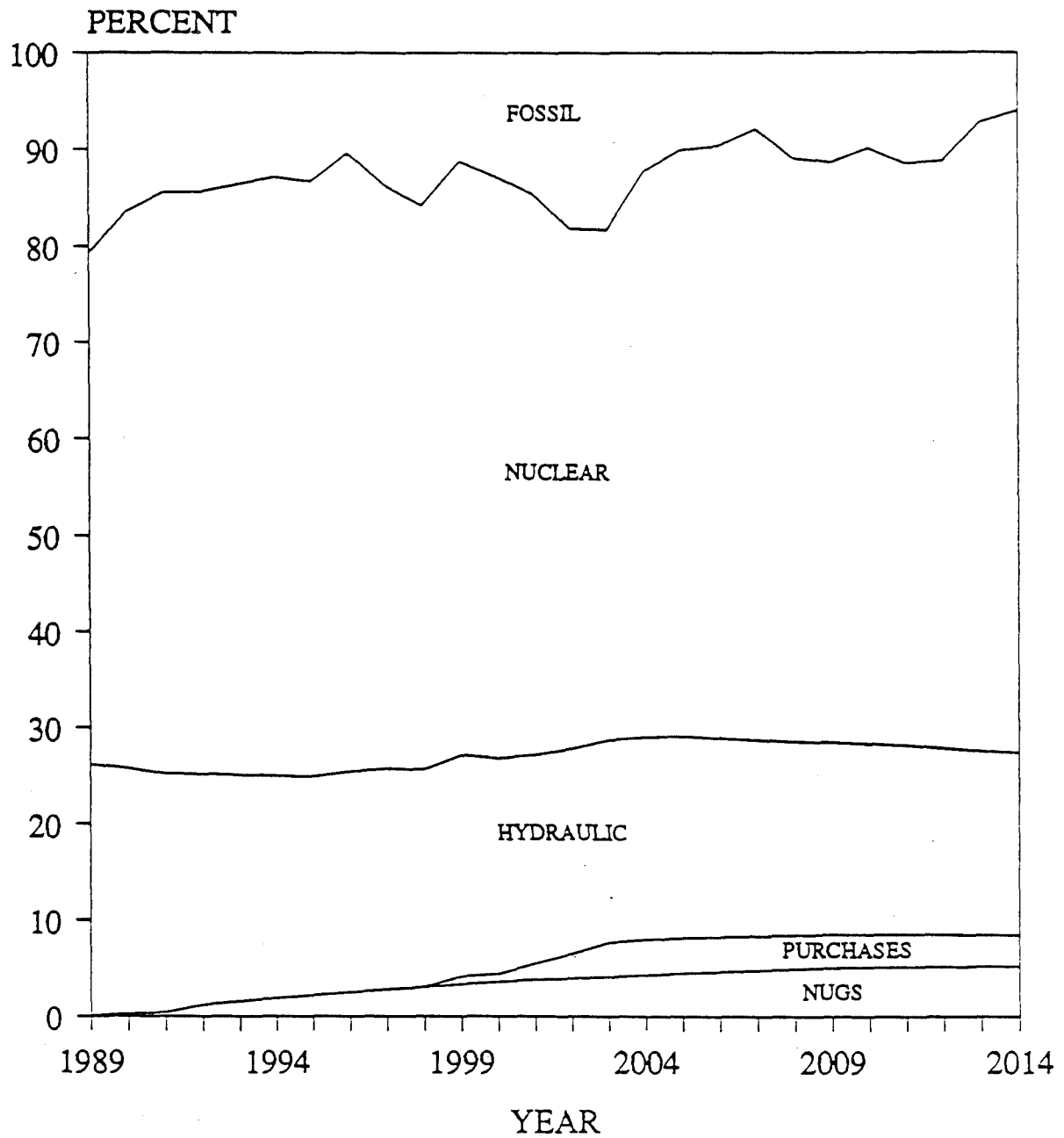


FIGURE 6-8(d)
ENERGY DIVERSITY - CASE 15
(BRANCH UPPER LOAD FORECAST)

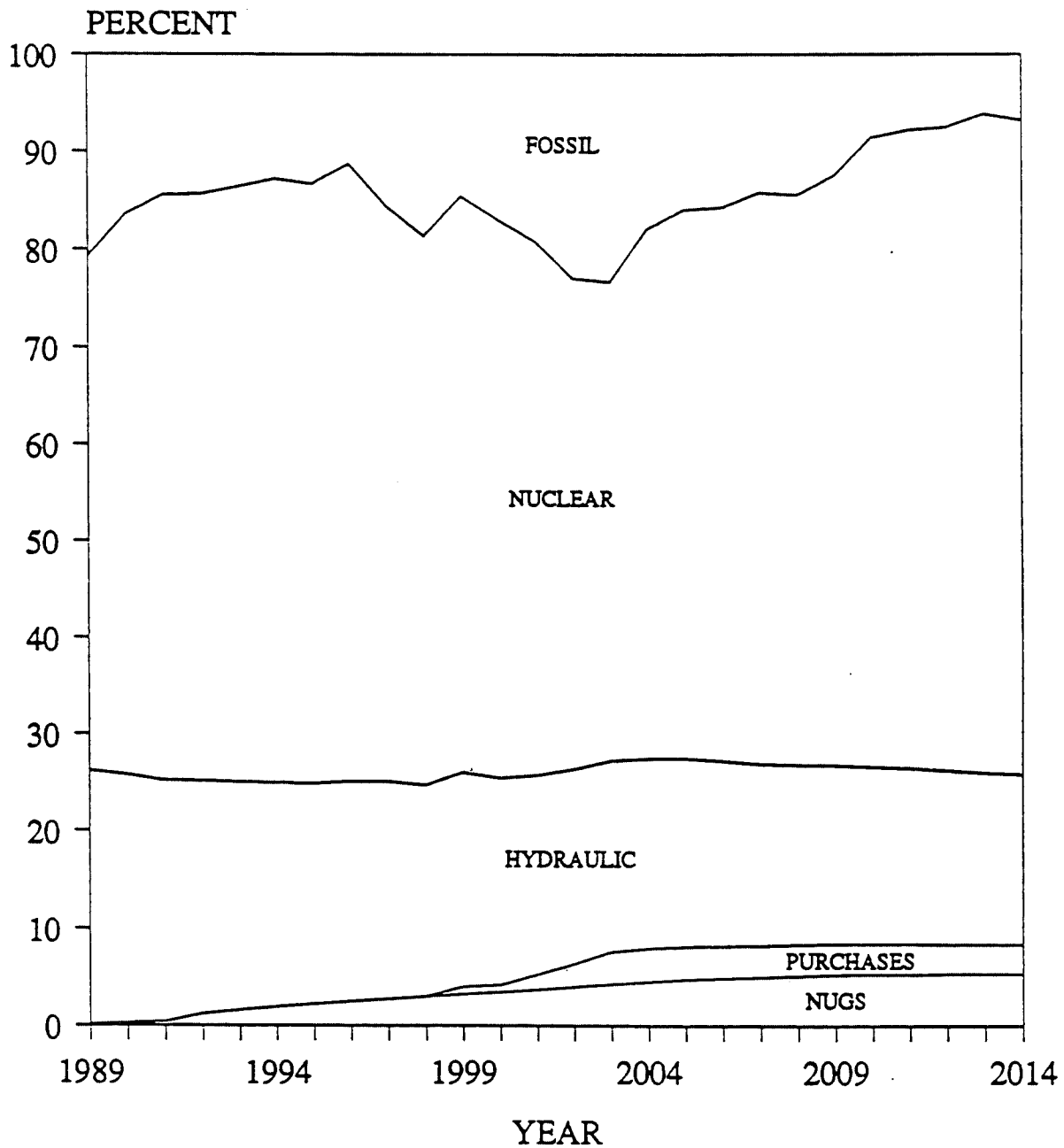


FIGURE 6-8(e)
ENERGY DIVERSITY - CASE 15
(UPPER LOAD FORECAST)

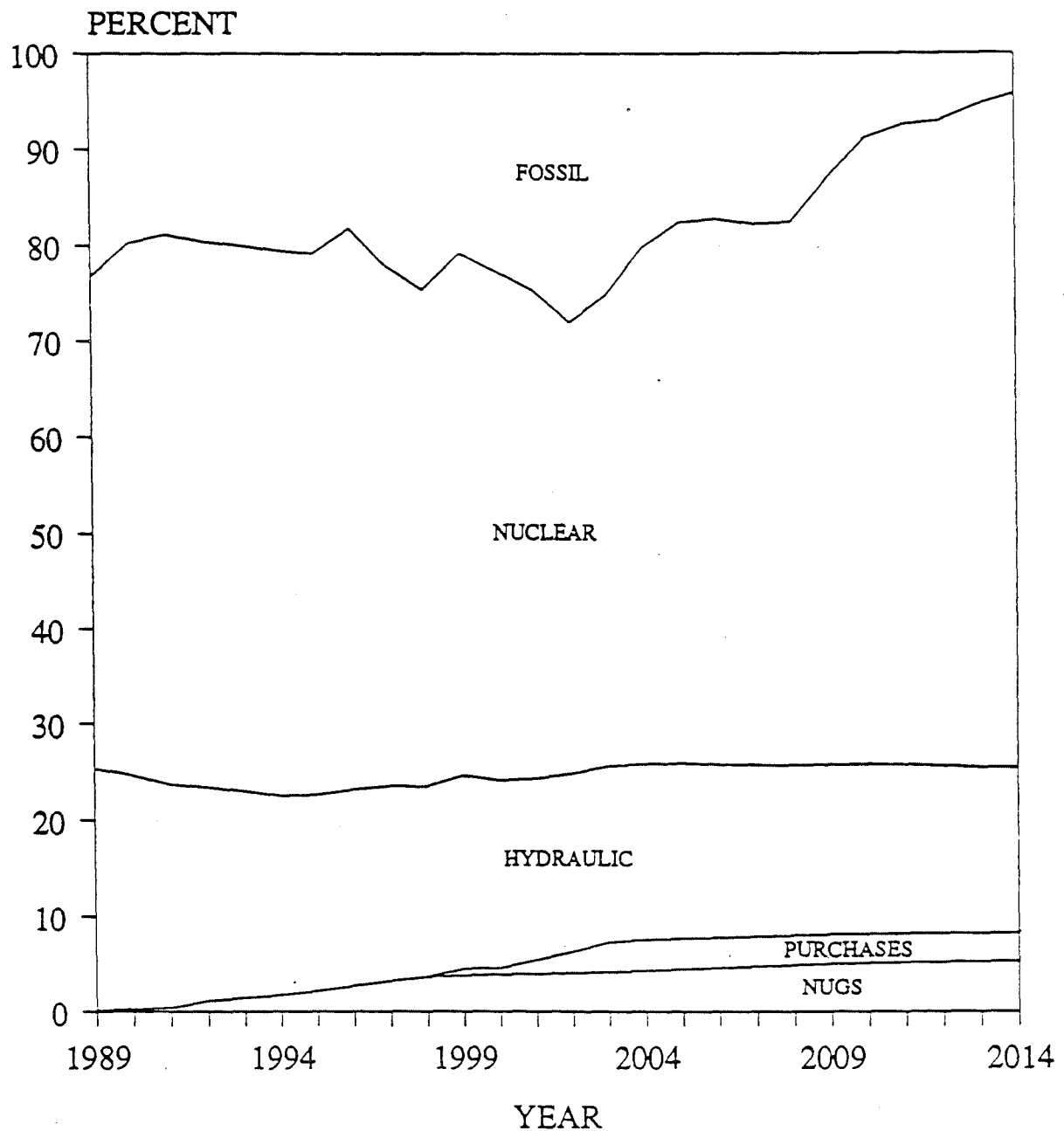


FIGURE 6-9(a)
ENERGY DIVERSITY - CASE 24
(LOWER LOAD FORECAST)

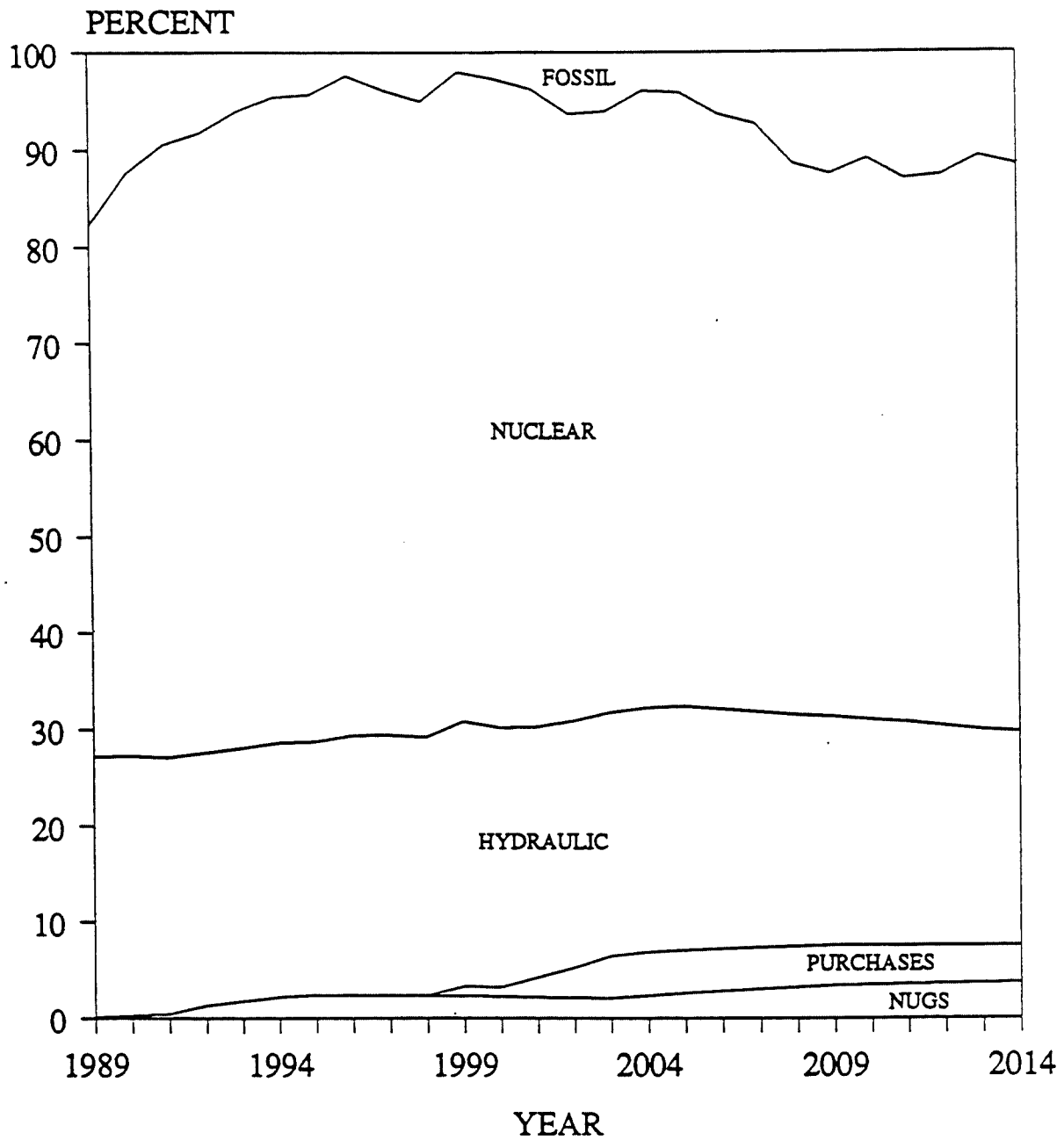


FIGURE 6-9(b)
ENERGY DIVERSITY - CASE 24
(BRANCH LOWER LOAD FORECAST)

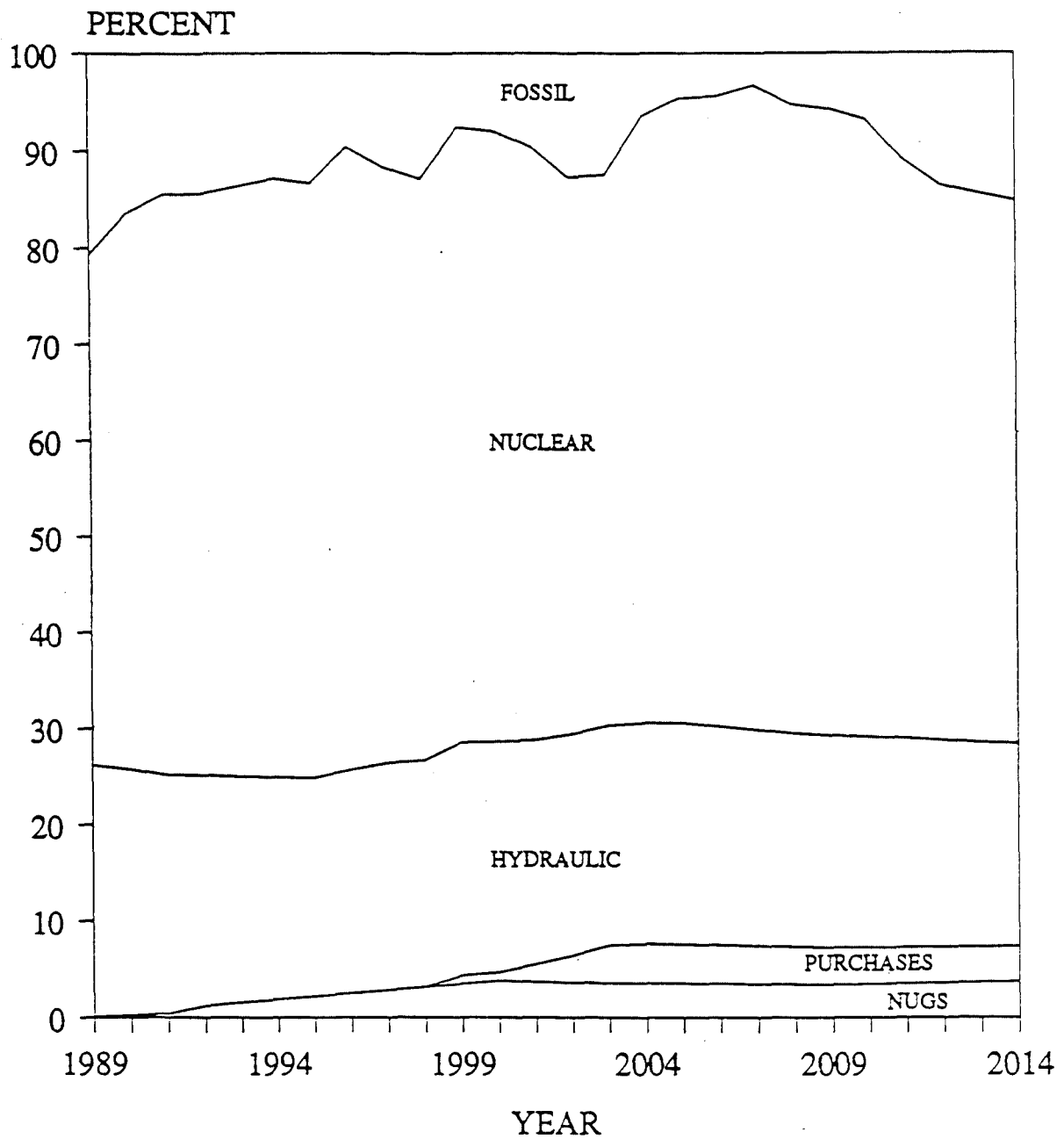


FIGURE 6-9(c)
ENERGY DIVERSITY - CASE 24
(MEDIAN LOAD FORECAST)

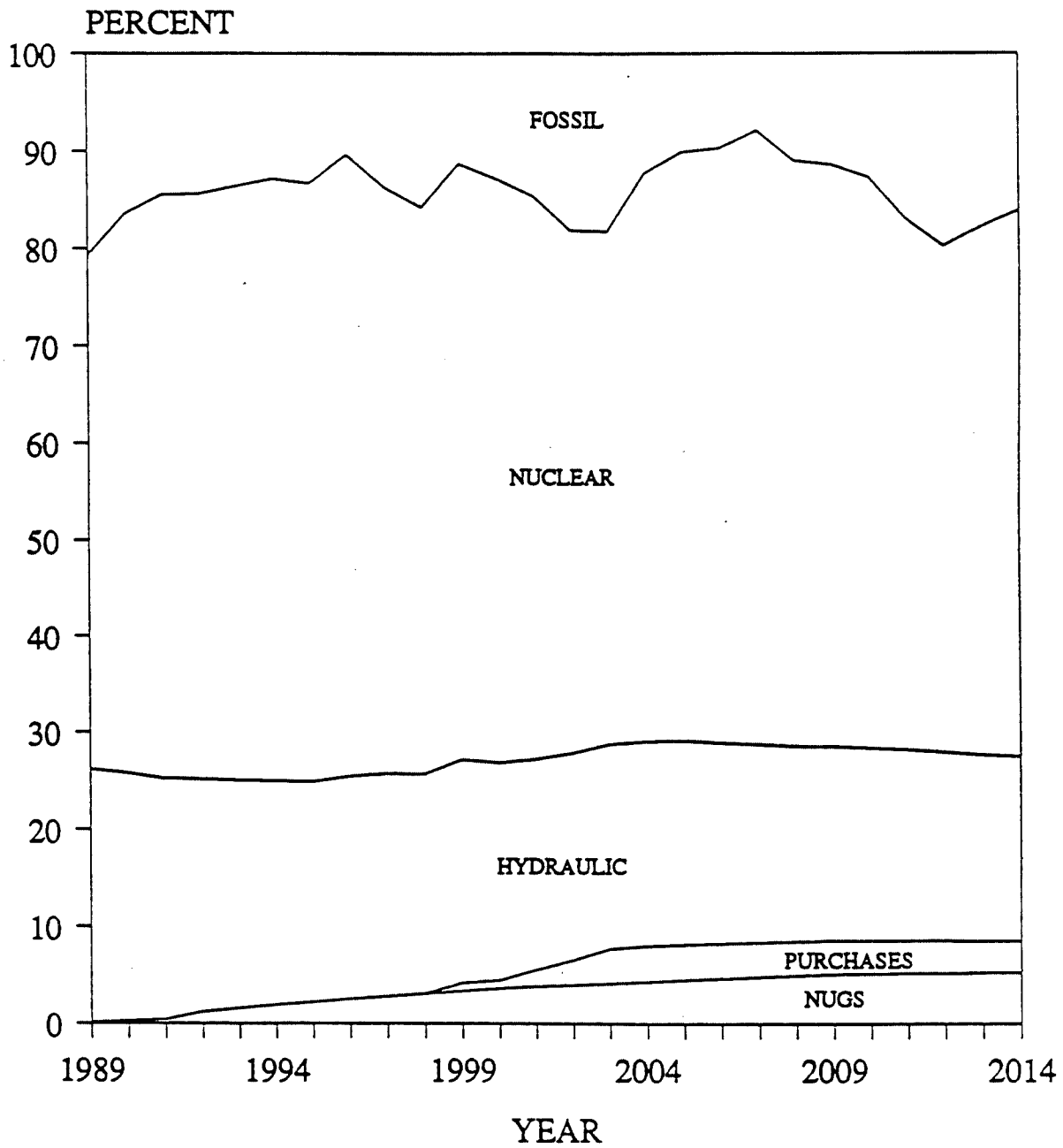


FIGURE 6-9(d)
ENERGY DIVERSITY - CASE 24
(BRANCH UPPER LOAD FORECAST)

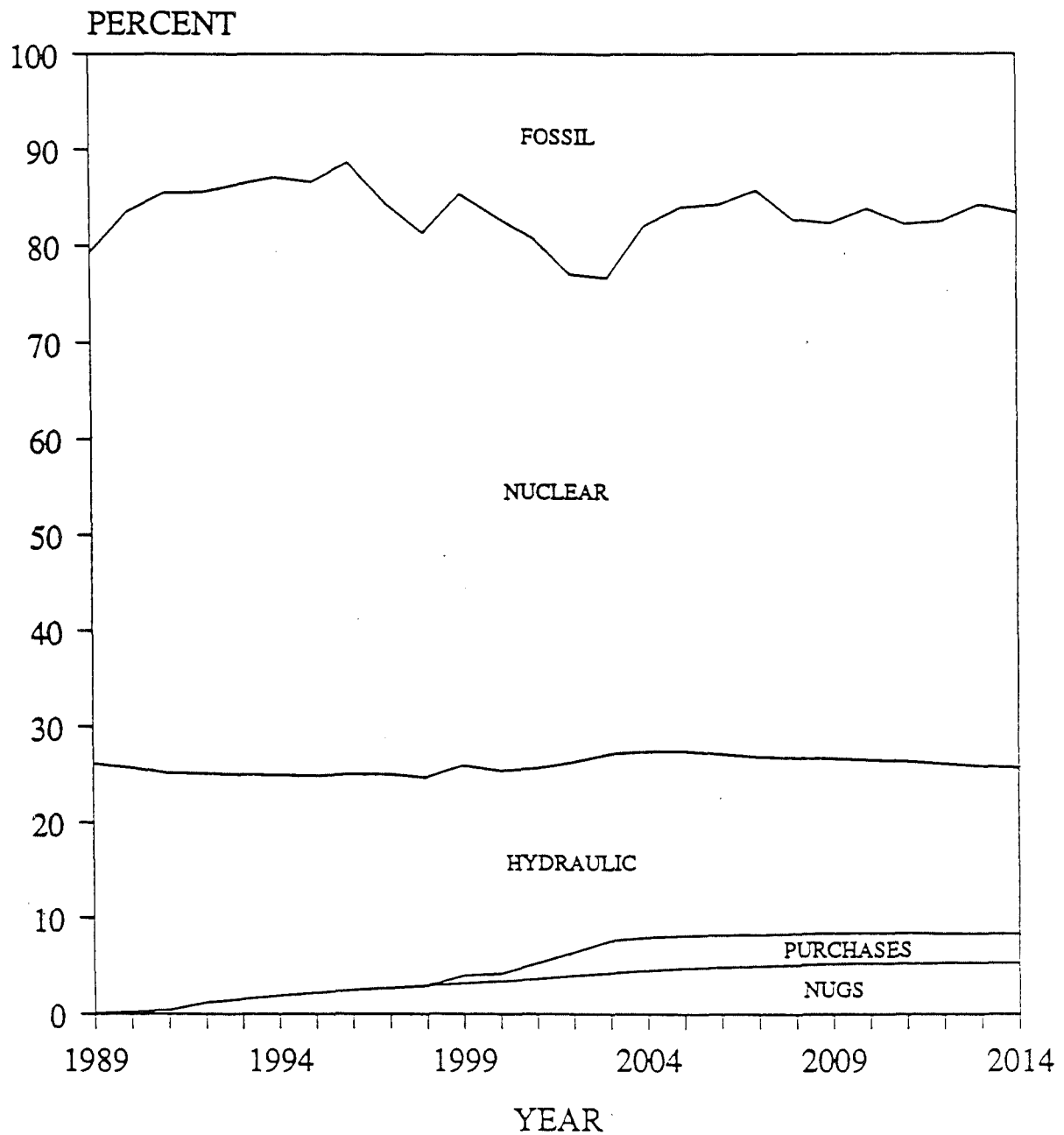


FIGURE 6-9(e)
ENERGY DIVERSITY - CASE 24
(UPPER LOAD FORECAST)

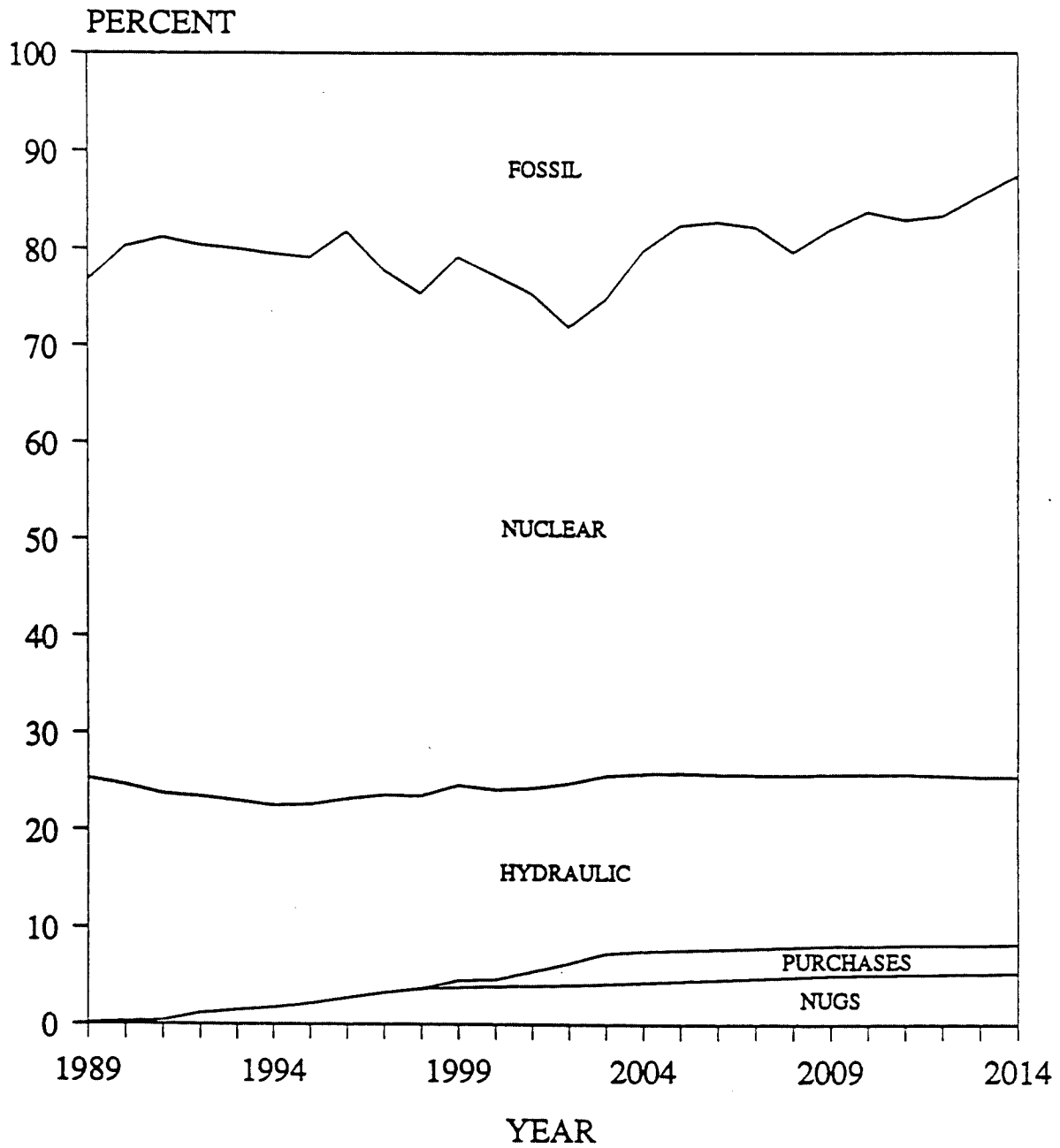


FIGURE 6-10(a)
ENERGY DIVERSITY - CASE 26
(LOWER LOAD FORECAST)

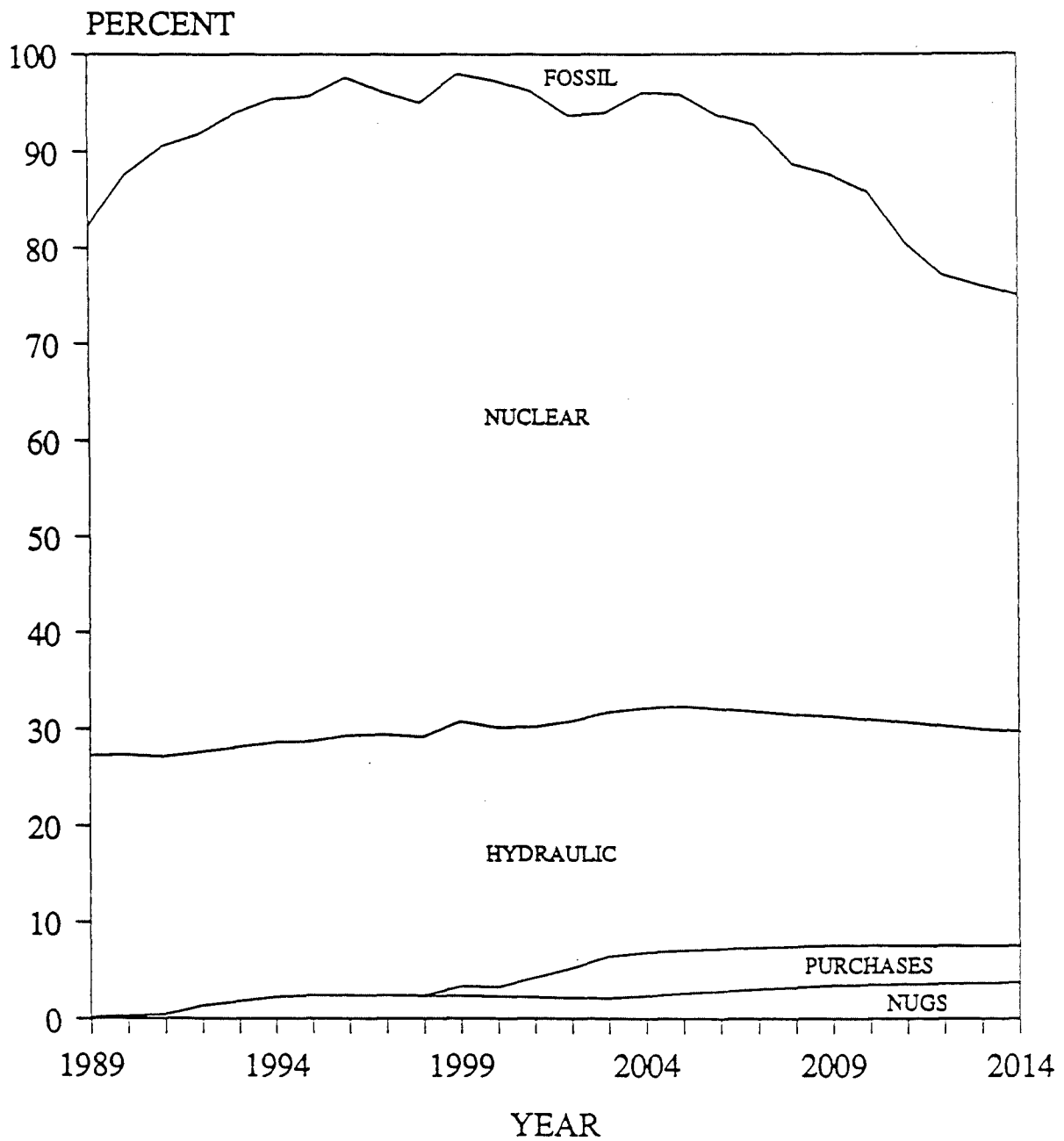


FIGURE 6-10(b)
ENERGY DIVERSITY - CASE 26
(BRANCH LOWER LOAD FORECAST)

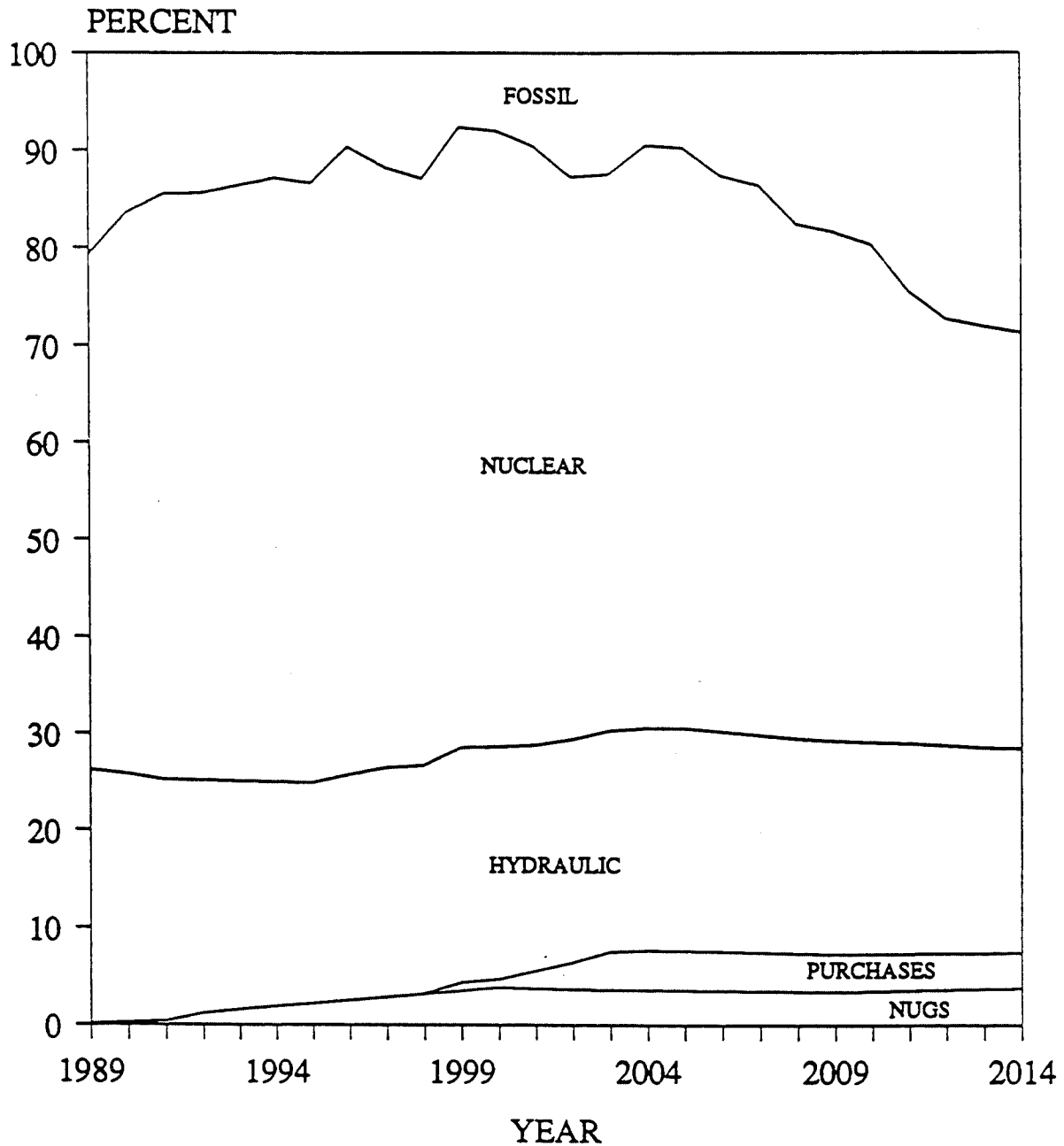


FIGURE 6-10(c)
ENERGY DIVERSITY - CASE 26
(MEDIAN LOAD FORECAST)

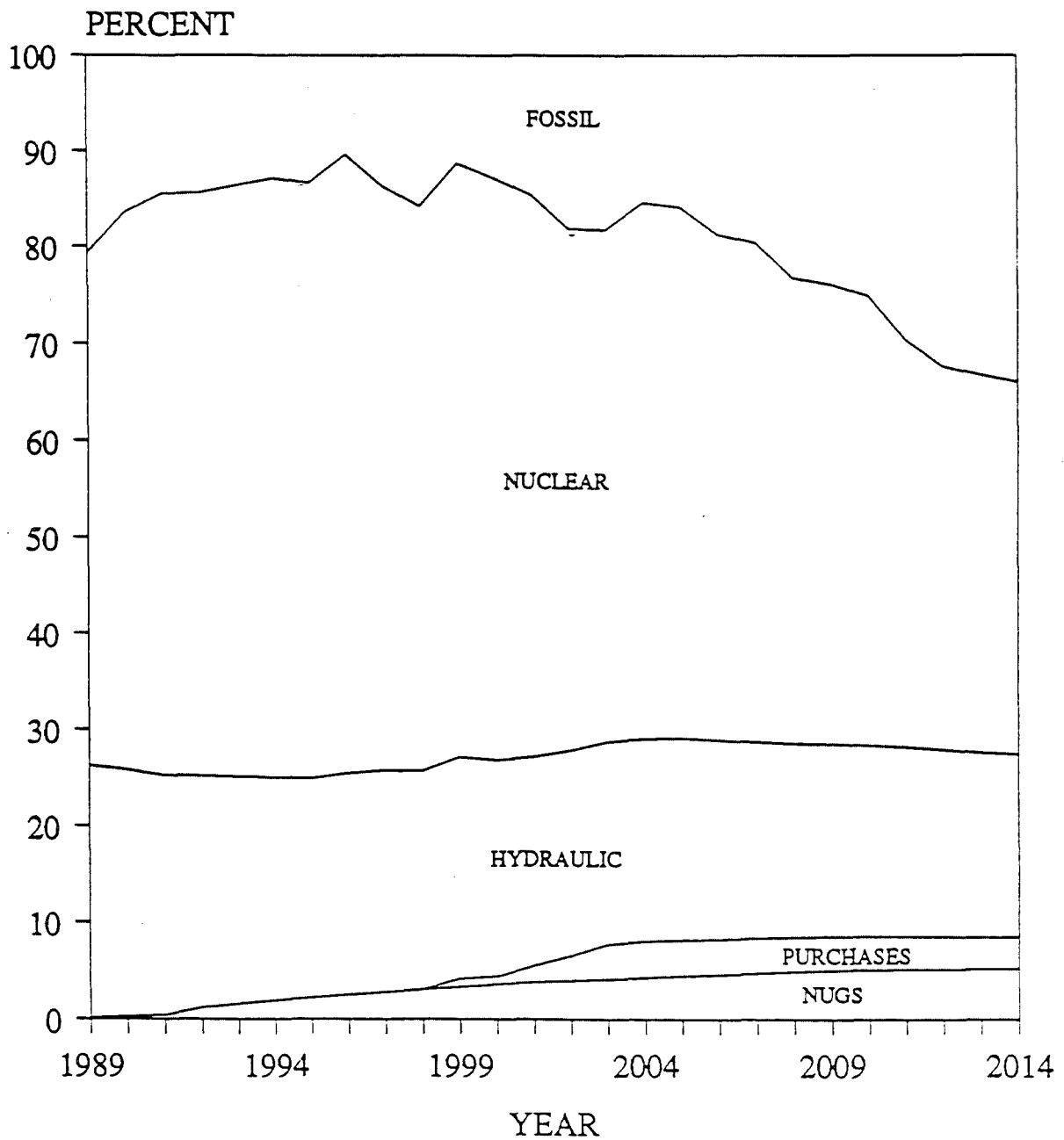


FIGURE 6-10(d)
ENERGY DIVERSITY - CASE 26
(BRANCH UPPER LOAD FORECAST)

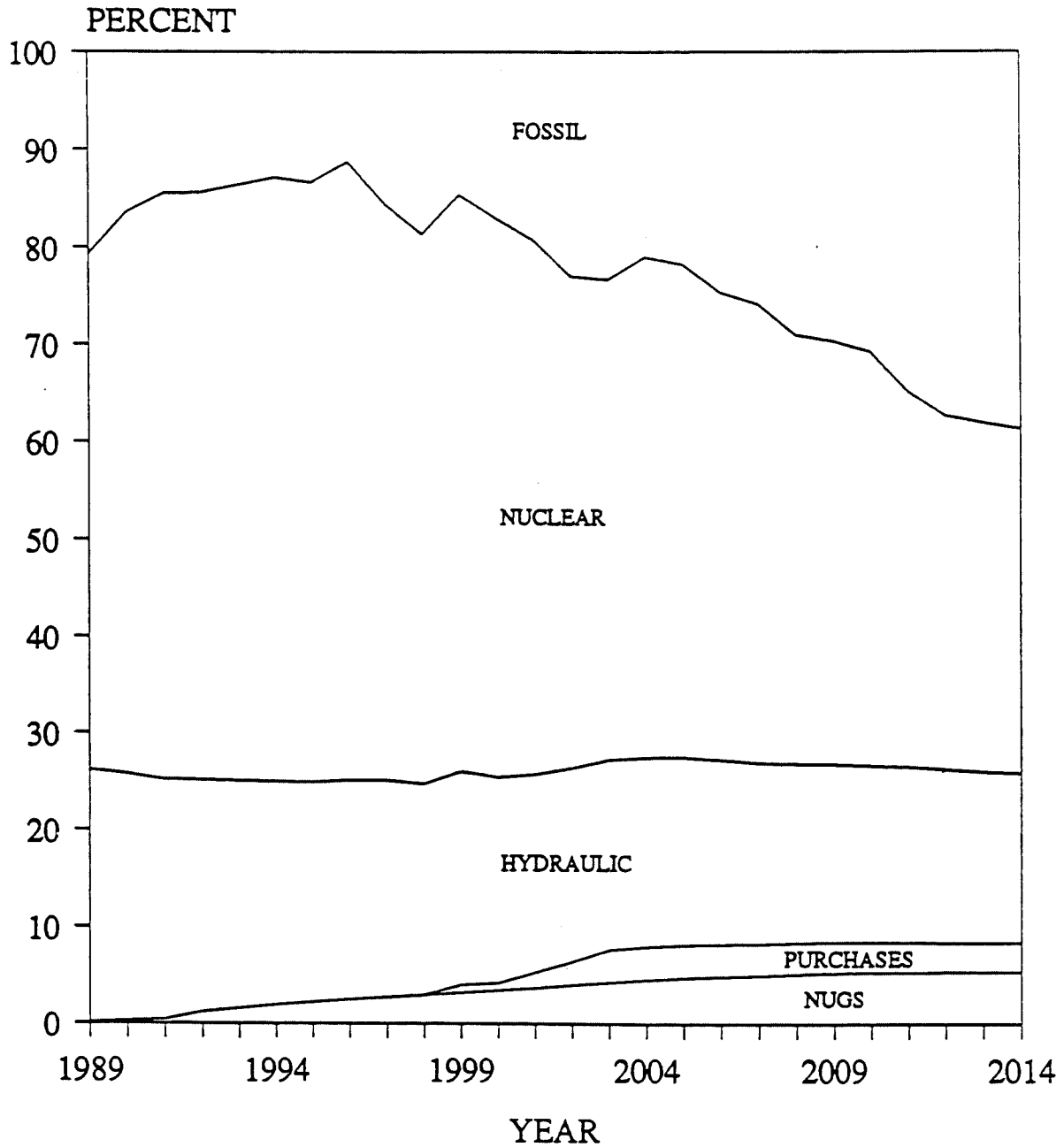
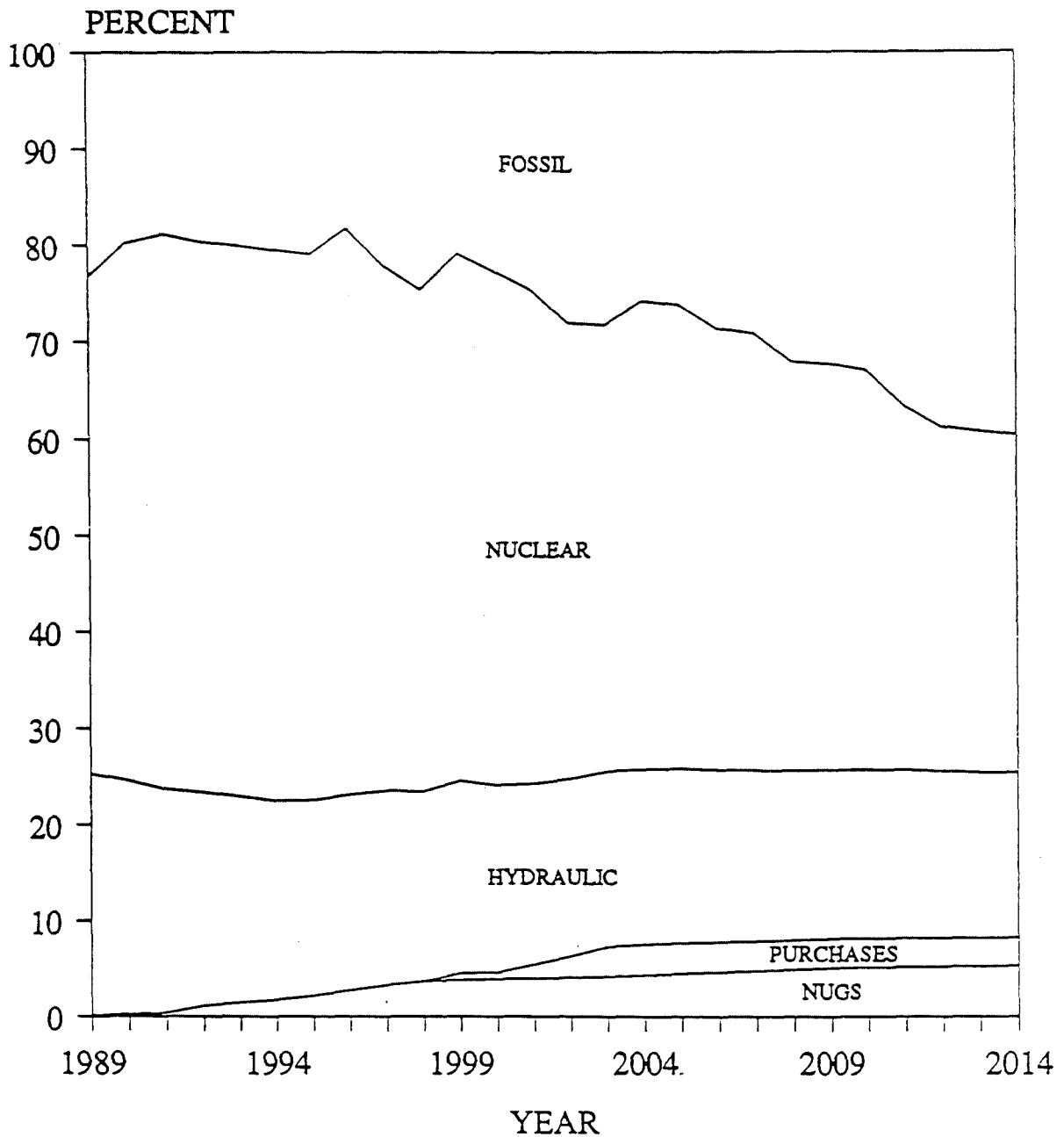


FIGURE 6-10(e)
ENERGY DIVERSITY - CASE 26
(UPPER LOAD FORECAST)



6.4.2 Mix Of Fossil And Nuclear Energy Production

Case 23

Under the five load paths, the fraction of nuclear production rises from an average of about 53% in 1989 to about 72% by 2014. Consequently, fossil energy production declines from about 21% in 1989 to less than 1% by 2014.

Cases 22 and 15

These two Cases have similar nuclear/fossil energy use trends, as well as similar portions of nuclear/fossil energy production, under common load forecasts.

Under the median, branch lower and branch upper load paths, nuclear generation supplies 53% of total energy needs in 1989. By 2014, Case 22 has 67% to 71% nuclear energy and Case 15 has 65% to 67%, depending upon load forecast. As a result, fossil energy production varies from 21% of total energy in 1989 to about 3% to 5% in Case 22, and about 6% to 7% in Case 15.

Under lower load forecast, nuclear energy production starts at 55% of total energy, and rises to about 66% by 2014. Fossil energy production declines from 18% of total energy to about 4% by 2014.

Under upper load forecast, nuclear energy production increases from 51% of total energy in 1989 to about 71% by 2014. Fossil energy production decreases from 23% of total energy in 1989 to about 3% to 4% by 2014.

Case 24

Case 24 follows the same nuclear/fossil production pattern as Cases 22 and 15. Nuclear generation in Case 24 provides a lower portion of total energy than the other two Cases, while fossil generation provides a higher portion.

Under the median, branch lower and branch upper load paths, nuclear energy production increases slightly from 53% of total energy in 1989 to about 56% to 58% by 2014, depending upon load forecast. Fossil energy production decreases from 21% of total energy in 1989 to about 15% to 17% by 2014.

Under lower load forecast, nuclear increases from 55% of total energy in 1989 to 59% by 2014, while fossil decreases from 18% of total energy to 12%.

Under upper load forecast, the nuclear portion rises from 51% in 1989 to 62% by 2014. The fossil portion declines from 23% to 13%.

Case 26

To about the turn of the century, Case 26 follows the same trends as the other Cases. After the year 2000, nuclear energy production decreases steadily and fossil generation increases.

Under median load forecast, nuclear energy production is about 39% of total energy by 2014 and fossil energy production is about 34%. Under branch lower and lower load forecasts, nuclear is about 44% of total energy, on average, and fossil is about 27%. Under branch upper and upper load forecasts, the nuclear and fossil portions are 35% and 39% respectively.

6.5 REVIEW

Energy production and the amount of fuel required to produce that energy are calculated using computer models, as part of the assessment of the economic and environmental impacts of demand/supply plans.

To meet the electricity demands of Ontario, purchases are made from US and Canadian utilities and non-utility generators. The balance of energy needs is supplied by Ontario Hydro's generation.

Ontario Hydro generating stations are fuelled with one of the five energy sources: uranium, coal, oil, gas and falling water. Each station's production is driven by the system operating strategy, which is to minimize the total cost of providing electricity to customers while meeting environmental requirements and standards. The order of generation, by least operating cost, is hydraulic, nuclear and fossil.

Energy production and fuel consumption estimates have been made for the five Cases under each of the five load forecast paths.

All five Cases feature the 1000 MW electricity purchase from Manitoba and hydraulic development program for all the load forecasts. Energy purchased from non-utility generators is the same in all Cases for each of the five load forecasts.

Together, utility and non-utility purchases and hydraulic generation provide about 25% to 30% of total energy requirements. Nuclear and fossil generation make up the remaining energy needs. The pattern of variation of nuclear and fossil energy mix is generally similar across all load forecasts. The main difference under different load forecast is the level of nuclear and fossil energy production.

The variation of nuclear energy production between Cases is mostly due to in-service dates for new nuclear facilities. From 1989 to 1996, nuclear production rises as Darlington comes into service and existing nuclear units, unavailable during retubing, are returned to service. Subsequently, nuclear energy production drops because of retubing one or two generating units at times and retirement of Pickering A units beginning in 2011.

Fossil energy production fluctuates with nuclear production -- rising during nuclear retubing, falling when new nuclear units come into service. The variation of fossil energy production between Cases is due to the timing and type of supply additions. Fossil energy production varies more widely than the other supply options, as fossil is generally used to meet demands after contracted utility and non-utility purchases, hydraulic and nuclear generation are fully utilized.

7. ACID GAS CONTROL

- 7.0 INTRODUCTION
- 7.1 ORIGINS OF ACID GAS EMISSIONS
- 7.2 ACID GAS EMISSION REGULATIONS
- 7.3 ACID GAS CONTROL STRATEGY
- 7.4 EMISSION CONTROL OPTIONS
- 7.5 ACID GAS CONTROL PLAN
- 7.6 ANNUAL ACID GAS EMISSIONS
- 7.7 ANALYSIS DATA
- 7.8 REVIEW

7.0 INTRODUCTION

The emission of acid gases from Ontario Hydro's fossil-fired generating stations is constrained by regulated limits imposed by the Ontario government. In order to ensure that the electricity demand in Ontario can be satisfied while remaining within the enacted regulations, Ontario Hydro must implement acid gas control measures where and when required. This chapter describes the approach for developing an acid gas control plan and the control plan assumed in the plan analysis.

7.1 ORIGINS OF ACID GAS EMISSIONS

Acid gas emissions are produced by the combustion of fossil fuels, such as coal, oil and natural gas. The major components of these emissions are sulphur dioxide (SO_2) and nitrogen oxides (NO_x).

Sulphur dioxide originates from the sulphur and sulphur compounds contained in the fuel. The coal and oil burnt by Ontario Hydro contains 0.3 to 2.5 percent sulphur. During combustion, 95% or more of this sulphur is released and oxidized to form SO_2 . The balance of the sulphur is retained in the ash. Natural gas as supplied, on the other hand, contains essentially no sulphur.

At ground level, high concentrations of sulphur dioxide is detrimental to plant and animal life, and human health. As a result, the Ontario Ministry of the Environment has established ambient air quality criteria for sulphur dioxide.

Nitric oxides are formed when organic nitrogen compounds in fossil fuels oxidize during combustion, and when atmospheric nitrogen is oxidized at temperatures above 1000°C . The NO_x emissions arising from atmospheric nitrogen are significantly affected by boiler design and operation.

In sunlight, nitric oxides react with volatile organic compounds (VOCs) to produce photo-oxidants, primarily ozone. At ground level, ozone affects plant and animal life. It is also thought to play a role in the further oxidation of SO_2 to create acid rain.

Both SO_2 and NO_x acidify natural precipitation, thereby creating "acid rain".

7.2 ACID GAS EMISSION REGULATIONS

Ontario Hydro's fossil generation is constrained by limits placed on acid gas emissions. Under the Environmental Protection Act, Ontario Regulation 281/87 sets the following limits on Ontario Hydro's annual acid gas emissions:

1. To the end of 1989, emissions of sulphur dioxide and nitric oxide must not exceed 430,000 tonnes, of which no more than 370,000 tonnes may be sulphur dioxide;
2. From 1990 to the end of 1993, emissions of sulphur dioxide and nitric oxide must not exceed 280,000 tonnes, of which no more than 240,000 tonnes may be sulphur dioxide;
3. In 1994 and subsequent years, emissions of sulphur dioxide and nitric oxide must not exceed 215,000 tonnes, of which no more than 175,000 tonnes may be sulphur dioxide.

These regulations are in addition to the ambient air quality criteria. Figure 7.2-1 shows the current legislated annual acid gas emission limits and Ontario Hydro's acid gas emissions since 1982. Acid gas emissions are continually assessed so that appropriate measures can be undertaken to ensure that these regulation limits are not exceeded.

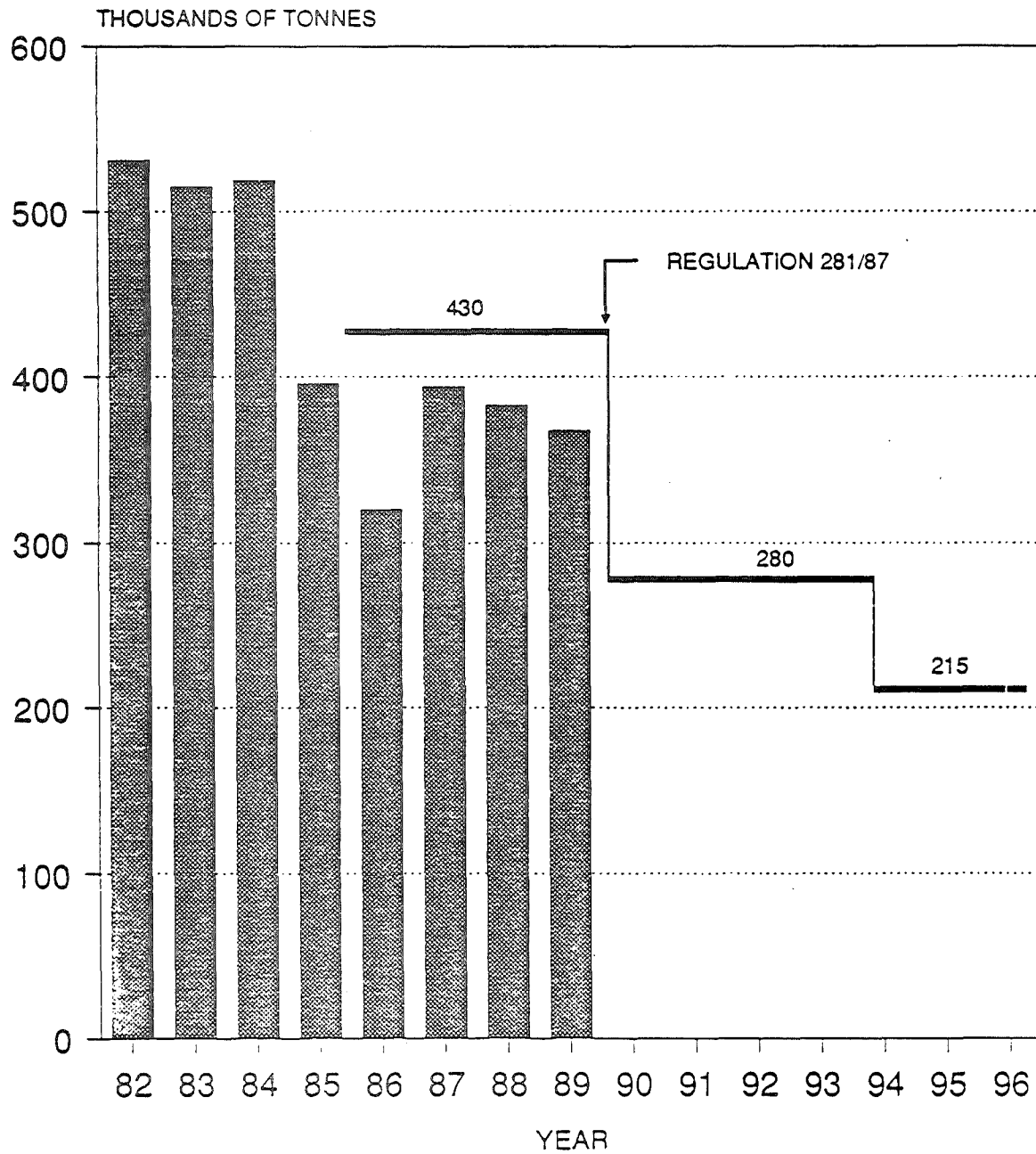
7.3 ACID GAS CONTROL STRATEGY

In managing acid gas emissions to protect the environment, Ontario Hydro's acid gas control policy is to:

1. Meet or better government regulated limits;
2. Aim for stepped reductions in each year to 1994; and
3. Achieve reductions in a cost effective manner.

The actions selected by Ontario Hydro to meet emission regulations follow an underlying acid gas control strategy. This strategy sets out principles for implementation of acid gas control measures, consistent with Ontario Hydro's acid gas control policy.

FIGURE 7.2-1
Ontario Hydro Acid Gas
Emissions and Limits



The three elements of this strategy are:

I *Select cost effective measures on the basis of marginal cost to the system.*

Ontario Hydro selects control measures which achieve lowest marginal costs for emission reduction. In making these selections, Hydro takes into account practical constraints, such as lead time, removal efficiency, future control needs, and station retirements.

A range of control measures is utilized. Using a number of measures mitigates against the failure of one, and provides a broader base for expansion of control. As well, economic benefits may be realized through competition between comparable measures.

II *Maintain adequate flexibility to respond to deviations from expectations.*

Fossil generation needs can vary significantly if there is a change in:

- a) the demand for electricity;
- b) the status of other generating stations; and
- c) demand management or non-utility generation.

In the past, there has been a number of circumstances which have led to significant changes in electricity production from fossil fuel generation:

1. A combination of a strong economy and hot summer weather helped create a demand for electricity in 1988 that was 4.7 TW.h higher than forecast.
2. In 1985 the outage of two units at Pickering for retubing resulted in a loss of over 7.5 TW.h of nuclear energy per year for several years.
3. Annual hydraulic generation has varied over the past 10 years from a low of 33.5 TW.h to a high of 38.8 TW.h, a range of 5.2 TW.h.

Continued variability in fossil generation use is expected. Ontario Hydro manages the acid gas implications of these uncertain fossil generation needs by maintaining the flexibility to handle a range of future conditions.

Some of this flexibility is provided by the inclusion of an acid gas planning margin. Ontario Hydro maintains an annual planning margin of at least 9 TW.h, equivalent to approximately 3 million tonnes of additional coal, or approximately the electricity production from a large nuclear unit for a year.

A planning margin is necessary because emissions must be below the regulated limit in every year, not just on average. The size of the margin is determined by balancing the costs of carrying the extra margin with the risks of having to use more expensive last minute measures to meet the emission limits. With an annual planning margin of 9 TW.h, Ontario Hydro should be able to keep acid gas emissions below the limits without having to frequently resort to last minute measures.

Since approvals for certain control options take a long time (3 years or more), some approvals are being pursued in advance of commitment dates. In February 1988, following two years of development, Ontario Hydro submitted an Environmental Assessment to the Ontario Government, which sought approval for the use of any of four different acid gas control technologies at any of its three major coal-fired stations. Approval, with certain conditions, was granted in 1989.

III Keep sufficient options in reserve to meet unforeseen contingencies.

Certain measures are held in reserve for use on short notice in the event of contingencies such as higher than forecast load growth and/or problems with hydraulic or nuclear units. These generally are more expensive than those in the acid gas control plan.

7.4 EMISSION CONTROL OPTIONS

7.4.1 Reduce the Use of Fossil Generation

Demand Management, non-utility generation*, hydraulic and nuclear generation, electricity imports, reducing planned sales, and transmission improvements reduce acid gas emissions by displacing fossil-fired generation.

Although demand for electricity increased over the 1970s and 1980s, it was largely met by new nuclear generation. As a result, acid gas emissions did not increase in proportion to the increase in electricity demand. As well, the nuclear generation capacity additions during this time period were able to displace existing fossil-fired generation, thereby further reducing emissions.

There can also be economic benefits associated with reductions in fossil generation. This occurs when the measure undertaken to displace fossil generation results in lower overall system costs.

7.4.2 Reduce the Sulphur Content in Fuel

Acid gas emissions can be reduced by burning lower sulphur coals, natural gas, or lower sulphur oil.

The two most recently constructed Ontario Hydro coal-fired stations, Atikokan TGS, and Thunder Bay TGS units 2 and 3, are designed and operated to burn low sulphur (0.4% S) lignite supplied from Western Canada. SO₂ emission rates from these stations are significantly lower than those from Ontario Hydro's other coal stations, which utilize higher sulphur bituminous coals.

Ontario Hydro has reduced acid gas emission rates by steadily lowering system average sulphur levels in coal, from 2.4 percent in 1976 to 1.3% in 1988. Further reductions, however, are not feasible without modification of the coal-fired stations.

* Combustion based non-utility generation facilities will emit acid gases, but the majority will be natural gas fuelled. These are expected to emit less NO_x per kW.h than Hydro's existing fossil stations because of their higher efficiency (eg. cogeneration). As well, natural gas fuelled generators emit only negligible amounts of SO₂.

All of the coal-fired stations in Southern Ontario are designed to burn medium to high sulphur U.S. coal*. The burning of lower sulphur coals in these stations leads to degraded precipitator performance and increased particulate emissions. The most economical way to overcome this is to utilize flue gas conditioning.

Sulphur trioxide/ammonia flue gas conditioning will be installed at three stations -- Lambton TGS, Nanticoke TGS and Lakeview TGS. Work at Lambton TGS and Nanticoke TGS will be completed in 1990, while work at Lakeview TGS will be completed from 1990 to 1994, as part of the general rehabilitation of the station. Flue gas conditioning will permit the burning of low sulphur coal at these stations, providing up to a 50 percent decrease in acid gas emissions over original design.

The use of lower sulphur fuels depends on the cost of the fuel, the cost of the station and infrastructure modifications required to burn the low sulphur fuel, and the lead-time available. A major advantage of using or switching to low sulphur fuels is the relatively short lead-time required.

Low sulphur fuel options characteristically have low capital costs and high fuelling costs. This makes them more practical for use on low capacity factor generating units or with generating units with limited remaining operating life. Fuelling costs are high because low sulphur fuels come at a premium.

7.4.3 Retrofit Emission Control Equipment

SO₂ emission control

SO₂ emission control equipment includes high efficiency scrubbers and injection technology. High efficiency scrubbers remove SO₂ from flue gases, and are up to 95% effective in reducing SO₂. Injection technologies, on the other hand, add chemicals during the combustion process. These chemicals combine with the SO₂ within the furnace, creating compounds which are then recovered. Injection technologies are up to 50% effective.

* Nanticoke TGS currently burns a 50:50 blend of medium sulphur U.S. coal and low sulphur Western Canadian Coal.

High efficiency scrubbers are proven and commercially available technology. While they carry a relatively high capital cost (\$250 M per pair of units*), they have a relatively low operating cost (\$15 M per year).

As a result, scrubbers are most cost effective when applied to high use generating units with relatively high SO₂ emissions and significant remaining operating lives. With high long-term use, the "low" operating costs tend to offset the "high" initial capital investment.

Scrubbers permit the use of less expensive higher sulphur coal in place of the low sulphur coal that would otherwise be used to reduce emissions. Savings on coal also offset the high initial capital investment. Savings depend on the fuel price differential between low and high-sulphur coal and the level of uncertainty in fuel price forecasts.

The retrofit of scrubbers to existing generating units takes up to a total of eight years. This includes the time required for tendering engineering, and approvals. Actual construction takes about three years.

Three scrubber processes are best suited to Ontario Hydro's coal-fired stations. All have advantages and disadvantages that will influence which option is selected for each station.

Wet Limestone Slurry Process

The most widely applied flue gas scrubbing alternative is the Wet Limestone Slurry (WLS) process. It uses limestone, mixed with water to form a slurry, as the scrubbing agent to remove SO₂ from the flue gas. The limestone slurry reacts with SO₂ to form waste by-products consisting mainly of calcium salts. The waste by-products leave the scrubber in a fluid stream, for either processing into saleable gypsum or disposal.

Advantages are: limestone is a comparatively inexpensive and abundant scrubbing agent; extensive utility operating experience; and proven reliability and availability. Disadvantages include: high capital costs and high operating costs.

* To minimize costs and make the best use of common equipment, scrubbers are installed on pairs of generating units.

Limestone Dual Alkali Process

A variation of the WLS process is the Limestone Dual Alkali process. It uses a clear sodium sulphite/bisulphite scrubbing solution to remove the SO_2 from the flue gas. The spent scrubbing solution is then regenerated by reaction with a limestone slurry. The sodium sulphite solution is reused in the scrubber, while the reacted slurry is collected and disposed of as in the WLS process.

Advantages are: lower maintenance costs than WLS; high SO_2 removal efficiency (above 90 percent) over a wide range of coal types; low operating costs; and operational flexibility. Disadvantages are: limited utility experience; need to purchase and store an extra scrubbing reagent; and soluble sodium salts contained in the waste material.

Lime Spray Dryer Process

A scrubber alternative with application in both utility and industrial applications is the Lime Spray Dryer Process. In this process, SO_2 is removed by a lime slurry sprayed into the flue gas stream. The water in this slurry evaporates within the gas stream. The reacted lime is then removed as a dry by-product.

Advantages are: reduced operating and maintenance costs; reduced potential for equipment wear; and simplified waste handling and disposal. Disadvantages include: lower SO_2 removal efficiency; limited commercial operating experience on high sulphur coals; high cost of lime; and high capital costs.

Injection technologies have lower capital costs and higher operating costs than high efficiency scrubbers. Thus, they are most cost effective when restricted to generating units with peaking operations.

Versus scrubbers, injection technology takes less time to implement in retrofit applications. This is largely due to the difference in construction lead times. Injection technology takes one to two years for construction versus three years for scrubbers.

The injection process best suited to Ontario Hydro's coal-fired stations is the Sorbent Furnace Injection Process:

Sorbent Furnace Injection absorbs SO_2 within the boiler rather than in a specially designed scrubber. Finely ground limestone, or other reagent, is injected into the boiler, where it reacts with the SO_2 in the gas stream to form calcium sulphate and sulphite. This is then collected along with the flyash at the back end of the boiler.

Advantages are: short lead times and low capital costs. Disadvantages are: lack of utility operating experience; low removal efficiency (about 50 percent); high operating costs; and wastes may require specialized handling.

NO_x emission control

NO_x control equipment includes combustion process modifications, injection technologies and Selective Catalytic Reduction (SCR).

One example of combustion process modification is the installation of low NO_x burners in the boiler. Nitrogen oxide emissions from Nanticoke TGS have been reduced 35 percent by the modification of burners on all units. These modifications were carried out from 1984 to 1987.

Further improvements can be made through various combinations of new pulverisers, windbox modifications, control changes, overfire air ports and burner modifications. These measures reduce the formation of NO_x by reducing the temperature of combustion and the amount of oxygen available for combustion. The cost of further combustion process modifications is about \$30M for a 500 MW unit. Operating costs would be low. It is estimated that these measures would provide NO_x reduction capabilities of up to 30 percent from current emission levels.

Combustion process modification can be a cost effective means of reducing total acid gas emissions in certain instances. It is particularly attractive when its use can avoid the implementation of higher cost SO_2 control options, or can meet a critical need for accelerated implementation of acid gas control. The latter would be a consequence of the shorter design and construction times required for this option.

Promising injection technologies such as urea injection are being developed as NO_x control measures. In simple terms, chemicals are injected into the furnace where they react with the NO_x produced to either form nitrogen and water or create other readily collected compounds. With these technologies, NO_x reductions of 50 to 60 percent are expected. Further research on these technologies is required, however, as they have yet to be proven on the commercial scale required by Ontario Hydro.

In Selective Catalytic Reduction, ammonia is injected into the flue gas stream. The flue gas/ammonia mixture then passes over a catalyst bed in a reactor vessel, where NO_x is reduced to nitrogen gas and water. SCRs offer a removal efficiency of 80 percent or greater. Capital costs are about \$60 M per 500 MW unit. Operating costs will be high as they are driven by the catalyst lifetime and replacement costs. Although SCR has yet to be run on North American coals and stations, units are operating successfully in Japan and parts of Europe.

Future generating stations will be built with sufficient control equipment to mitigate their environmental impact. Thus, it is expected that any new pulverized coal station built by Hydro will have SCR units or equivalent.

7.5 ACID GAS CONTROL PLAN

Representative Acid Gas Control Plans were developed for use in all of the cases in the DSP. The plans combine a variety of control options into separate representative control programs for each of the five load forecasts analyzed. While each program is capable of meeting current emission regulations, the options may be reduced or supplemented as required in the future.

7.5.1 Formulating an Acid Gas Control Plan

In developing an acid gas control plan, the following steps are taken:

1. The annual fossil energy requirement for the plan is calculated, either by station or group of units.
2. On a year-by-year basis, the control options for each fossil unit are specified.
3. For each year of the forecast period, the combination of available control options which results in the lowest marginal cost for emission reduction, that meets the regulation and provides a 9 TW.h margin, is selected.

4. Practical constraints such as operating life and lifetime costs are taken into account. For example, scrubbers are not selected if required for only a year .

The marginal removal costs (\$/Mg_{removed}) for each control option vary by station, by station annual capacity factor (i.e. usage) and by year. An illustrative example of these costs are given in Figure 7.5-1 for Lambton TGS and Nanticoke TGS in the year 2000. Similar data are calculated for each year of the planning horizon. These are then used to determine the most cost effective option for reducing acid gas emissions in each year.

FIGURE 7.5-1

ILLUSTRATIVE MARGINAL COSTS
FOR ACID GAS CONTROL OPTIONS
(year 2000 \$)

OPTION	MARGINAL COST*		
	(\$/Mg _{removed})		
	Lambton TGS (70% ACF)	Nanticoke TGS	
		(31% ACF)	(13% ACF)
100% Western Canadian Coal (No Loss of Capability)	744	963	1203
100% Low Sulphur U.S. Coal	310	158	158
50/50 Blend Western Canadian/U.S. Low Sulphur Coal	604	558	633
Scrubber High Sulphur U.S. Coal With Low NO _x Burners	217	708	2241
Limestone Injection	683	1677	3664
20% Natural Gas With 80% U.S. Low Sulphur Coal	694	815	904
100% Natural Gas	1685	2079	2273

* Relative to 1989 fuel use at stations

As shown in Figure 7.5-1, there can be significant differences in costs between the options and between stations. For example, the use of scrubbers to reduce emissions from generating stations with high annual capacity factors can be cost effective. With Lambton TGS operating at an annual capacity factor of 70 percent, the marginal removal costs of scrubbers is only 217 \$/Mg_{removed}. This is the lowest cost option. However, for Nanticoke TGS units, operating at an annual capacity factor of only 13 percent, scrubbers are amongst the highest

cost options. At low capacity factors, the use of low sulphur coal options are the most economic (eg. 158 \$/Mg_{removed}).

Marginal removal costs provide an indication of the relative cost effectiveness of the various options on a year by year basis. In practice, however, a control option must not only be cost effective in a particular year, but also over the entire remaining life of the station. This is especially true for options such as scrubbers, which require a significant capital expenditure. It is impractical and expensive to utilize such an option for only a year or two. Thus, in developing an acid gas control plan, the long term financial implications must be weighed against short term advantages and disadvantages.

In addition to minimizing costs, an acid gas control plan must recognize uncertainties. The plan must consider a range of possible future coal use, provide a margin to allow for uncertainty, and keep some measures in reserve for contingency response until new, more economical measures can be added to the system.

7.5.2 Acid Gas Control Plan Attributes

Acid gas control will be accomplished through two main options - the retrofit of control equipment to existing fossil stations, and the use of lower sulphur fuel (eg. low sulphur coal). Control equipment consists of either scrubbers or combustion process modifications (CPM) or both. These are designated major control measures as they involve capital modification to the station and require scheduling of design, construction and installation.

Figure 7.5-2 shows the Acid Gas Control Plan in-service dates for these control measures. It is assumed that scrubbers and CPM will be employed initially at Lambton TGS, followed by Nanticoke TGS, where required.

The major control measures provide economic control of acid gas emissions over the long-term. Additional acid gas reductions can be accomplished by the use of lower sulphur coals. The potential exists to obtain US coal with sulphur levels down to 0.8 percent and Western Canadian coal with sulphur levels as low as 0.3 percent. It is estimated that this additional measure will be sufficient to ensure that the regulations can be met in all load forecast cases.

The schedule for the major control measures extends to the year 2005. Beyond that date, no additional measures are planned on existing stations. This is partly due to the retirement shortly thereafter of much of the existing coal-fired capacity and its replacement with cleaner generation.

FIGURE 7.5-2

ACID GAS CONTROL PLAN

PLAN: ALL
PROGRAM: REFERENCE CASE

FORECAST	GAS	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005
LOWER	SO ₂	L12-FGD											
	NO _x	L12-CPM	L34-CPM										
DECREASING	SO ₂	L12-FGD	L34-FGD										
	NO _x	L12-CPM	L34-CPM			N14-CPM							
MEDIAN	SO ₂	L12-FGD	L34-FGD										
	NO _x	L12-CPM	L34-CPM			N14-CPM							
INCREASING	SO ₂	L12-FGD	L34-FGD							N12-FGD	N34-FGD		
	NO _x	L12-CPM	L34-CPM			N14-CPM							
UPPER	SO ₂	L14-FGD		N14-FGD	N58-FGD								
	NO _x		L12-CPM	L34-CPM		N12-CPM	N34-CPM						

LEGEND: FGD - Flue Gas Desulphurization (Scrubbers)
CPM - Combustion Process Modification
L12 - Lambton TGS units 1 & 2
N14 - Nanticoke TGS units 1 to 4

1989 DEMAND/SUPPLY PLAN

Common to all Demand/Supply Plans are a number of items which affect future acid gas emissions. These include: maximum economic demand management and non-utility generation, the orderly development of remaining economic hydraulic resources, transmission improvements, and maximum use of available hydraulic and nuclear generation. Each of these reduce the amount of fossil generation required and, in turn, the production of acid gases. This leaves the retrofit of control measures, new nuclear generation, and utility purchases as the remaining options available to further reduce fossil generation.

A single representative plan for retrofits to existing facilities was applied to all plans. This is largely due to the fact that for a given load forecast, all plans are essentially the same up to the year 2000. Beyond that time there is some variation which is a result of differences in new generation brought into service. In all plans, however, all new generation will have lower acid gas emission rates than the existing generation replaced. Thus, the role of retrofits is to ensure compliance with existing regulations from now to the early 2000s.

The projected acid gas emissions are based on the Acid Gas Control Plan and an assumed fuel program. Over most years in the plan, flexibility is provided by a number of potential measures. Coal sulphur levels can be further reduced by utilizing very low sulphur coals such as Western Canadian coal. Prior to station retirement, R.L. Hearn TGS can be demothballed and operated on natural gas. Alternatively, another existing fossil station could be converted to operate on natural gas. These high cost measures remain in reserve to meet contingencies and load forecasts over and above those planned for.

The Acid Gas Control Plan was applied to each of the Demand/Supply Plans in turn. The fossil fuel specific generation and corresponding acid gas emissions for all cases of each plan were determined and are presented in the following sections.

7.5.3 Fuel Specific Generation

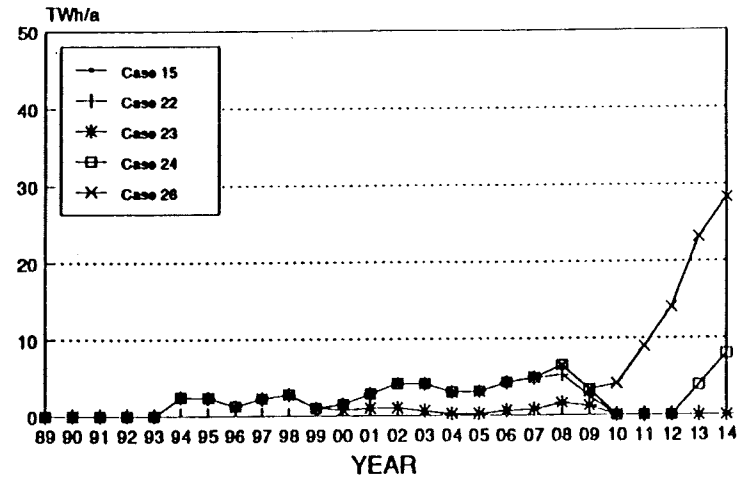
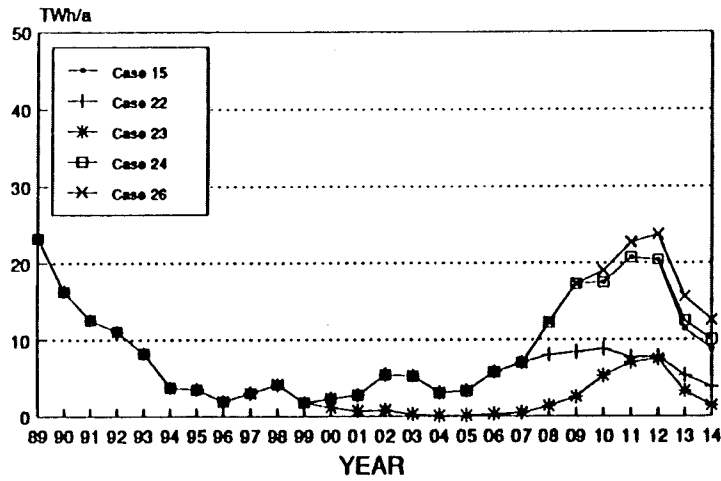
The fossil fuel specific generation for each of the plans and load forecasts is shown in Figures 7.5-3 through 7.5-7. The fossil fuels are separated into four fuel types: scrubbed coal, unscrubbed coal, natural gas/light fuel oil (LFO), and residual oil.

Scrubbed coal refers to the coal utilized by existing fossil generating units equipped with scrubbers or new conventional steam cycle coal stations with scrubbers. It is assumed that these stations would be fuelled with a 2.5 percent sulphur US bituminous coal. Unscrubbed coal generation encompasses the

FIGURE 7.5-3

UNSCRUBBED COAL GENERATION

SCRUBBED COAL GENERATION



LOWER LOAD FORECAST

NATURAL GAS/LFO GENERATION

RESIDUAL OIL GENERATION

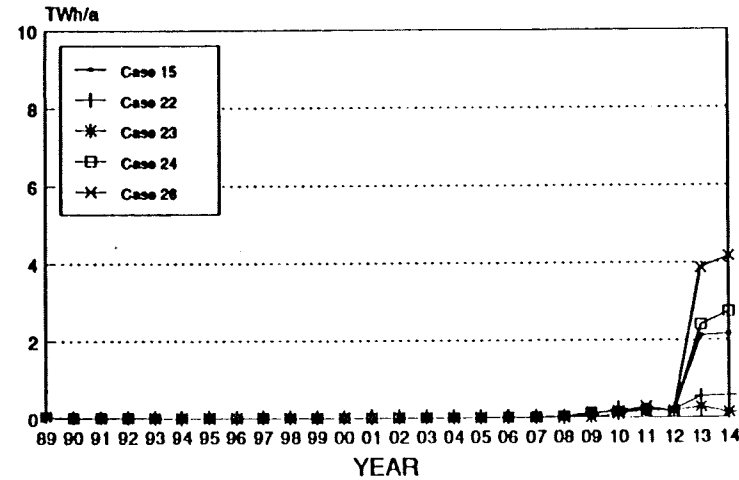
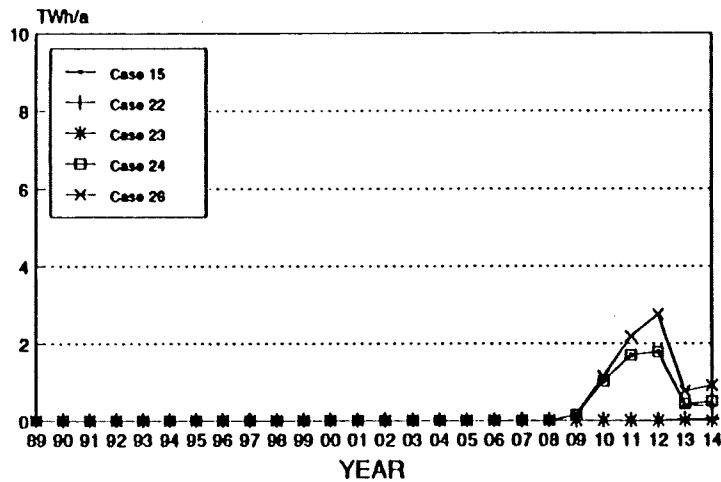
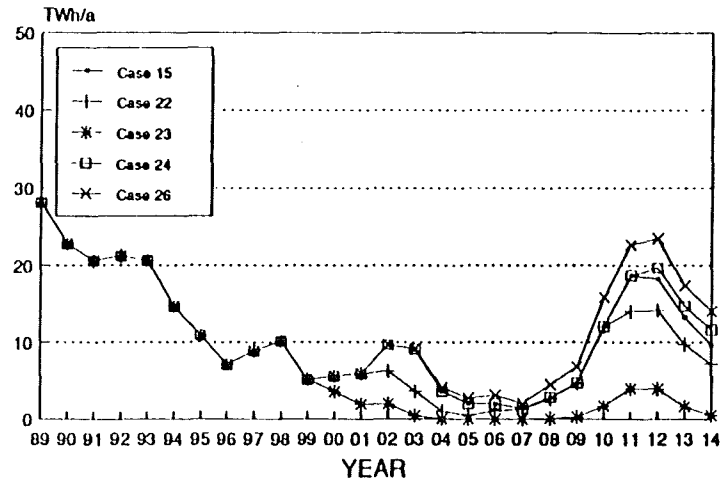
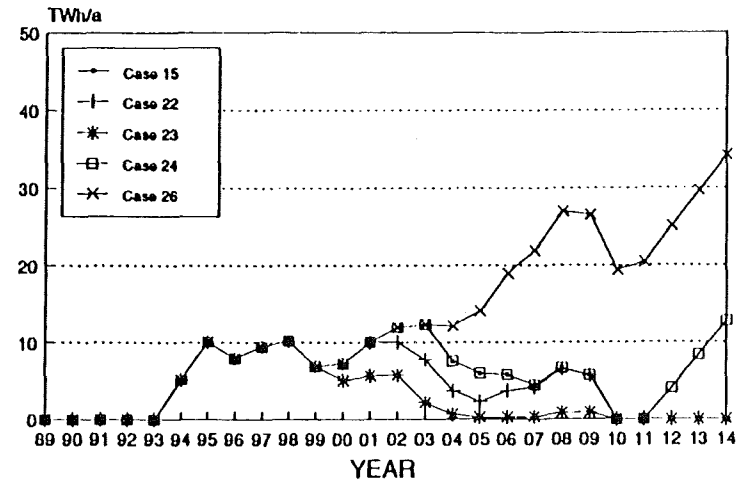


FIGURE 7.5-4

UNSCRUBBED COAL GENERATION

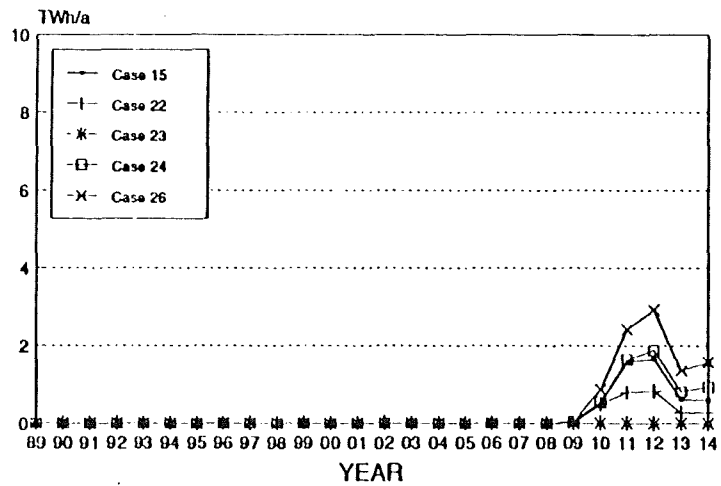


SCRUBBED COAL GENERATION

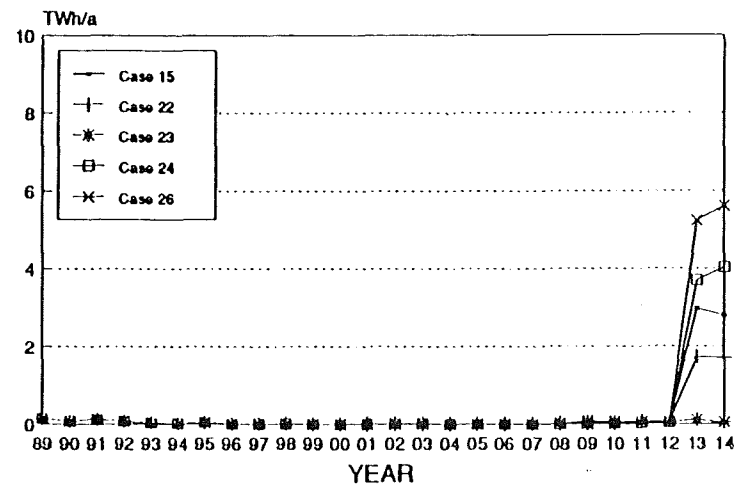


BRANCH LOWER FORECAST

NATURAL GAS/LFO GENERATION



RESIDUAL OIL GENERATION



UNSCRUBBED COAL GENERATION

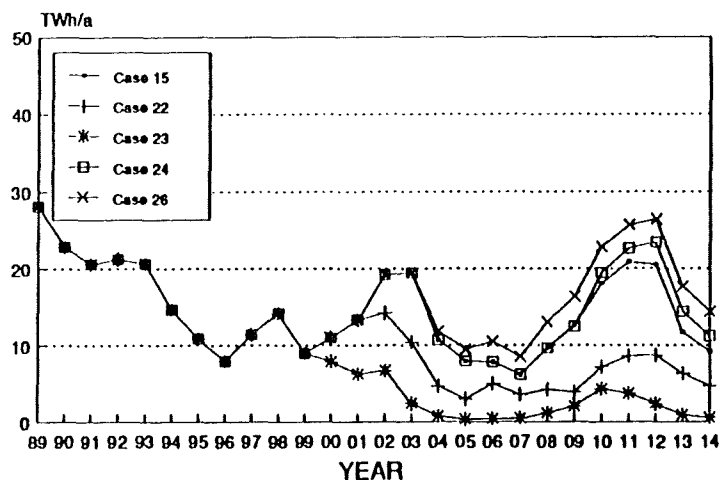
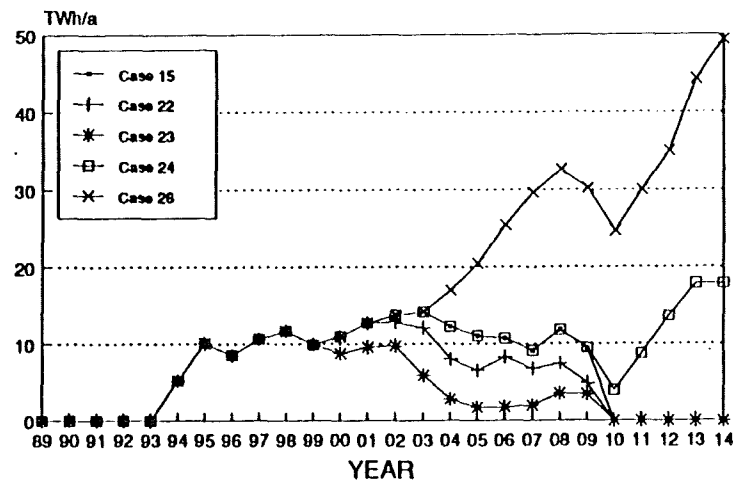


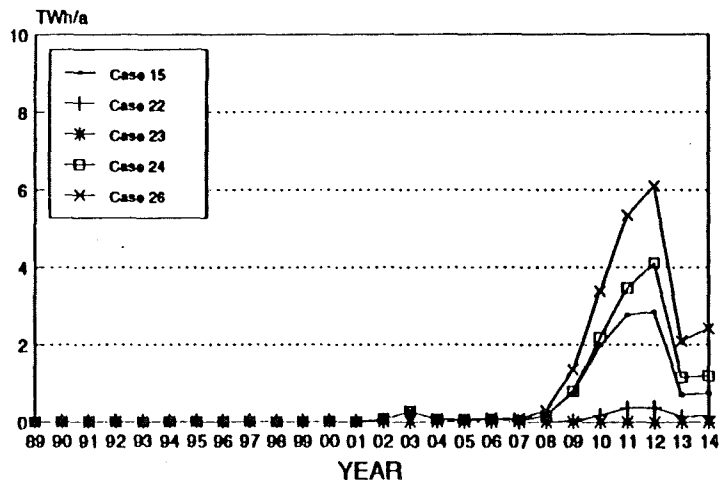
FIGURE 7.5-5

SCRUBBED COAL GENERATION



MEDIAN LOAD FORECAST

NATURAL GAS/LFO GENERATION



RESIDUAL OIL GENERATION

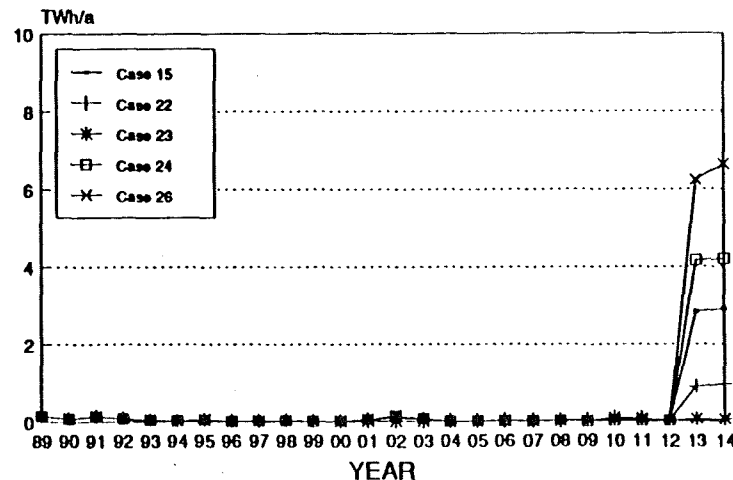
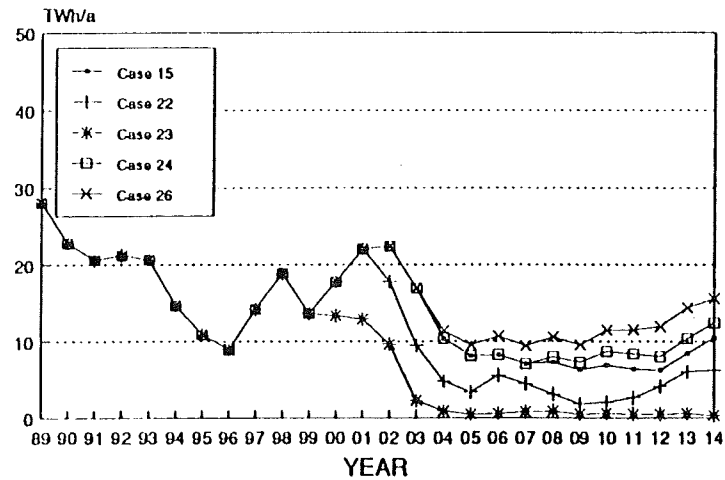
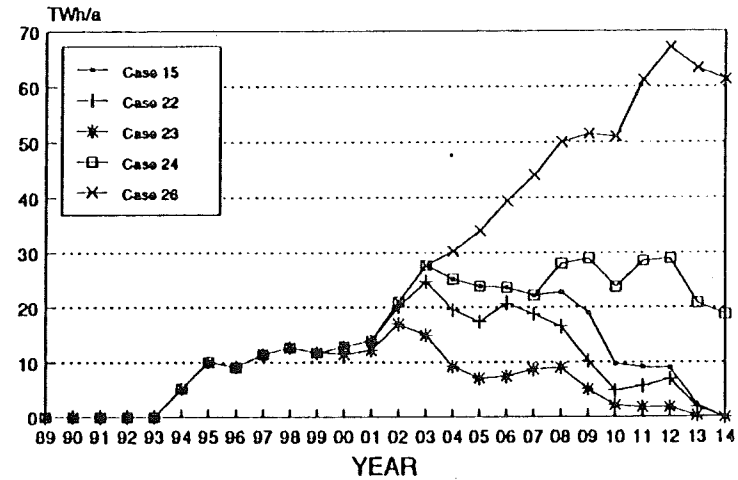


FIGURE 7.5-6

UNSCRUBBED COAL GENERATION

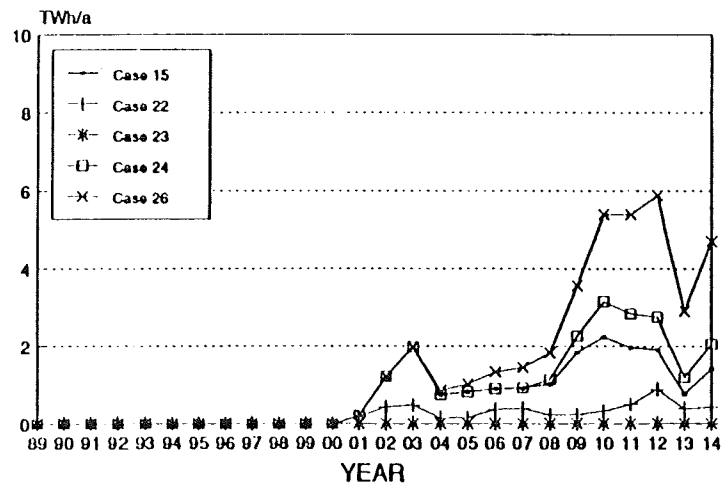


SCRUBBED COAL GENERATION

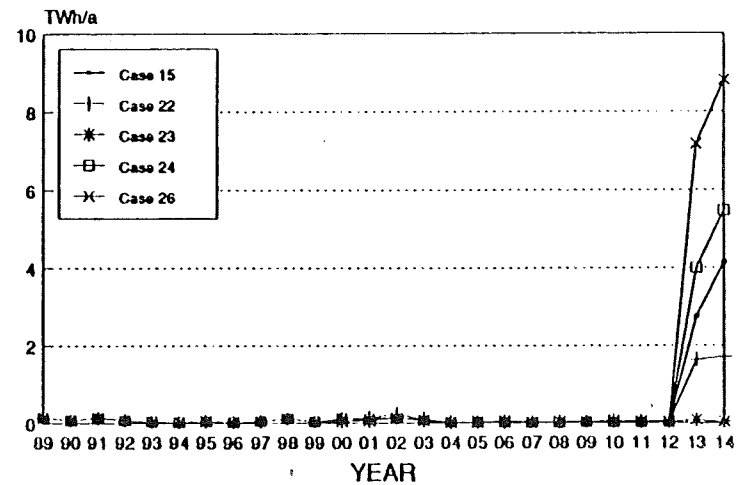


BRANCH UPPER FORECAST

NATURAL GAS/LFO GENERATION



RESIDUAL OIL GENERATION



UNSCRUBBED COAL GENERATION

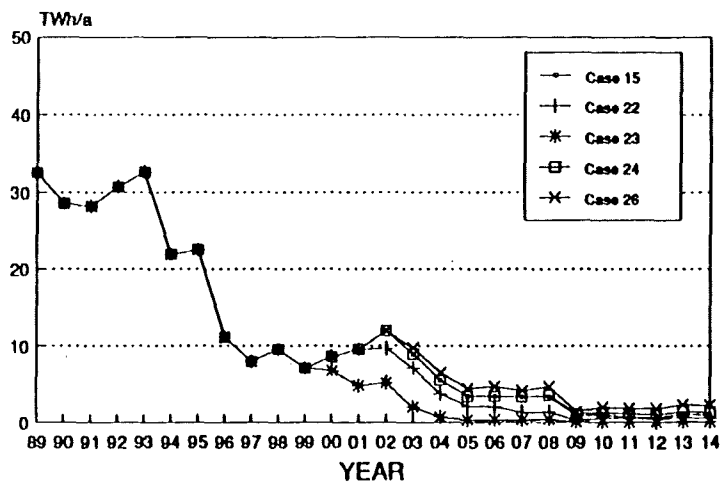
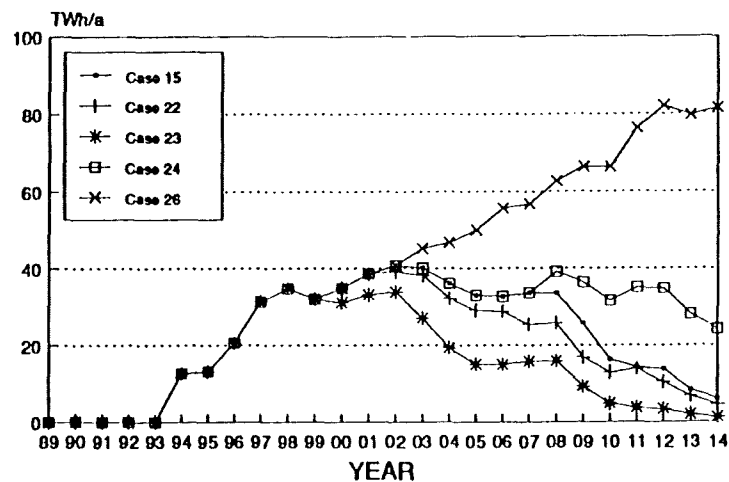


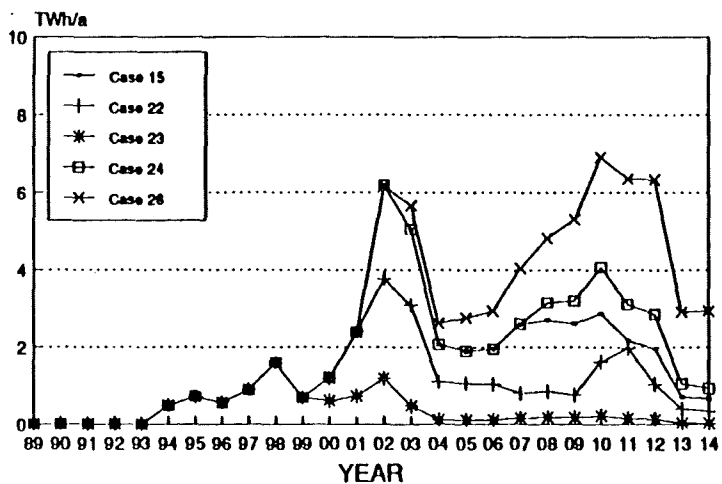
FIGURE 7.5-7

SCRUBBED COAL GENERATION

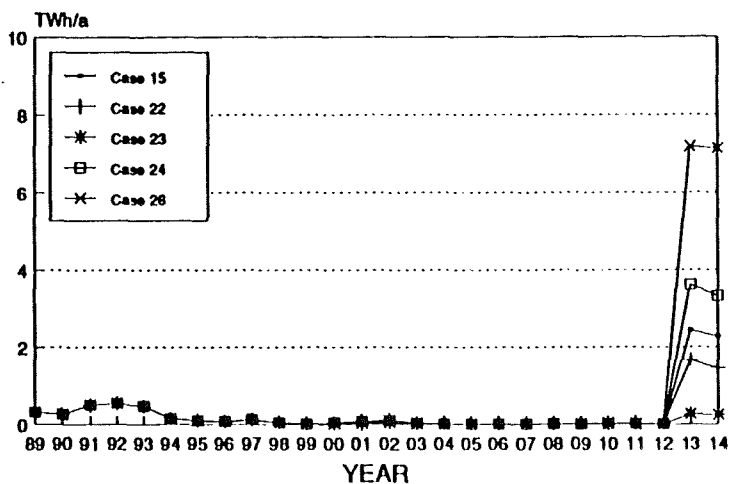


UPPER LOAD FORECAST

NATURAL GAS/LFO GENERATION



RESIDUAL OIL GENERATION



remaining coal used on the system. It includes both lignite and the bituminous coals used in the fossil units on the system which do not have scrubbers. Reduction in coal sulphur content for acid gas control is accomplished by adjustments in the sulphur content of the unscrubbed coal purchases. There is the potential to return R.L. Hearn TGS to service and operate it on natural gas, or to convert an other station such as Lakeview TGS to natural gas operation. In most cases, however, the consumption of this fuel is associated with new CTU and combined-cycle facilities. Residual oil generation is that generation associated with the use of Lennox TGS.

As expected, the fossil fuel specific generation is similar for all of the plans prior to the addition of new supply options. After this point, the fuel specific generation is a function of the type of generation added. Plans with new nuclear generation have the lowest fossil fuel generation and hence lowest fossil fuel requirements.

7.6 ANNUAL ACID GAS EMISSIONS

The estimated total annual acid gas emissions for each of the plans is shown in Figures 7.6-1 through 7.6-5. These are based on the Acid Gas Control Plan presented in section 7.5. Also shown in the figures are acid gas emissions, separated into SO_2 and NO_x . The focus of these estimates is on the long term post 1994 period.

Acid gas emissions are calculated to remain below the regulated limits in all cases. The amount by which the expected emissions are below the regulation represents the planning margin. Typically this corresponds to 9 TWh of additional fossil generation.

The Acid Gas Control Plan contains sufficient control measures to ensure the emission regulations are respected in all cases. In certain cases and under specific load forecasts, this represents more acid gas control equipment than is necessary. For example, in Case 22, branch upper load forecast, a second pair of scrubbers at Nanticoke is not required and could be eliminated. To maintain a consistent acid gas control program across all the cases, such refinements were not attempted.

The lower load forecast case for all plans does not require the retrofit of control measures to meet current acid gas emission regulations. It has been assumed for this case, however, that the installation of a single pair of scrubbers and CPM at Lambton TGS will proceed as currently envisaged.

FIGURE 7.6-1
PROJECTED ACID GAS EMISSIONS
[Case 15]

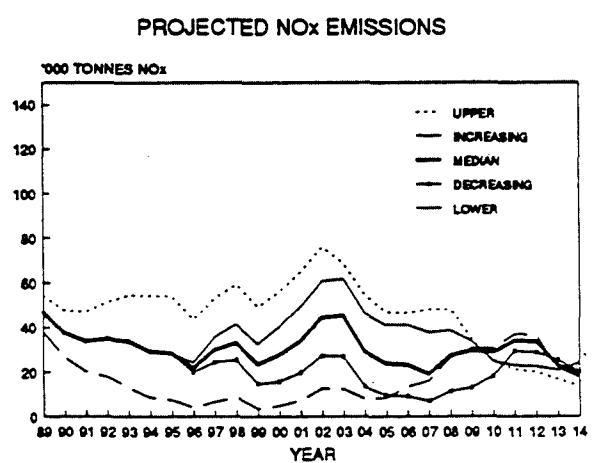
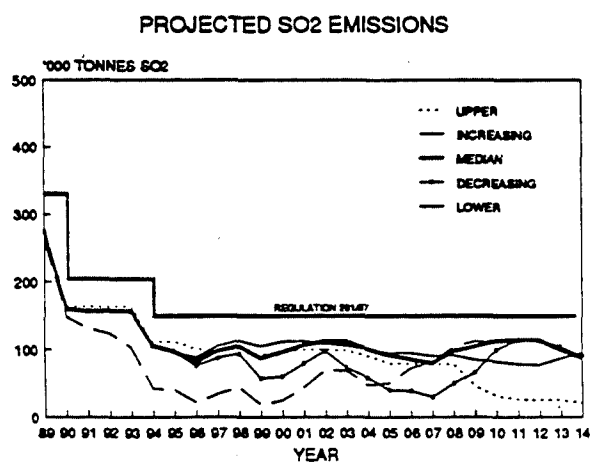
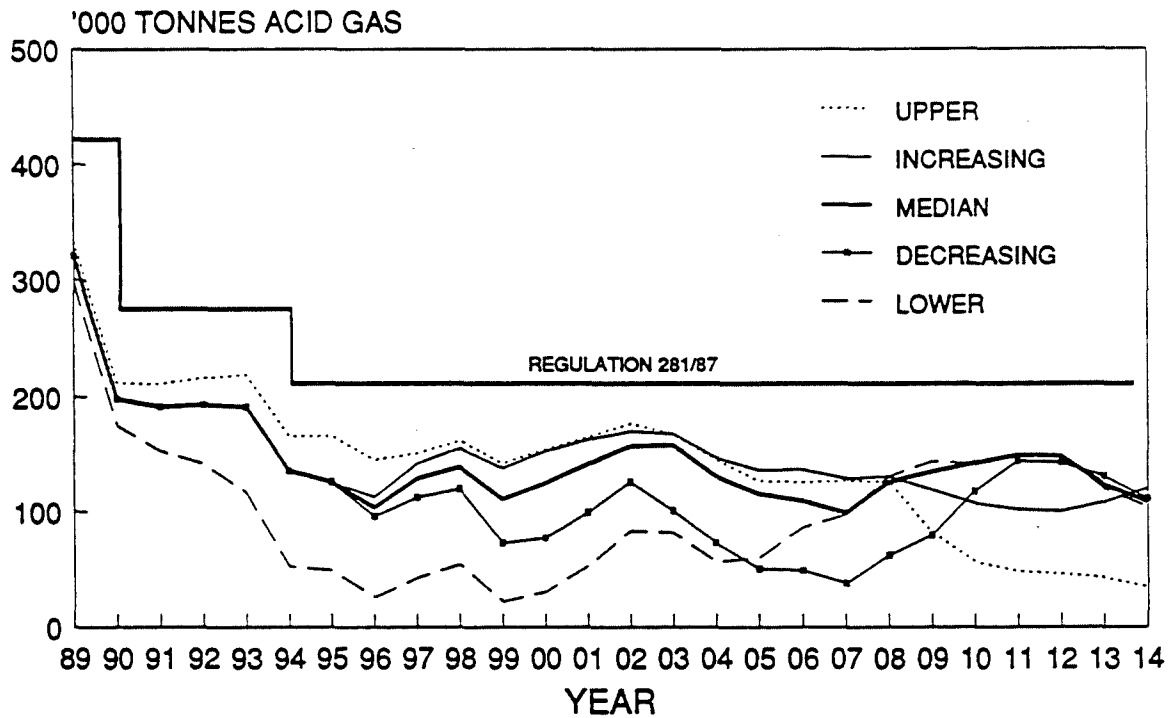


FIGURE 7.6-2
PROJECTED ACID GAS EMISSIONS
[Case 22]

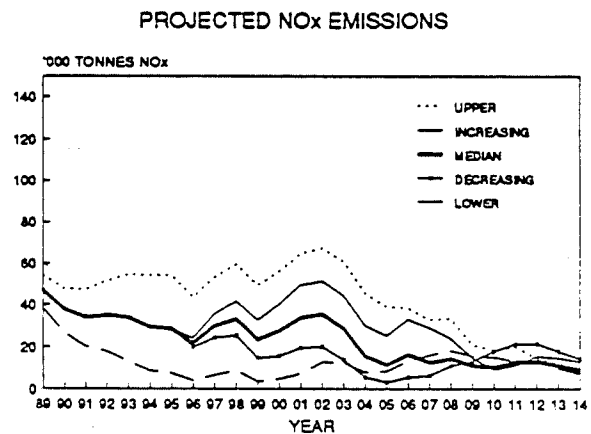
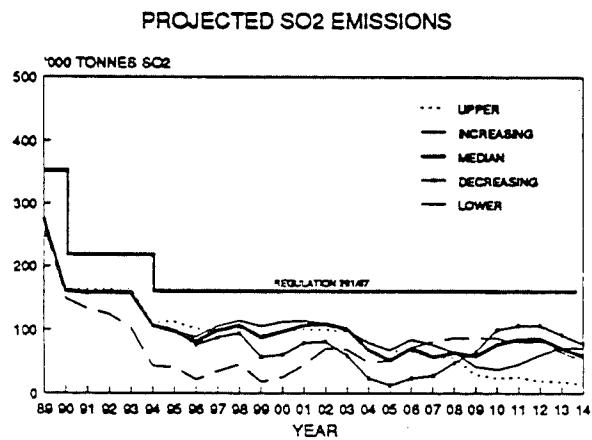
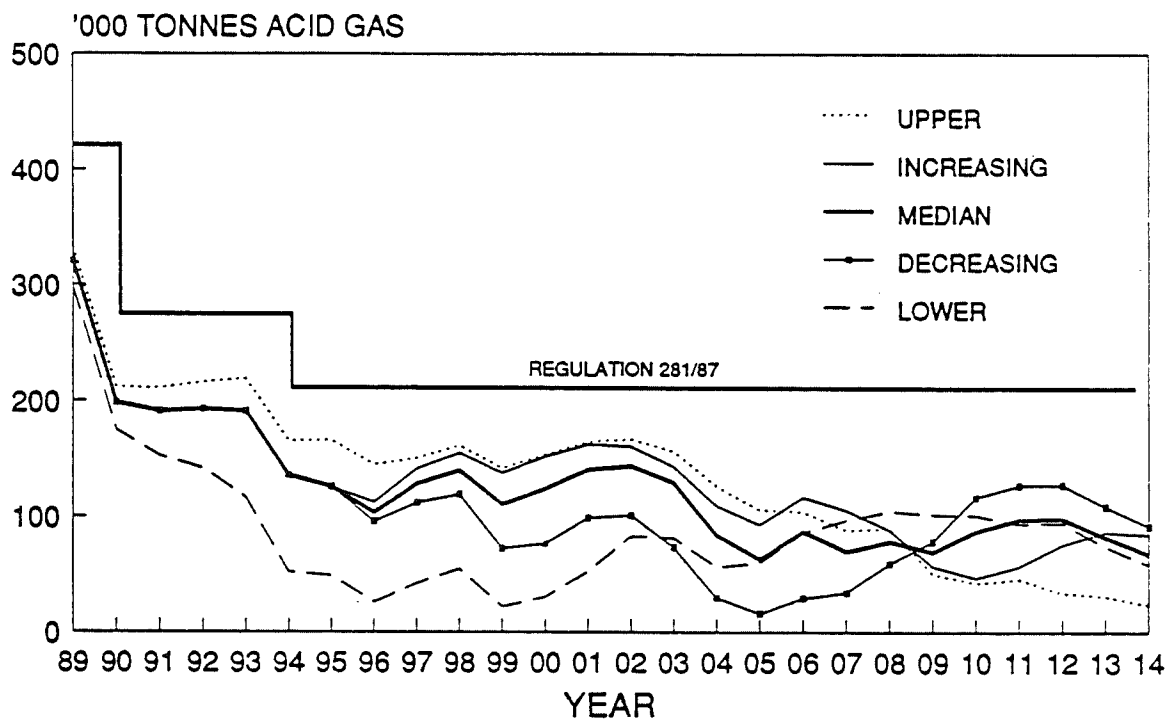
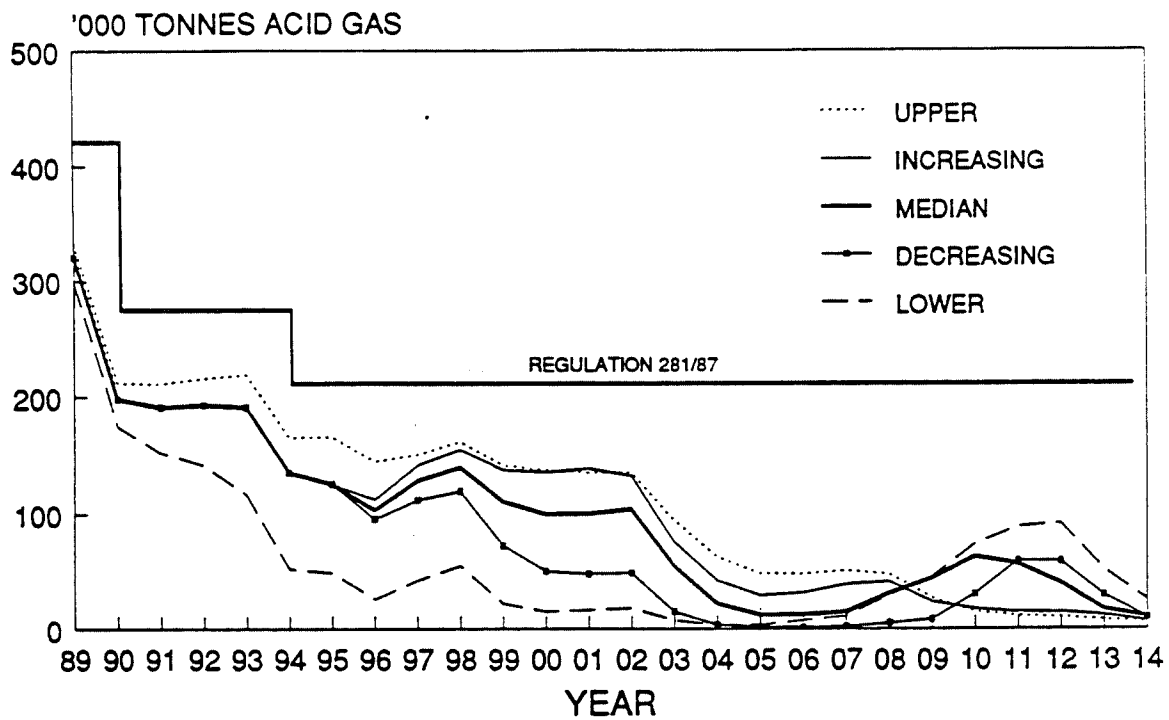
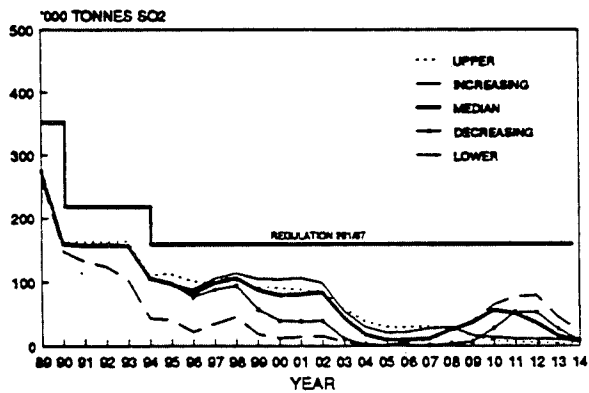


FIGURE 7.6-3
PROJECTED ACID GAS EMISSIONS
[Case 23]



PROJECTED SO₂ EMISSIONS



PROJECTED NO_x EMISSIONS

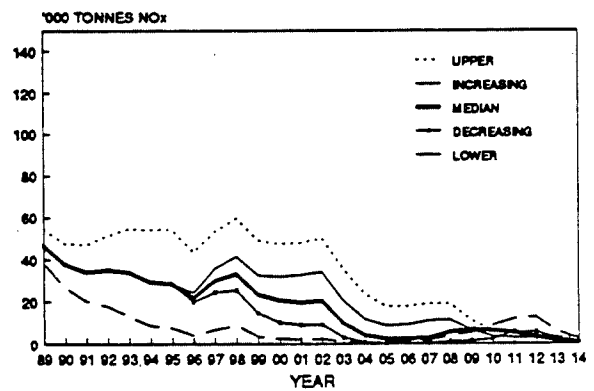


FIGURE 7.6-4
PROJECTED ACID GAS EMISSIONS
[Case 24]

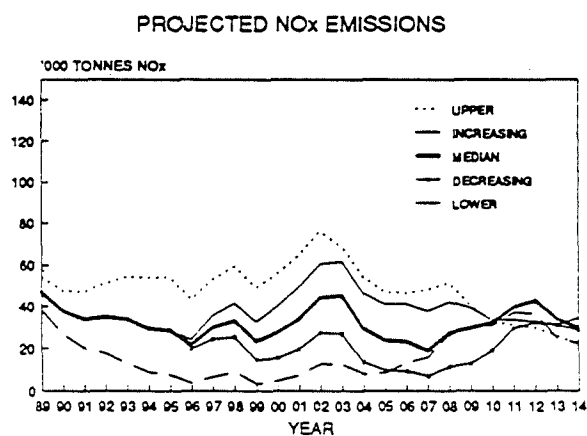
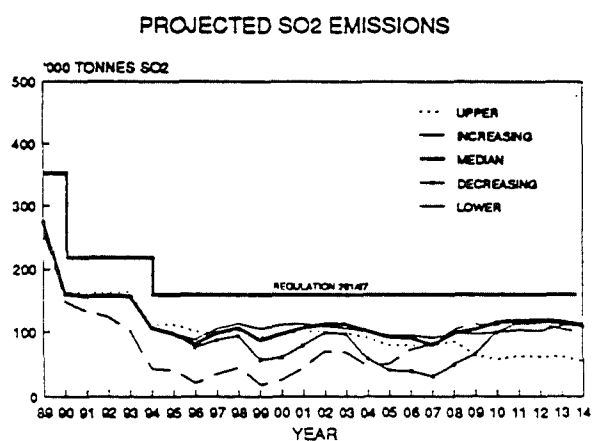
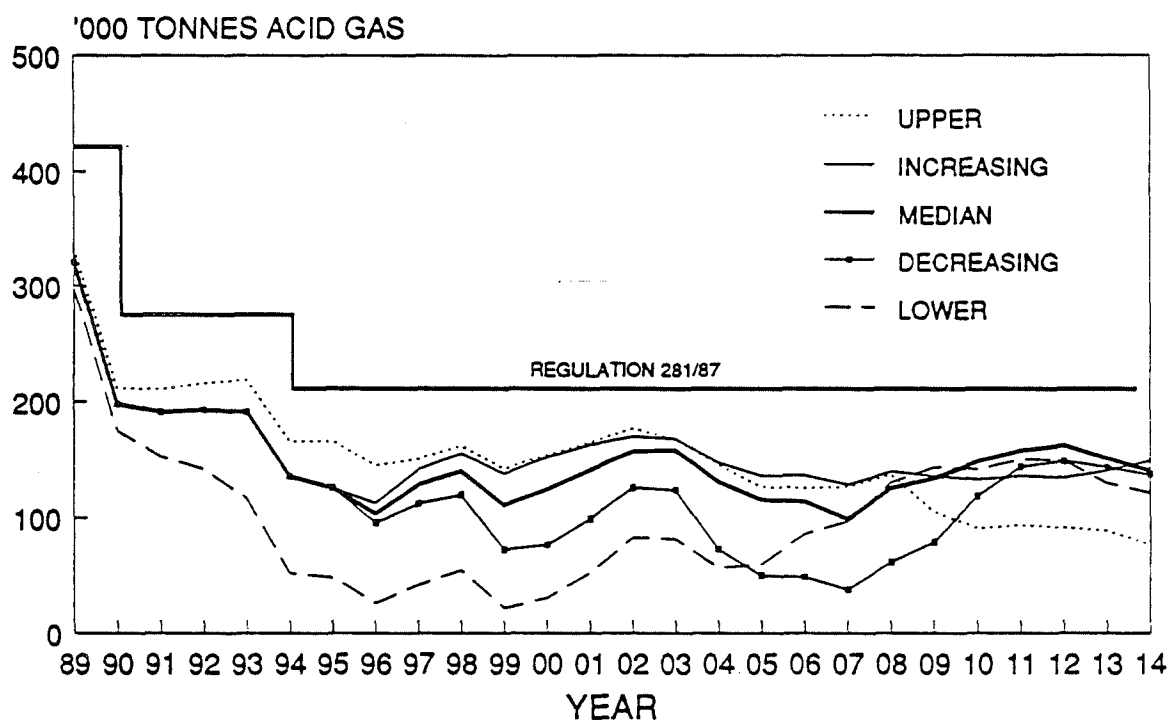
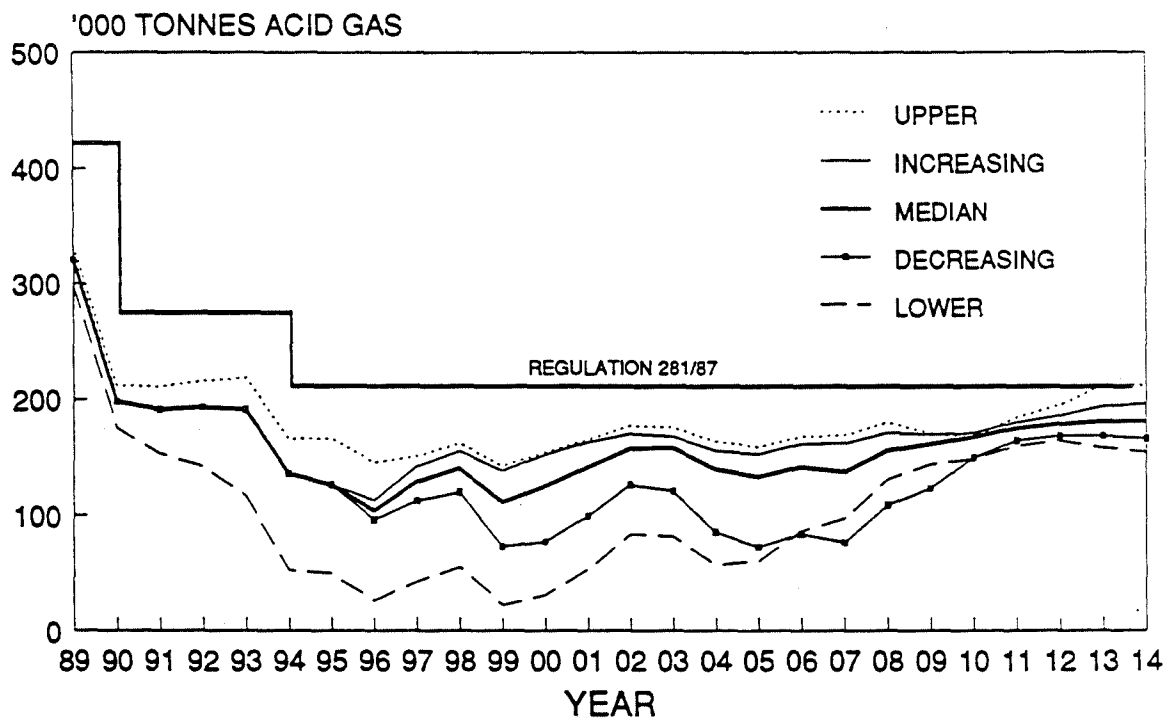
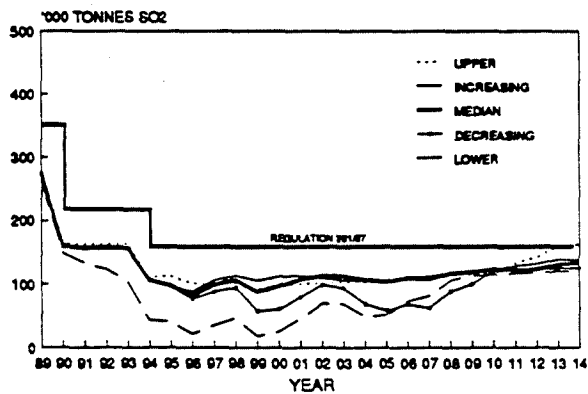


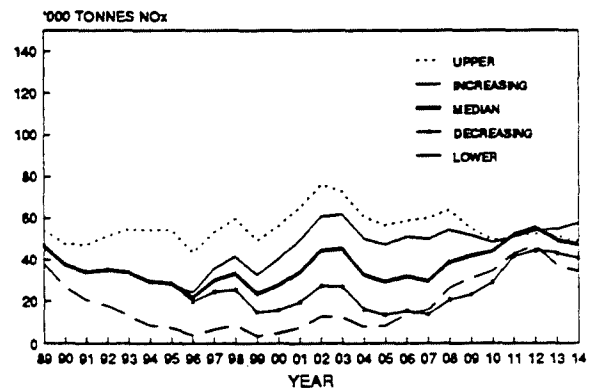
FIGURE 7.6-5
PROJECTED ACID GAS EMISSIONS
[Case 26]



PROJECTED SO₂ EMISSIONS



PROJECTED NO_x EMISSIONS



The upper case requires greatly accelerated installation schedules for scrubbers and CPM at Lambton TGS and Nanticoke TGS. This would require an enormous effort by both Ontario Hydro and equipment manufacturers.

The Control Plan for the branch upper and branch lower cases is identical to the median case prior to the year 1999. This corresponds to the recognition date for the change in load forecast. This results in more acid gas control measures than is required in the branch lower load forecast case. The measures, however, are sufficient for the median and branch upper load forecast cases.

In the longer term, post 2000, acid gas emissions remain below regulated limits, through the retirement of existing fossil generation and the addition of new "cleaner" generation. This is true for all cases except Case 26. In this case, all new generation is fossil based. As a result, acid gas emissions tend to increase from the year 2005 onward. In the upper load forecast case, emissions are at the limit by the year 2014. If the 9 TW.h margin was included in the estimates, the emission limits would likely be exceeded if extraordinary measures were not undertaken. These measures could include the use of low sulphur coal in scrubbed fossil units and/or the increased use of natural gas.

7.7 ANALYSIS DATA

Station Emission Characteristics:

The acid gas emissions for the various plans were calculated utilizing generic emission factors for each of the fossil stations. These factors, in grams per kiloWatt-hour, are given in Figure 7.7-1. Blending of high and low sulphur coals is assumed in unscrubbed units, where advantageous.

FIGURE 7.7-1

Acid Gas Emission Factors

<u>Fuel/Generation Type</u>	<u>Emission Rates (g/kW.h)</u>	
	SO ₂	NO _x
High Sulphur Coal	16.70	1.70
Low Sulphur Coal	5.30	1.70
Western Canadian Coal	2.30	1.70
Natural Gas	0.00	1.80
Unscrubbed Coal	5.30	1.70
Unscrubbed Coal with CPM	5.30	1.36
Scrubbed Coal	1.64	1.40
Scrubbed Coal with CPM	1.64	1.12
New Pulverized Coal Station	1.64	0.25
Lignite	4.30	1.30
CTU-Natural Gas	0.00	1.20
CTU-Oil	0.00	1.90
Combined-Cycle - Natural Gas	0.00	0.80
IGCC	0.47	0.25
Natural Gas	0.00	1.20
Residual Oil	2.80	1.30

7.8 REVIEW

The emission of acid gases from Ontario Hydro's fossil-fired generating stations is constrained by regulated limits imposed by the Ontario government under the Environmental Protection Act. In order to ensure that the electricity demand in Ontario can be satisfied while remaining within the enacted regulations, Ontario Hydro must implement acid gas control measures where and when required.

In managing acid gas emissions to protect the environment, Ontario Hydro's acid gas control policy is to: meet or better government regulated limits; aim for stepped reductions in each year to 1994; and achieve reductions in a cost effective manner. The actions selected to meet emission regulations follow an underlying acid gas control strategy consistent with this policy. The three elements of the strategy are: select cost effective measures on the basis of marginal cost to the system; maintain adequate flexibility to respond to deviations from expectations; and keep sufficient options in reserve to meet unforeseen contingencies.

There are several control options capable of reducing acid gas emissions. Demand Management, non-utility generation, hydraulic and nuclear generation, electricity imports, reducing planned sales, and transmission improvements can reduce acid gas emissions by displacing fossil-fired generation. Acid gas emissions can be reduced by burning lower sulphur coals, natural gas, or lower sulphur oil. As well, the retrofit of emission control equipment to existing stations will reduce these emissions.

Emission control equipment includes high efficiency scrubbers and injection technology for SO₂ control and combustion process modifications, injection technologies and Selective Catalytic Reduction for NO_x control.

Representative Acid Gas Control Plans were developed which combine a variety of control measures into separate control programs for each of the five load forecasts analyzed. While each program is capable of meeting current emission regulations, the measures may be reduced or supplemented as required in the future.

In all of the programs acid gas control is accomplished through two primary measures - the retrofit of control equipment to existing fossil stations, and the use of lower sulphur fuel (eg. low sulphur coal). Retrofits of control equipment to existing stations are designated major control measures as they involve capital modification to the station and require scheduling of design, construction and installation. The schedule for these measures extends to the year 2005. Beyond that date, no additional measures are planned on existing stations.

Acid gas emissions are calculated to remain below the regulated limits in all cases. The amount by which the expected emissions are below the regulation represents the planning margin. Typically this corresponds to 9 TWh of additional fossil generation. This is true for all cases except Case 26. In this case, all new generation is fossil based. As a result, acid gas emissions tend to increase from the year 2005 onward. In the upper load forecast case, emissions are at the limit by the year 2014.

Over most years in the plan, additional flexibility is provided by a number of potential measures. Coal sulphur levels can be further reduced by utilizing very low sulphur coals. Prior to retirement, R.L. Hearn TGS can be demothballed and operated on natural gas or another existing fossil station could be converted to operate on natural gas. These high cost measures remain in reserve to meet contingencies and load forecasts over and above those planned for.

8. COSTS

8.0 INTRODUCTION

8.1 COST RESULTS

8.2 BUILDING THE RISK ASSESSMENT MODEL

8.3 DETERMINISTIC COSTS

8.4 SENSITIVITY ANALYSIS

8.5 PROBABILISTIC ANALYSIS

8.6 REVIEW

8.0 INTRODUCTION

This chapter supplements the cost information presented in Chapter 15 of the DSP Report. It explains how costs are calculated for the Demand/Supply Plans and provides more information on:

- the model used to compute plan costs
- the allocation of capital and fixed costs
- the derivation of costs of the existing system and future systems
- the sensitivity analysis of costs
- the probability analysis for calculating expected costs
- the cumulative probability distributions of plan costs and differences relative to one another

8.1 COST RESULTS

This chapter also provides more details on the cost results.

For each of the five demand/supply plans described earlier in Chapter 4, costs are presented for all five load forecast paths considered in the plan formulation -- median, branch upper, upper, branch lower and lower.

Details of the sensitivity analyses that identify the significant variables to use in the probability analysis are described.

Results from the probability analysis are also shown. Cost bands are described for cases where each cost estimate, such as the discount rate, is fixed at its low, median and upper value, while all other estimates are allowed to vary. This provides additional information on the sensitivity of plan costs to certain conditions.

The next section, 8.2, describes the model used to analyze costs, its data sources, the model's capabilities and the allocation of present value costs.

The third section describes several applications of the model. In particular, there is an explanation of the calculations of the values in Figure 15-46, Cost of Ontario

Hydro New Major Supply, and Figure 15-47, Total Cost of New Demand/Supply Options and Operating the Existing System, both of the DSP Report.

The fourth section describes the sensitivity studies done to identify which cost estimates have the most significant influence in the evaluation of plan costs.

The last section contains the details on the probability analyses.

8.2 BUILDING THE RISK ASSESSMENT MODEL

Figure 8.2-1 presents an overview of the flow of data in and out of the Risk Assessment Model (RAM). This was used as the cost evaluation tool.

For each demand/supply case and under each load forecast path, there is a unique application of RAM. This model integrates the life cycle cost data for the options and economic values (escalation and discount rates) and carries out deterministic and probabilistic analyses for the present value cost evaluation. Central to this evaluation is the allocation of costs to the planning period, 1989 to 2014.

The following paragraphs describe the main elements and data sources of the process. As well, a description of cost allocation in RAM is provided. Specific model applications and analyses are described in Sections 8.3, 8.4 and 8.5.

8.2.1 Demand/Supply Plans

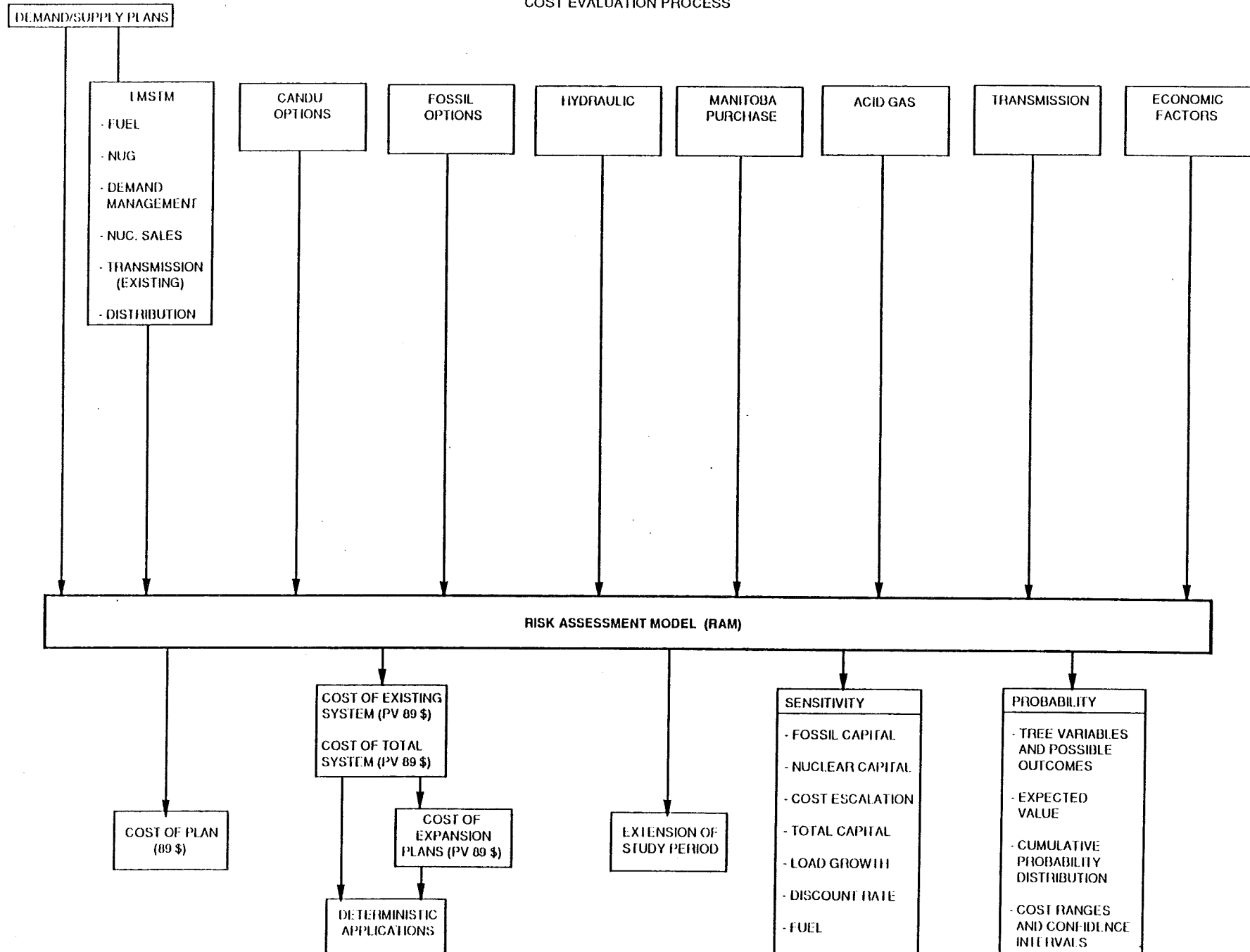
Chapter 4 defines the demand/supply cases with their specific options and in-service dates for supply options. This information is fundamental for building a cost model.

8.2.2 LMSTM

The production simulation model used in the development of the Plan is referred to as LMSTM. Details of this model are discussed in Chapter 2.

LMSTM provided costs of variable OM&A for nuclear, fossil and acid gas controls, hydraulic OM&A, fuel and fuel related costs and water rentals. In addition, LMSTM output is used for other capital and other operating costs, such as demand management, non-utility generation, existing and incremental growth related transmission costs, and total distribution costs.

FIGURE 8.2-1
COST EVALUATION PROCESS



8.2.3 CANDU Option Costs

CANDU nuclear cost data are based on the Ontario Hydro Presentations to the Ontario Nuclear Cost Inquiry (ONCI). These costs were reviewed by an independent panel, appointed by the Ontario government. The Panel concluded that the cost estimates are complete and are appropriate for use in planning.

The life cycle costs include: capital costs for design, approval, construction, commissioning, retubing (i.e. fuel channel replacement), capital modifications during the operating life, decommissioning and associated overheads; operating, maintenance and administration (OM&A) costs for ongoing training, labour, material, purchased services, interest on inventories, overheads and the heavy water costs associated with tritium removal, upgrading and makeup; and fuel costs for acquisition and fuel waste management, including disposal. Life cycle costs include those costs attributable to the option after its assumed station life (40 years).

8.2.4 Fossil Option Costs

The costs of fossil options are based on the Thermal Cost Review. These costs were requested by Hydro's Board of Directors and underwent an independent expert review by consultants.

Life cycle cost categories for capital, OM&A and fuel costs are similar to those for the nuclear option. Also included are capital, OM&A and fuel related costs for acid gas controls, where appropriate.

8.2.5 Hydraulic Costs

Hydraulic costs are drawn from Ontario Hydro's estimates associated with each proposed development.

The cost of the Hydraulic Plan, as described in Chapter 12 of the DSP Report, is common to all demand/supply plans. Life cycle costs for the proposed projects within the Hydraulic Plan are captured in the LMSTM and RAM models. These costs include capital, OM&A and water rental charges over the assumed station service lives (90 years).

8.2.6 Manitoba Purchase

The cost of the Manitoba Purchase is common to all demand/supply plans. The costs included in the plans are for capacity, energy and energy credits associated with the transmission capability. The cost of capacity and energy are derived from the Manitoba-Ontario Power Transaction Agreement of December 7, 1989, and the

Electricity Sale Agreement of August 28, 1987. The energy credits are cost savings derived from the capability of the transmission lines to incorporate additional short term economy electricity sales.

8.2.7 Acid Gas Controls For The Existing System

Acid gas control costs are derived from Ontario Hydro's estimates.

Life cycle costs include capital costs such as design, approvals, construction, commissioning, operator training, capital modification and rehabilitation during the station's operating life, and OM&A costs associated with operating the control equipment.

8.2.8 Transmission

Capital costs for new transmission are taken from studies described in Chapter 5. Other capital and all transmission OM&A are taken from LMSTM.

8.2.9 Economic Factors

Discount rates, escalation rates and their bands (i.e. low, median and upper estimates) are input to RAM. Ontario Hydro's Economic Outlook of September 1988 is the basis for the Corporate Financial Discount Rate (CFDR), the various escalation rates, Consumer Price Index (CPI) and provincial Gross Domestic Product (GDP) used in RAM.

8.2.10 Basic Functions of RAM

RAM was built to perform the risk assessment and calculate the costs for every individual case. More specifically, the Risk Assessment Model performs the following basic functions:

- integrate all cost data involved in the financial evaluation of the cases
- integrate all economic parameters required for financial evaluations
- provide the present value cost for each case and load forecast path (both total cost and by major cost groups), and
- perform financial sensitivity analyses and probabilistic simulations.

8.2.11 Allocation of Costs

One important feature performed by RAM is computing present value costs allocated to the planning period.

Present value costs are used in order to compare plans that have different patterns

of expenditures for capital, OM&A, and fuel costs. Chapter 6 of the DSP Report dicusses this and other cost concepts.

The method used to allocate the present value of fixed costs recognizes that some options will have a life that ends after the planning period (1989-2014). Examples of these fixed costs are the acquisition costs of design, approval, construction, commissioning and capital modification.

The present value of fixed costs is allocated on the basis of unit-years. A unit-year is one unit operating for one year. Unit-years are used to calculate an allocation factor, which is applied to the present value of total fixed costs.

What follows is an example of the process for allocating acquisition costs attributable to a 4x881 MW CANDU station, in which units are placed in service on an annual basis beginning in January of 2004. The same process applies to the allocation of post in-service fixed costs such as capital modifications, and total fixed OM&A.

Figure 8.2-2 illustrates the calculation of the present value cost to be allocated to the planning period. The second column lists the acquisition costs, which are in 1988 dollars as expressed in ONCI. The third column lists the present value of these costs. These are calculated using specific escalation rates associated with nuclear projects and Hydro's Corporate Financial Discount Rate (CFDR). The total present value of acquisition costs in 1989 dollars is 3,550.4 M\$.

A portion of this present value total for acquisition of a CANDU generating station is allocated to the planning period. The allocation is based on the ratio of the present value of unit-years within the planning period to the present value of unit-years for the entire station life. Calculating the present value of unit-years is necessary to equate the present value of life cycle expenditures to the present value of costs allocated over the station life.

The fourth column lists the unit-years for the entire life of the station. The total is 153 unit-years, which includes the effects of retubing. The fifth column is a listing of the present value factors for each year that are to be applied to the unit-years. These factors are derived using GDP as the escalation rates and CFDR as the discount rate. The procedure is similar to that used to determine the present value of a cash flow.

The sixth column is the cumulative present value total of unit-years. For example, by the end of 2006, the cumulative present value of unit-years is 1×0.466 plus 2×0.444 plus 3×0.422 , which equals 2.62.

FIGURE 8.2 - 2

EXAMPLE OF ALLOCATING THE PRESENT VALUE ACQUISITION COSTS
OF A 4 * 881 MW CANDU GENERATING STATION

YEAR	ACQUISITION COST 1988\$M	PRESENT VALUE OF ACQUISITION COSTS '89 PV \$M	UNIT YEARS	UNIT YEAR PV FACTOR (REAL/GDP)	CUMULATIVE PV OF UNIT YEARS
1989	1.04	1.06		1.023	0.00
1990	3.39	3.30		0.968	0.00
1991	10.35	9.63		0.917	0.00
1992	37.75	33.46		0.871	0.00
1993	50.59	42.67		0.826	0.00
1994	49.59	39.91		0.781	0.00
1995	51.05	39.19		0.739	0.00
1996	131.85	96.88		0.700	0.00
1997	262.81	185.60		0.665	0.00
1998	472.06	320.03		0.631	0.00
1999	710.30	461.77		0.599	0.00
2000	948.57	591.33		0.567	0.00
2001	1053.10	630.41		0.539	0.00
2002	939.28	540.70		0.514	0.00
2003	615.47	340.70		0.489	0.00
2004	291.97	155.42	1	0.466	0.47
2005	87.21	44.64	2	0.444	1.35
2006	27.08	13.34	3	0.422	2.62
2007	0.76	0.36	4	0.402	4.23
2008		0.00	4	0.383	5.76
2009		0.00	4	0.365	7.22
2010		0.00	4	0.347	8.61
2011		0.00	4	0.331	9.93
2012		0.00	4	0.316	11.19
2013		0.00	4	0.302	12.40
2014		0.00	4	0.288	13.55
2015		0.00	4	0.275	14.65
2016		0.00	4	0.263	15.71
2017		0.00	4	0.252	16.71
2018		0.00	4	0.241	17.68
2019		0.00	4	0.230	18.60
2020		0.00	4	0.221	19.48
2021		0.00	4	0.211	20.33
2022		0.00	4	0.202	21.13
2023		0.00	4	0.193	21.91
2024		0.00	4	0.185	22.64
2025		0.00	4	0.177	23.35
2026		0.00	4	0.169	24.03
2027			4	0.162	24.67
2028			4	0.155	25.29
2029			4	0.148	25.89
2030			4	0.142	26.45
2031			3	0.136	26.86
2032			3	0.130	27.25
2033			3	0.124	27.62
2034			3	0.119	27.98
2035			3	0.114	28.32
2036			3	0.109	28.64
2037			4	0.104	29.06
2038			4	0.099	29.46
2039			4	0.095	29.84
2040			4	0.091	30.20
2041			4	0.087	30.55
2042			4	0.083	30.88
2043			4	0.080	31.20
2044			4	0.076	31.51
2045			1	0.073	31.58
2046				0.070	31.58
2047				0.067	31.58
2048				0.064	31.58
2049				0.061	31.58
2050				0.058	31.58
TOTAL	5744.20	3550.40	153.50		

TOTAL 1989 PV - 3550.4 MS
PV OF UNIT YEARS TO 2014 - 13.55
PV OF UNIT YEARS FOR STATION LIFE - 31.58
PV FACTOR FOR ALLOCATION - 43%
PV ALLOCATED ACQUISITION COST - 1523.7 MS

The cumulative present value of unit-years to the end of the planning period, 2014, is 13.55; to the end of the station life, it is 31.58. The ratio of these values, 0.429, is multiplied by the present value total of acquisition costs, resulting in an allocated present value cost of 1,523.7 M\$ in 1989 dollars.

For this station, 43% of the total present value cost is allocated. This equals in \$1.523 billion.

If the planning period were longer, additional fixed costs would be allocated to the period. For example, if the planning period included years up to 2045, then all of the acquisition costs for the station would be allocated.

The key result of this allocation process is that it takes into account the life cycle costs of the options. It provides a basis to compare cases that have options with different in-service dates and different service lives. Compared to a simple prorating approach, this process allocates more costs to the early years of the station's life.

The same allocation method was used for the fixed costs of all new fossil options, acid gas measures and transmission projects. The allocation of the hydraulic capital program and the Manitoba Purchase, which are common to all plans, was also calculated in a similar fashion.

To complete the calculation of a plan's present value cost, the present value of other annual costs, such as variable OM&A, and fuel and fuel related costs, are added to the allocated fixed costs.

8.3 DETERMINISTIC COSTS

As illustrated earlier in Figure 8.2-1, deterministic cost evaluations are one of several applications of the risk assessment models.

The deterministic applications described here include the main costs of the proposed DSP in 1989 dollars and two figures from the DSP Report: Figure 15-46, Cost of Ontario Hydro New Major Supply, and Figure 15-47, Total Cost of New Demand/Supply Options and Operating the Existing System. As well, to complement the illustration provided for median load in the latter set, similar figures are shown for the other four load forecasts.

8.3.1 Cost of Proposed Plan in 1989 Dollars

The magnitude of costs for main components of the Proposed Plan is presented in Figure 8.3-1 in January 1989 dollars.

The elements of the costs shown in Figure 8.3-1 are:

- Nuclear costs correspond to the capital costs of new plants;
- Fossil cost consists of the capital costs of all new options and acid gas control retrofits on existing plants;
- Purchase NUGs cover cost of purchase from planned non-utility generators;
- Demand Management and Load Displacement NUG are expenses for Ontario Hydro and participants on current and future programs;
- Manitoba Purchase comprises both the new 1,000 MW deal and the previous agreement of 200 MW;
- Hydraulic corresponds to capital costs incurred for new projects;
- Transmission cost apply to new site-specific projects (radial and inter-area); and
- Fuel consists of a portion of the total fuel bill that can be attributed to load growth beyond year 1993.

Figure 8.3-1
Proposed Demand/Supply Plan Period 1989 to 2014

<u>Component</u>	<u>1989 Billion Dollars*</u>
Nuclear	19.1
Fossil	3.2
Purchase NUGs	6.2
Demand Management and Load Displacement NUG	10.3
Manitoba Purchase	3.8
Hydraulic	4.8
Transmission	2.7
Fuel for Growth beyond 1993	10.4
Total	60.5

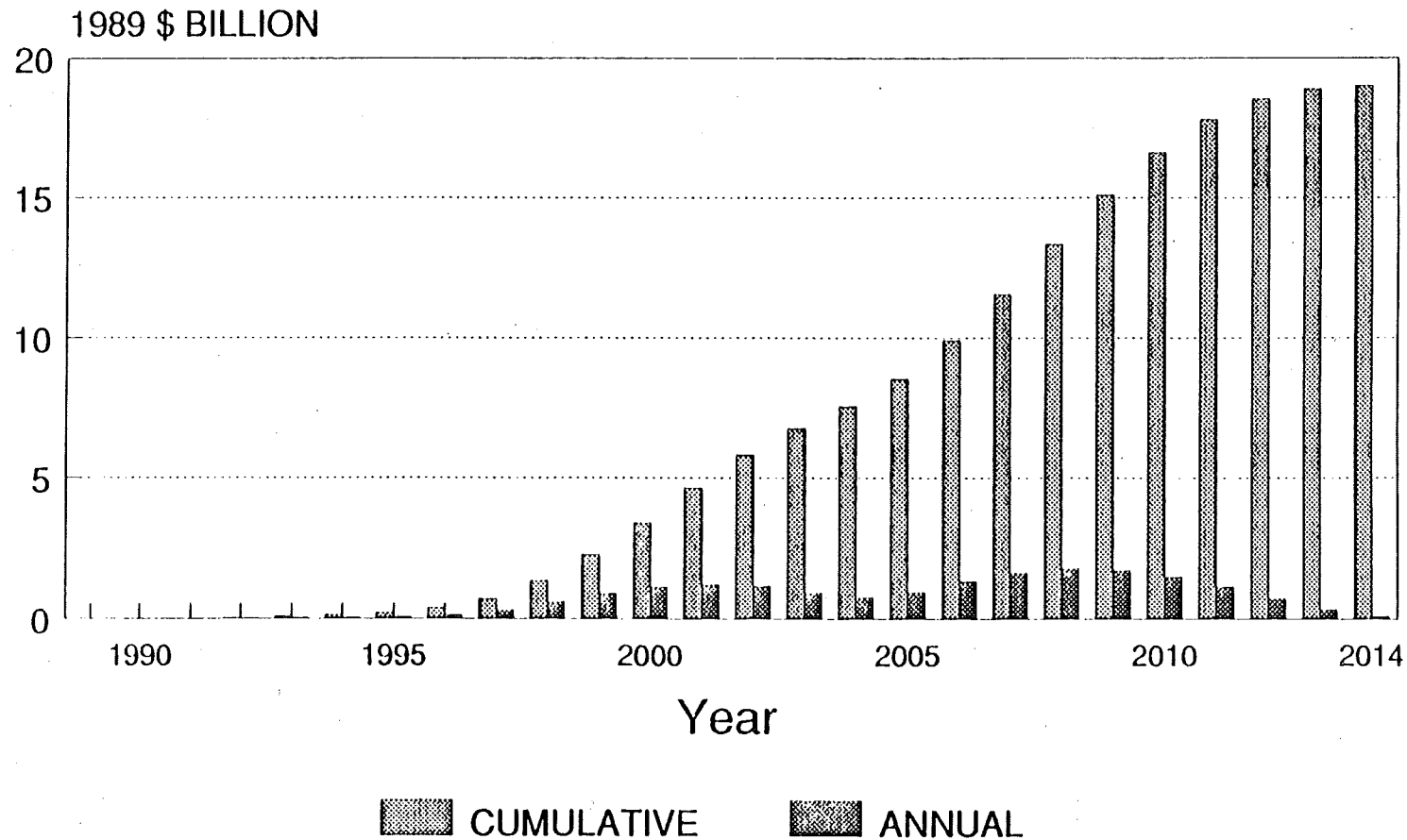
*Note: Totals were rounded.

Figures 8.3-2 through 8.3-10 show both the cumulative and annual expenses of the above components according to their planned cash flow schedules. In some instances, annual costs end before year 2014; in others, cash flows continue beyond 2014, the end of the study period.

If interest and cost escalation were subsequently added, the costs discussed in this section would be higher.

FIGURE 8.3-2

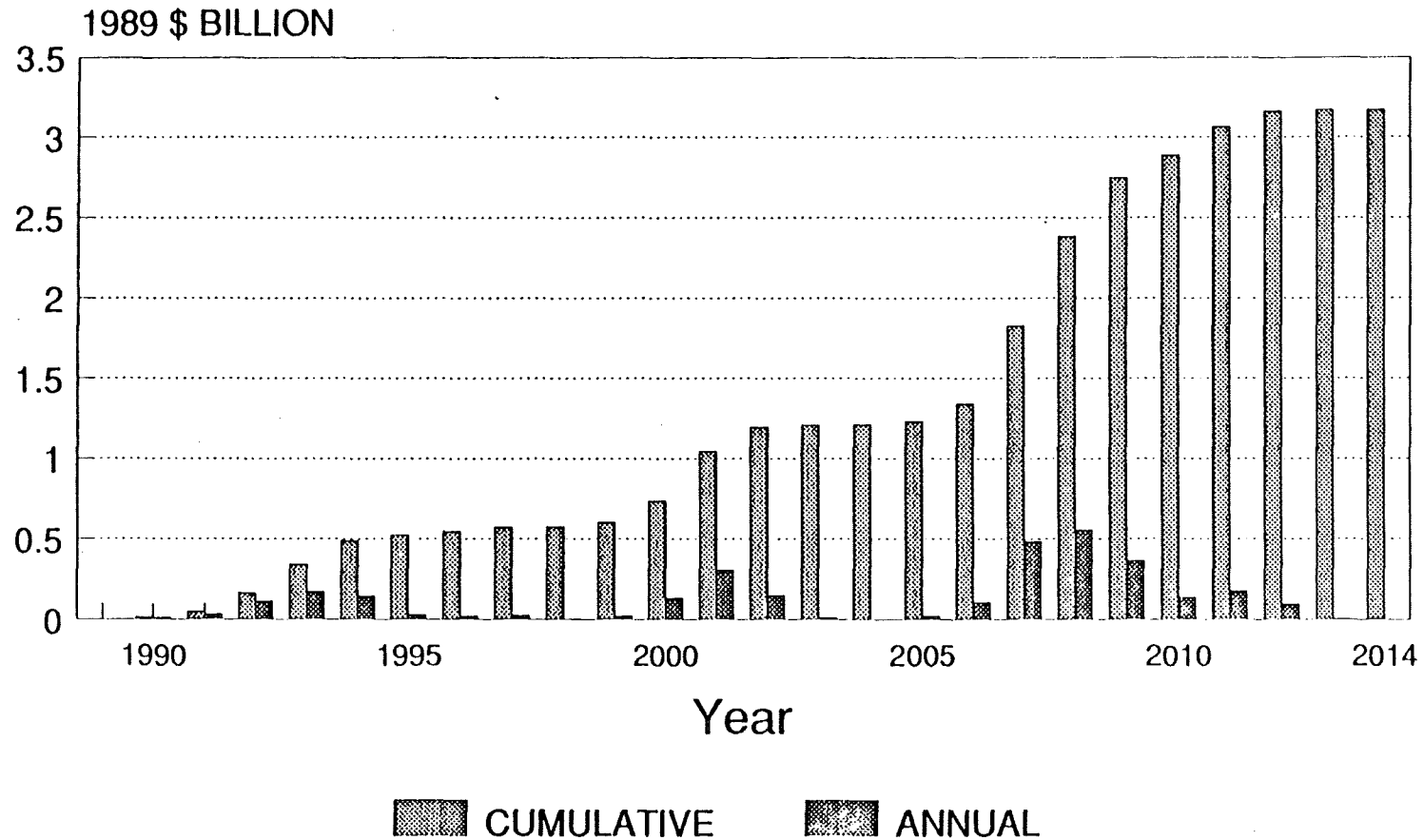
CASE 15 - MEDIAN LOAD NEW NUCLEAR CAPITAL



CASH FLOW FROM 1989 TO 2014

FIGURE 8.3-3

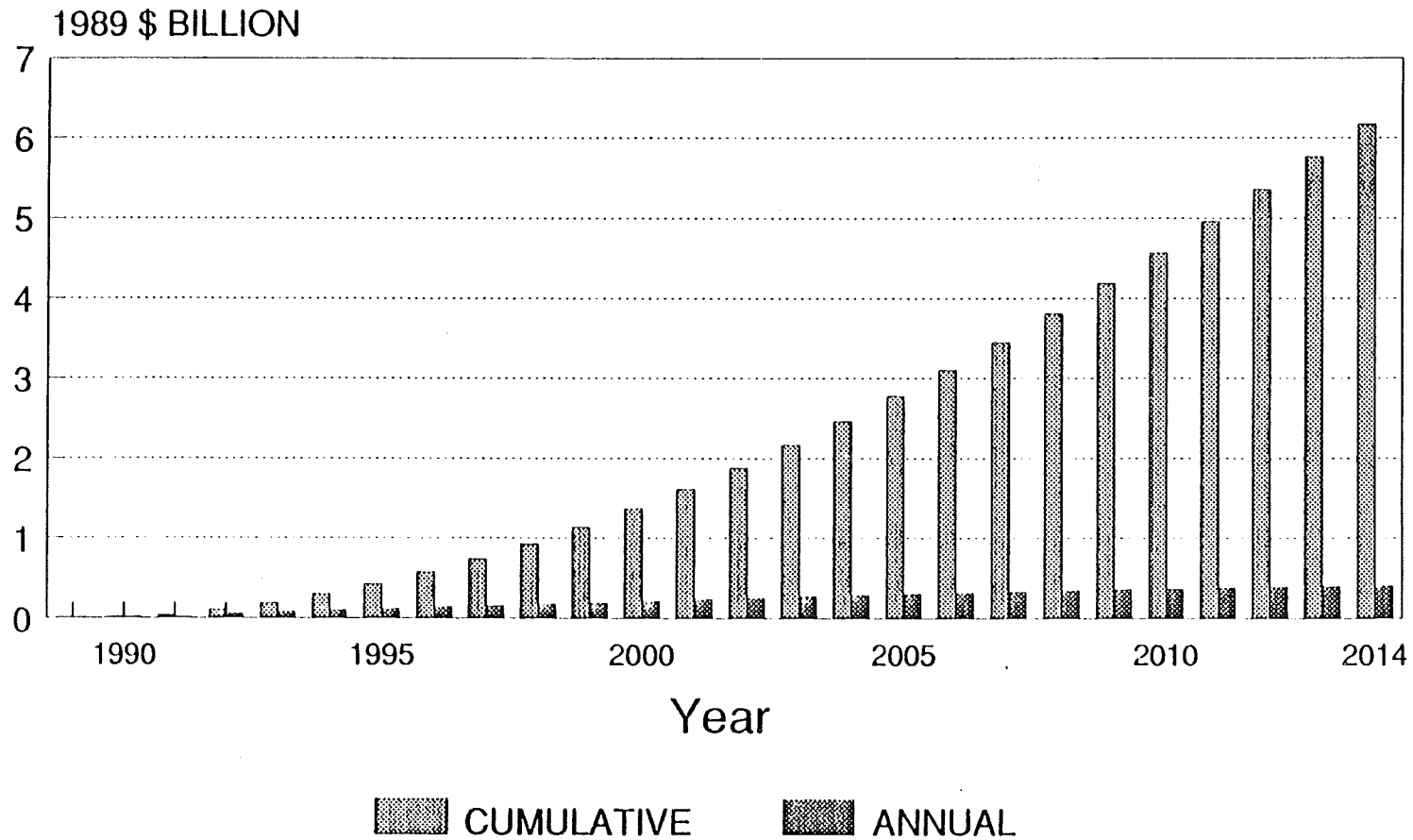
CASE 15 - MEDIAN LOAD NEW FOSSIL CAPITAL



CASH FLOW FROM 1989 TO 2014

FIGURE 8.3-4

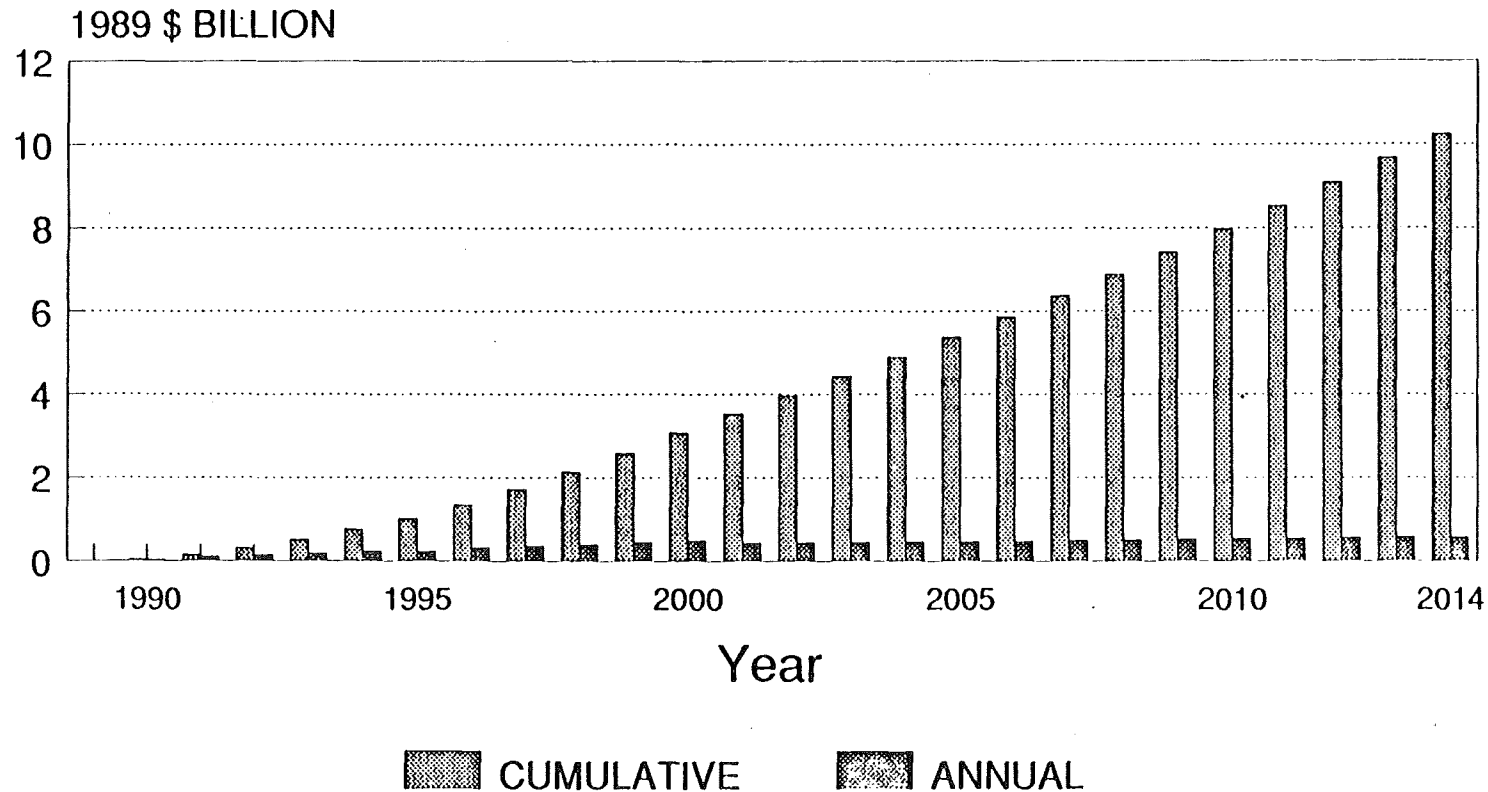
CASE 15 - MEDIAN LOAD NON-UTILITY GENERATION



CASH FLOW FROM 1989 TO 2014

FIGURE 8.3-5

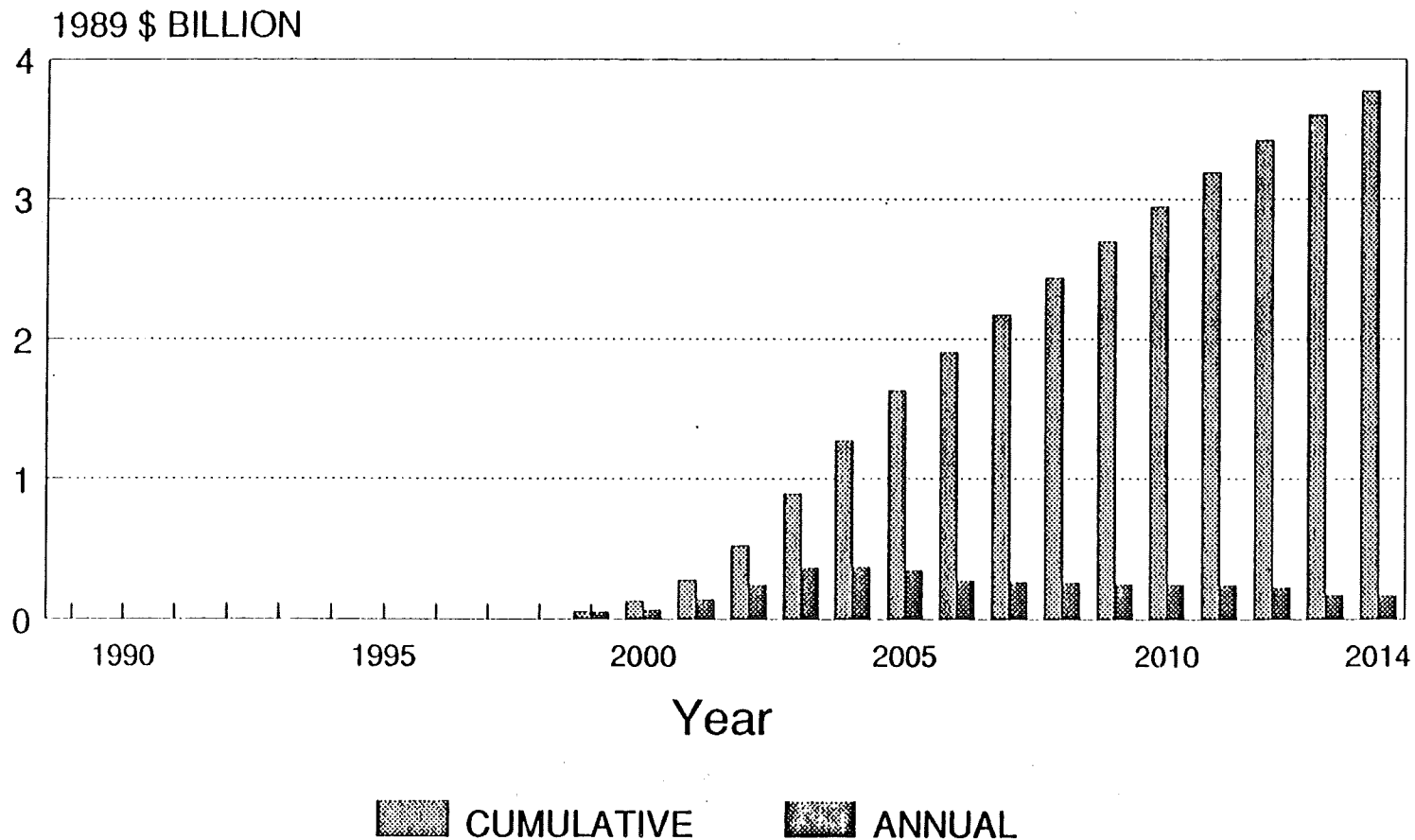
CASE 15 - MEDIAN LOAD DEMAND MANAGEMENT AND LOAD DISPLACEMENT NUG



CASH FLOW FROM 1989 TO 2014

FIGURE 8.3-6

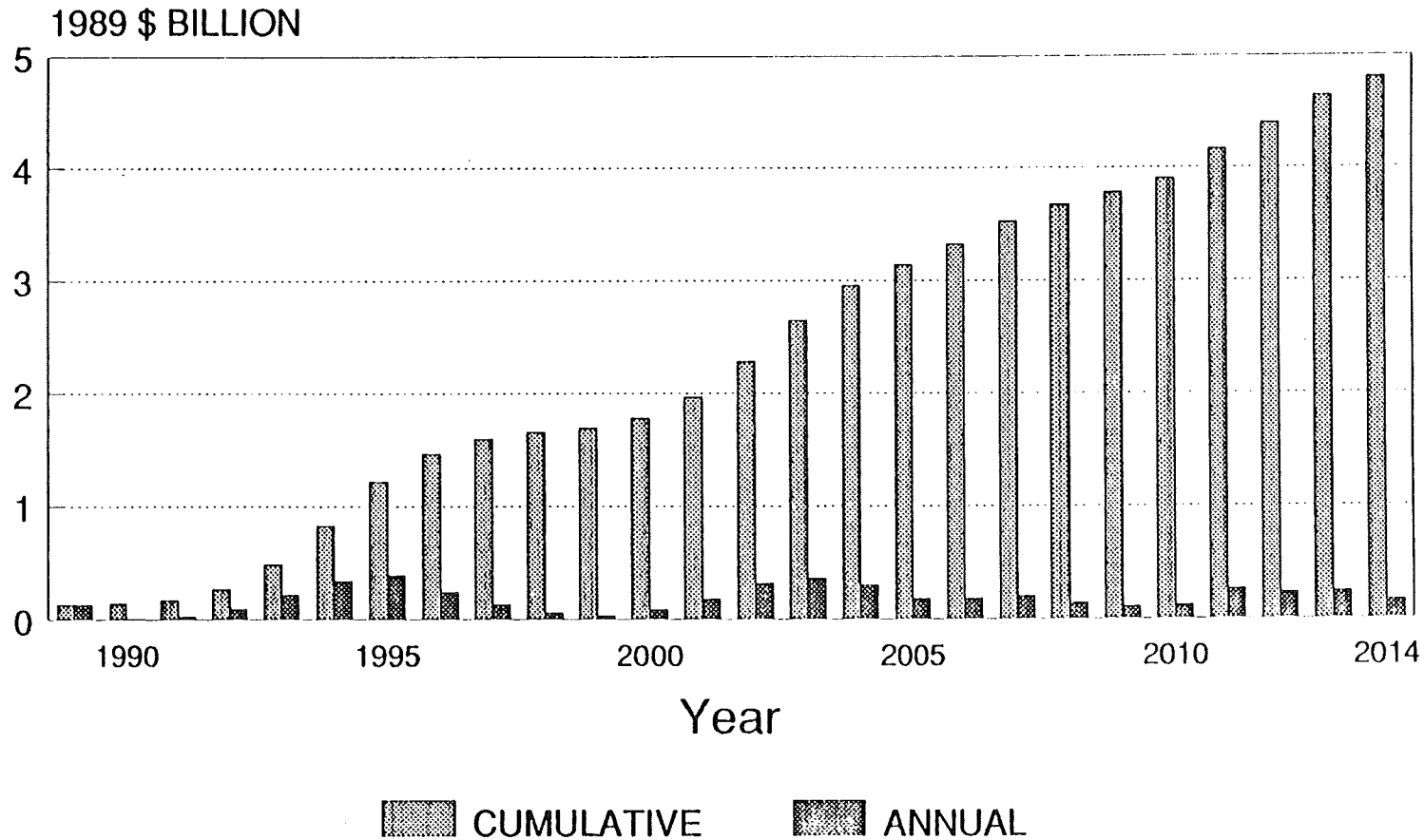
CASE 15 - MEDIAN LOAD MANITOBA PURCHASE



CASH FLOW FROM 1989 TO 2014

FIGURE 8.3-7

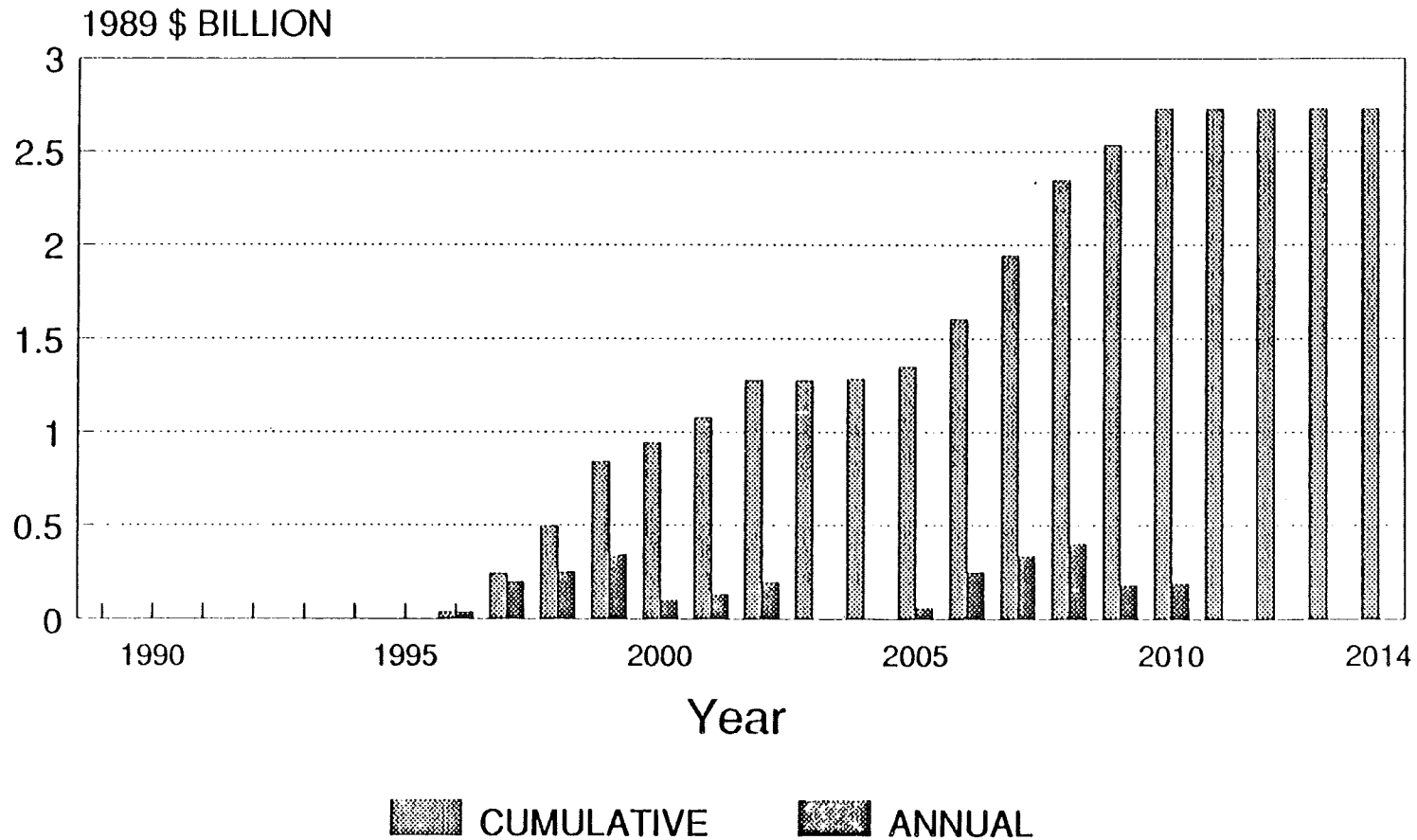
CASE 15 - MEDIAN LOAD NEW HYDRAULIC CAPITAL



CASH FLOW FROM 1989 TO 2014

FIGURE 8.3-8

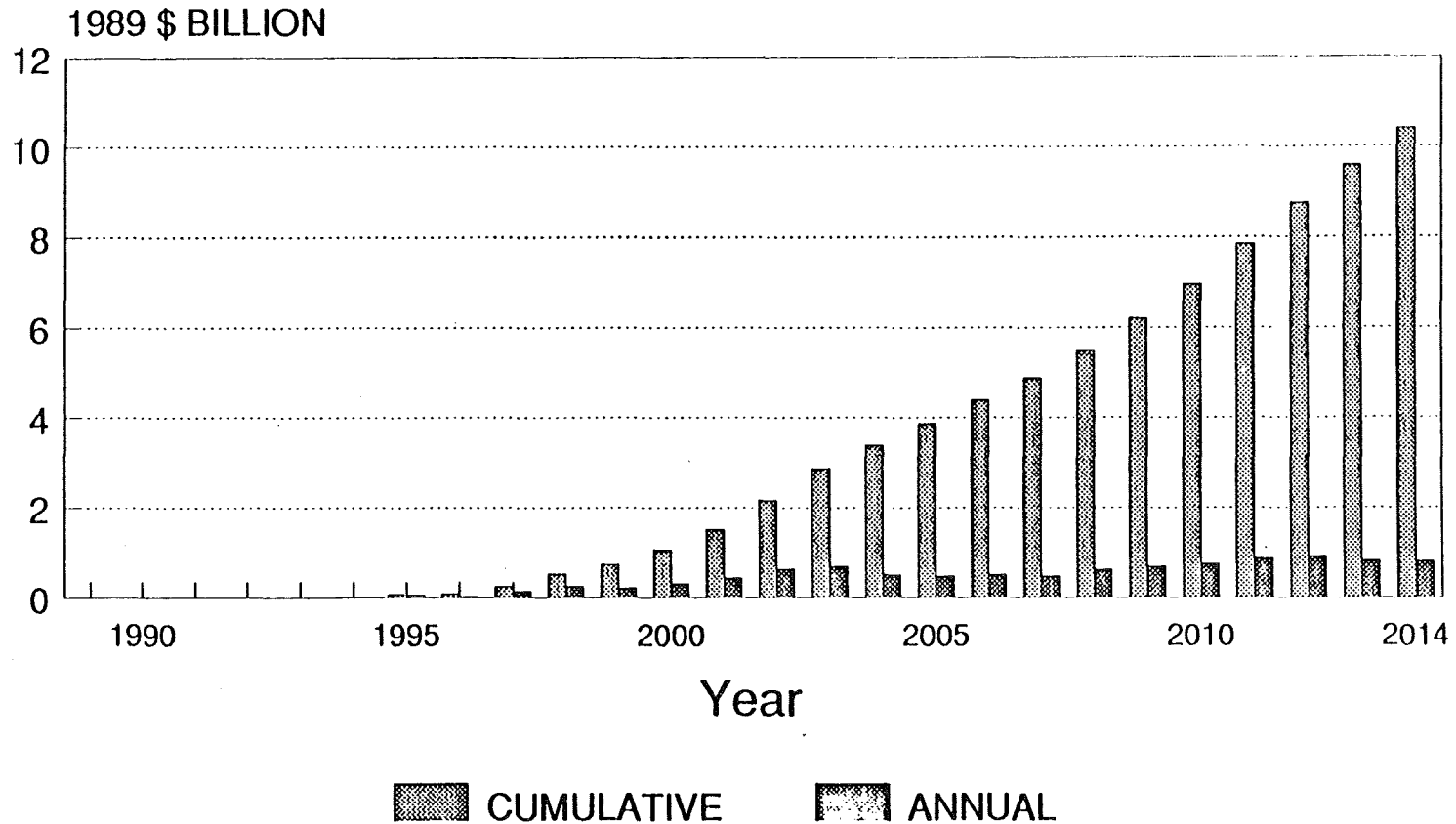
CASE 15 - MEDIAN LOAD NEW SITE-SPECIFIC TRANSMISSION



CASH FLOW FROM 1989 TO 2014

FIGURE 8.3-9

CASE 15 - MEDIAN LOAD FUEL

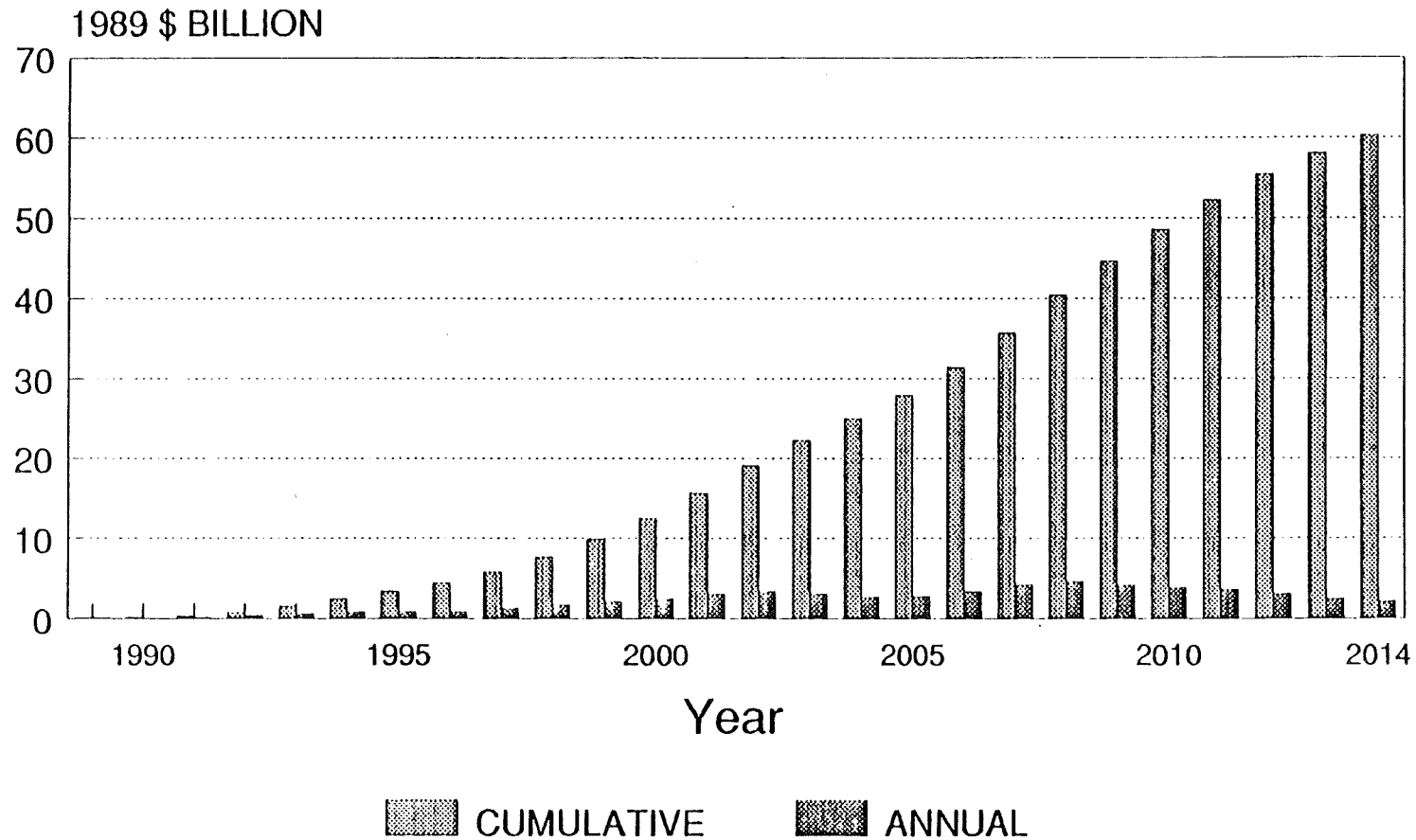


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CASH FLOW DUE TO LOAD GROWTH
BEYOND YEAR 1993

FIGURE 8.3-10

CASE 15 - MEDIAN LOAD MAIN COST COMPONENTS



CASH FLOW FROM 1989 TO 2014

8.3.2 Cost of Existing and New Systems

Much of the total cost of one plan is common to all plans. These common elements include the Demand Management Plan, the Non-Utility Generation Plan, the Hydraulic Plan, and the Manitoba Purchase Plan. Also, common to all plans is much of the cost of operating and maintaining the existing system.

Much of the analysis of costs focuses on the difference in cost between plans. It is also useful to understand what decisions on options are driving the cost differences. This requires a division in costs by major groups and removal of common costs.

Separating the costs of the common elements is straight forward.

Separating the common costs of utilizing the existing system is more difficult because the operation of the system is dependent on what options are included in the major supply cases.

To define a common cost for the existing system Hydro used costs associated with the system when its load meeting capability closely matches the forecast customer demand. For all load forecast paths, except the lower forecast, this happens about the year 1993. For the lower load forecast, this happens about the year 2000.

Variable operating costs of the existing system in the year 1993 are extended to 2014. Annual fixed costs associated with the existing system are left unchanged. Common cost of the existing system then, is all of the costs up to 1993, and the accumulation of variable costs to 2014. For the lower load forecast path, a similar approach is applied, using 2000, the year in which load meeting capability matches demand, as the base year for extending variable operating costs.

The difference between total system costs and existing system costs represents the costs of new major supply cases. The differences in plan costs preserve the impact major supply cases have on the existing system.

Figure 8.3-11 shows the major cost groups for the existing and new systems for median load forecast. The figure is a compilation of cost information derived from data residing within RAM. The first three columns (A, B and C as indicated at the bottom of the figure) provide the data for the existing system; the remaining columns provide data for the total system costs of the five demand/supply plans evaluated. The total system is the existing system, plus the options added according to each plan.

FIGURE C.3-11

Section I. PRESENT VALUE FOR BASIC GROUP COSTS OF NEW AND EXISTING SYSTEMS (1989 M\$ PV) - MEDIAN LOAD FORECAST

1	Project		EXISTING PV\$M 1989		Project		CASE 23 PV\$M 1989		Project		CASE 22 PV\$M 1989		Project		CASE 15 PV\$M 1989		Project		CASE 24 PV\$M 1989		Project		CASE 26 PV\$M 1989	
2																								
3																								
4	Nuclear	Capital	0		Nuclear	Capital	5165		Nuclear	Capital	3382		Nuclear	Capital	2189		Nuclear	Capital	1639		Nuclear	Capital	0	
5		Fix OMA	7812		New	Fix OMA	2553		New	Fix OMA	1675		New	Fix OMA	1063		New	Fix OMA	810		New	Fix OMA	0	
6		Fuel	5799			Fuel	8713			Fuel	8550			Fuel	8363			Fuel	8299			Fuel	5902	
7																								
8																								
9		Salces	27			Salces	333			Salces	189			Salces	119			Salces	96			Salces	72	
10																								
11		Total	13584			Total	14097			Total	11418			Total	9536			Total	8651			Total	5920	
12																								
13	Fossil	Capital	0		Fossil	Capital	92		Fossil	Capital	208		Fossil	Capital	517		Fossil	Capital	908		Fossil	Capital	1926	
14		Fix OMA	2554		New	Fix OMA	0		New	Fix OMA	25		New	Fix OMA	73		New	Fix OMA	262		New	Fix OMA	847	
15		Fuel	5726			Fuel	4073			Fuel	4976			Fuel	6085			Fuel	6508			Fuel	8301	
16																								
17																								
18																								
19																								
20		Total	8280			Total	4165			Total	5208			Total	6675			Total	7768			Total	11163	
21																								
22	AG Cble	Capital	0		AG Cble	Capital	346		AG Cble	Capital	346		AG Cble	Capital	346		AG Cble	Capital	346		AG Cble	Capital	346	
23		Fix OMA	0			Fix OMA	95			Fix OMA	95			Fix OMA	95			Fix OMA	95			Fix OMA	95	
24		Var OMA [Foss Fuel]				Var OMA [Foss Fuel]				Var OMA [Foss Fuel]				Var OMA [Foss Fuel]				Var OMA [Foss Fuel]			Var OMA [Foss Fuel]			
25		Total	0			Total	441			Total	441			Total	441			Total	441			Total	441	
26																								
27	Hydraulic	Capital	0		Hydraulic	Capital	1189		Hydraulic	Capital	1189		Hydraulic	Capital	1189		Hydraulic	Capital	1189		Hydraulic	Capital	1189	
28		Fix OMA	1238		New	Fix OMA	200		New	Fix OMA	200		New	Fix OMA	200		New	Fix OMA	200		New	Fix OMA	200	
29		Var OMA	1526			Var OMA	1609			Var OMA	1609			Var OMA	1609			Var OMA	1609			Var OMA	1609	
30																								
31		Purch 200	0			Purch 200	148			Purch 200	148			Purch 200	148			Purch 200	148			Purch 200	148	
32																								
33																								
34		Total	2963			Total	3146			Total	3148			Total	3146			Total	3146			Total	3146	
35																								
36	Gen Trans	Capital	352		Gen Trans	Capital	1047		Gen Trans	Capital	1047		Gen Trans	Capital	1047		Gen Trans	Capital	1047		Gen Trans	Capital	1047	
37																								
38																								
39		Other OMA	138			Other OMA	342			Other OMA	342			Other OMA	342			Other OMA	342			Other OMA	342	
40		Total	490			Total	1389			Total	1389			Total	1389			Total	1389			Total	1389	
41																								
42	New Trans	Cap & OM	0		New Trans	Cap & OM	766		New Trans	Cap & OM	580		New Trans	Cap & OM	478		New Trans	Cap & OM	478		New Trans	Cap & OM	439	
43																								
44																								
45	Distrib	Capital	2837		Distrib	Capital	3322		Distrib	Capital	3322		Distrib	Capital	3322		Distrib	Capital	3322		Distrib	Capital	3322	
46																								
47																								
48		Other OMA	8714			Other OMA	11228			Other OMA	11228			Other OMA	11228			Other OMA	11228			Other OMA	11228	
49		Total	11551			Total	14550			Total	14550			Total	14550			Total	14550			Total	14550	
50																								
51	Fuels	Total	14074		Fuels	Total	15185		Fuels	Total	15924		Fuels	Total	16867		Fuels	Total	17296		Fuels	Total	18782	
52																								
53	NUGS	Capital			NUGS	Capital			NUGS	Capital			NUGS	Capital			NUGS	Capital			NUGS	Capital		
54		Fix OMA	0			Fix OMA				Fix OMA				Fix OMA				Fix OMA				Fix OMA		
*Line																								
Col.	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	

FIGURE 8.3-11 (CONTINUED)

Section I. PRESENT VALUE FOR BASIC GROUP COSTS OF NEW AND EXISTING SYSTEMS (1909 M\$ PV) - MEDIAN LOAD FORECAST

55		Var OMA	1023		Var OMA	2642		Var OMA	2642		Var OMA	2642		Var OMA	2642		Var OMA	2642					
56																							
57		Total	1023		Total	2642		Total	2642		Total	2642		Total	2642		Total	2642					
58																							
59	DM	Capital	868	DM	Capital	3103	DM	Capital	3103	DM	Capital	3103	DM	Capital	3103	DM	Capital	3103					
60																							
61																							
62		Other OMA	893		Other OMA	1552		Other OMA	1552		Other OMA	1552		Other OMA	1552		Other OMA	1552					
63		Total	1561		Total	4655		Total	4655		Total	4655		Total	4655		Total	4655					
64																							
65	Other	Capital	9244	Other	Capital	9244	Other	Capital	9244	Other	Capital	9244	Other	Capital	9244	Other	Capital	9244					
66																							
67																							
68		OMA	8444		OMA	8444		OMA	8444		OMA	8444		OMA	8444		OMA	8444					
69																							
70																							
71																							
72		Total	17688		Total	17688		Total	17688		Total	17688		Total	17688		Total	17688					
73																							
74	Purchase	Capital	0	Purchase	Capital	1183	Purchase	Capital	1183	Purchase	Capital	1183	Purchase	Capital	1183	Purchase	Capital	1183					
75	1000 MW	Fix OMA		1000 MW	Fix OMA		1000 MW	Fix OMA		1000 MW	Fix OMA		1000 MW	Fix OMA		1000 MW	Fix OMA						
76																							
77																							
78		Total	0		Total	1183		Total	1183		Total	1183		Total	1183		Total	1183					
79																							
80	Sales	Total	27	Sales	Total	333	Sales	Total	189	Sales	Total	119	Sales	Total	96	Sales	Total	72					
81																							
82																							
83				Fixed OMAA		Fixed OMAA		Fixed OMAA		Fixed OMAA		Fixed OMAA		Fixed OMAA		Fixed OMAA							
84				of Existing System	11607	of Existing System	11607	of Existing System	11607	of Existing System	11607	of Existing System	11607	of Existing System	11607	of Existing System	11607						
85																							
86				Project	TOTAL	76330	Project	TOTAL	74507	Project	TOTAL	73991	Project	TOTAL	74199	Project	TOTAL	74823					
*Line																							
Col.	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W

There is one exception in this figure. Fixed OM&A for nuclear, fossil, acid gas controls and hydraulic are for new equipment only; and except for acid gas controls, which corresponds to new retrofits on existing plants, are labelled New Fixed OM&A. The fixed OM&A for the existing system is added separately at the bottom of the figure (line 84).

Figure 8.3-12 summarizes the cost sources for the major cost groups for Case 15, median load forecast. The first two columns link to the line number and cost groups of Figure 8.3-11. The third column describes what costs are in the cost group. The fourth column links back to the original source data provided earlier in this chapter. The fifth column links to RAM, where all data are integrated. The final column presents some comments on the data.

Figure 8.3-13 presents results when existing system costs are subtracted from the total system costs (note: the fixed OM&A for new nuclear, fossil, hydraulic, and acid gas controls on existing plants were taken directly from Figure 8.3-11). The resulting costs are the costs attributed to the Major Supply Cases for median load forecast.

FIGURE 8.3-12

1989 Demand/Supply Plan General Data/Source Description Present Value of Basic Group Costs

Illustration: Case 15 - Median Load Forecast

Line #	Cost Group	Description	Source Name	End Model	Comments
Section I. Basic Cost Groups of Existing and New Systems					
4	Nuclear Capital	Capital of new nuclear units	ONCI	RAM	Approval cost added according to specified dates.
5	Nuclear Fixed OM&A	Fixed OM&A of new nuclear units	ONCI	RAM	
6	Nuclear Fuel	Nuclear fuel of all generating units	LMSTM	RAM	
9	Nuclear Sales	Net Revenue from all nuclear sec. sales	LMSTM	RAM	
11	Nuclear Total	Sum of lines 1 through 10			
13	Fossil Capital	Capital of new fossil units	TCR	RAM	Approval cost added according to specified dates.
14	Fossil Fixed OM&A	Fixed OM&A of new fossil units	TCR	RAM	
15	Fossil Fuel	Fossil fuel of all generating units	LMSTM	RAM	
20	Fossil Total	Sum of lines 13 through 19			
22	AG Controls Capital	Capital of acid gas controls on existing units	ACID GAS	RAM	Cost of approval blended with the costs of capital.
23	AG Fixed OM&A	Fixed OM&A of AG controls on existing units	ACID GAS	RAM	
24	AG Var. OM&A	(combined with foss. fuel and var. OM&A)	LMSTM	RAM	
25	AG Total	Sum of lines 22 through 24			
27	Hydraulic Capital	Capital of new hydraulic projects	HYDRO CAP.	RAM	
28	Hydraulic Fixed OM&A	Fixed OM&A of new hydraulic plants	LMSTM	RAM	Difference between new and existing systems.

Notes:

ONCI: Ontario Nuclear Cost Inquiry
LMSTM: Load Management Strategy Testing Model
TCR: Thermal Cost Review
RAM: Risk Assessment Model

FIGURE 8.3-12 (CONTINUED)

1989 Demand/Supply Plan General Data/Source Description Present Value of Basic Group Costs

Illustration: Case 15 - Median Load Forecast

Line #	Cost Group	Description	Source Name	End Model	Comments
29	Hydraulic Var. OM&A	Water rentals and var. OM&A of all generating units	LMSTM	RAM	
31	Hydraulic Purchase	5X200 MW purchase from Manitoba	LMSTM	RAM	
34	Hydraulic Total	Sum of lines 27 through 29			
36	Generic Transmission Capital	Capital cost of existing system & growth-related	LMSTM	RAM	New specific projects excluded.
37	Generic Transmission Other OM&A	Total OM&A of existing system	LMSTM	RAM	New specific projects excluded.
40	Generic Trans. Total	Sum of lines 36 through 39			
42	New Trans. Capital, OM&A	Total of capital and OM&A of site-specific transmission	TRANS.	RAM	New site-specific projects.
45	Distr. Capital	Capital cost charged to existing system	LMSTM	RAM	Includes municipal costs.
46	Distribution Other OM&A	Total OM&A of existing system	LMSTM	RAM	Includes municipal costs.
49	Distr. Total	Sum of lines 45 through 48			
51	Fuels	Total var. OM&A all units (fuels), purch. NUGS, 5X200 MW purchase, unsupplied energy, and nuc. sec. sales.	LMSTM	RAM	All fuel and variable OM&A modeled.
53	NUGS Var. OM&A	Purchase NUGS	LMSTM	RAM	
56	NUGS Total	Sum of lines 53 through 55			

NOTES:

ONCI: Ontario Nuclear Cost Inquiry
LMSTM: Load Management Strategy Testing Model
TCR: Thermal Cost Review
RAM: Risk Assessment Model

FIGURE 8.3-12 (CONTINUED)

1989 Demand/Supply Plan
General Data/Source Description
Present Value of Basic Group Costs

Illustration: Case 15 - Median Load Forecast

Line #	Cost Group	Description	Source Name	End Model	Comments
59	DM Capital	Capital cost of DM for Hydro and Participants	LMSTM	RAM	
62	DM Other OM&A	Total OM&A of DM both Hydro's and participants'	LMSTM	RAM	
63	DM Total	Sum of lines 59 through 62			
65	Other Capital	Capital cost charged for other resources. Includes rebaring. Excl. costs of DM, Trans., Distr., and Dartington.	LMSTM	RAM	
68	Other OM&A	Other OM&A of existing system	LMSTM	RAM	
72	Other Total	Sum of lines 65 and 68			
78	Purchase Total	Total purchase cost of 1000 MW from Manitoba	MAN. PURCH.	RAM	
80	Nuc. Sales Total	Net Revenue from all nuclear sec. sales	LMSTM	RAM	(same as line no. 9)
84	Existing System Fixed OM&A Total	Total fixed OM&A of existing system (complement to that of new system)	LMSTM (special run)	RAM	Cost computed separately with LMSTM.
88	Project Total	Total Case's PV	RAM	RAM	Sum of all costs modeled.

Section II: Costs of expansion Cases relative to estimate of Existing System

104 to 180 Values result from costs of expansion Cases net of corresponding costs for Existing System.

Notes:
ONCI: Ontario Nuclear Cost Inquiry
LMSTM: Load Management Strategy Testing Model
TCR: Thermal Cost Review
RAM: Risk Assessment Model

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101	EXISTING			Project	CASE 23		Project	CASE 22		Project	CASE 15		Project	CASE 24		Project	CASE 26	
102	PV\$M 1990				PV\$M 1990			PV\$M 1990			PV\$M 1990			PV\$M 1990			PV\$M 1990	
103																		
104	Nuclear	Capital	0	Nuclear	Capital	5165	Nuclear	Capital	3352	Nuclear	Capital	2189	Nuclear	Capital	1630	Nuclear	Capital	0
105		Fix OMA	0		Fix OMA	2553		Fix OMA	1675		Fix OMA	1083		Fix OMA	810		Fix OMA	0
106		Fuel	0		Fuel	914		Fuel	751		Fuel	584		Fuel	500		Fuel	193
107																		
108																		
109		Salces	0		Salces	308		Salces	181		Salces	91		Salces	69		Salces	45
110																		
111		Total	0		Total	8937		Total	5969		Total	3947		Total	3018		Total	238
112																		
113	Fossil	Capital	0	Fossil	Capital	92	Fossil	Capital	208	Fossil	Capital	517	Fossil	Capital	908	Fossil	Capital	1926
114		Fix OMA	0		Fix OMA	0		Fix OMA	25		Fix OMA	73		Fix OMA	262		Fix OMA	847
115		Fuel	0		Fuel	-1653		Fuel	-750		Fuel	360		Fuel	872		Fuel	2665
116																		
117																		
118																		
119																		
120		Total	0		Total	-1560		Total	-518		Total	950		Total	2042		Total	5437
121																		
122	AG Cnts	Capital	0	AG Cnts	Capital	346	AG Cnts	Capital	346	AG Cnts	Capital	346	AG Cnts	Capital	346	AG Cnts	Capital	346
123		Fix OMA	0		Fix OMA	95		Fix OMA	95		Fix OMA	95		Fix OMA	95		Fix OMA	95
124		Var OMA	[Foss Fuel]		Var OMA	[Foss Fuel]		Var OMA	[Foss Fuel]		Var OMA	[Foss Fuel]		Var OMA	[Foss Fuel]		Var OMA	[Foss Fuel]
125		Total	0		Total	441		Total	441		Total	441		Total	441		Total	441
126																		
127	Hydraulic	Capital	0	Hydraulic	Capital	1189	Hydraulic	Capital	1189	Hydraulic	Capital	1189	Hydraulic	Capital	1189	Hydraulic	Capital	1189
128		Fix OMA	0		Fix OMA	200		Fix OMA	200		Fix OMA	200		Fix OMA	200		Fix OMA	200
129		Var OMA	0		Var OMA	84		Var OMA	84		Var OMA	84		Var OMA	84		Var OMA	84
130																		
131		Purch 200	0		Purch 200	148		Purch 200	0		Purch 200	148		Purch 200	148		Purch 200	148
132																		
133																		
134		Total	0		Total	1620		Total	1473		Total	1620		Total	1620		Total	1620
135																		
136	Gen Trans	Capital	0	Gen Trans	Capital	696	Gen Trans	Capital	696	Gen Trans	Capital	696	Gen Trans	Capital	696	Gen Trans	Capital	696
137																		
138																		
139		Other OMA	0		Other OMA	204		Other OMA	204		Other OMA	204		Other OMA	204		Other OMA	204
140		Total	0		Total	899		Total	899		Total	899		Total	899		Total	899
141																		

FIGURE 8.3-13 (CONTINUED)

Section II. PRESENT VALUE FOR BASIC GROUP COSTS OF NEW SYSTEM NET OF EXISTING COSTS (1989 M\$ PV) - MEDIAN LOAD FORECAST

155		Var OMA	0		Var OMA	1619		Var OMA	1619		Var OMA	1619		Var OMA	1619		Var OMA	1619					
156																							
157		Total	0		Total	1619		Total	1619		Total	1619		Total	1619		Total	1619					
158																							
159	DM	Capital	0	DM	Capital	2235	DM	Capital	2235	DM	Capital	2235	DM	Capital	2235	DM	Capital	2235					
160																							
161																							
162		Other OMA	0		Other OMA	859		Other OMA	859		Other OMA	859		Other OMA	859		Other OMA	859					
163		Total	0		Total	3094		Total	3094		Total	3094		Total	3094		Total	3094					
164																							
165	Other	Capital	0	Other	Capital	0	Other	Capital	0	Other	Capital	0	Other	Capital	0	Other	Capital	0					
166																	Flx OMA						
167																	Var OMA						
168		OMA	0		OMA	0		OMA	0		OMA	0		OMA	0		OMA	0					
169																							
170																							
171																							
172		Total	0		Total	0		Total	0		Total	0		Total	0		Total	0					
173																							
174	Purchase	Capital	0	Purchase	Capital	1183	Purchase	Capital	1183	Purchase	Capital	1183	Purchase	Capital	1183	Purchase	Capital	1183					
175	1000 MW	Flx OMA		1000 MW	Flx OMA		1000 MW	Flx OMA		1000 MW	Flx OMA		1000 MW	Flx OMA		1000 MW	Flx OMA						
176																							
177																							
178		Total	0		Total	1183		Total	1183		Total	1183		Total	1183		Total	1183					
179																							
180	Sales	Total	0	Sales	Total	306	Sales	Total	161	Sales	Total	91	Sales	Total	69	Sales	Total	45					
*Line																							
Col	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W

8.3.3 Cost of Ontario Hydro New Major Supply

In the DSP Report, Figure 15-46 shows the cost of Ontario Hydro new major supply for median load forecast. Figure 8.3-14 shows how these values were determined from the cost values in Figure 8.3-13. The formulas refer to coordinates in Figure 8.3-13. For example, +O104 refers to the value in Figure 8.3-13 under column O at line 104, which is 2,189 M\$ (PV 1989).

Figures 8.3-15 through 8.3-19 show the costs of new major supply for the five load forecast paths. The differences between the major supply cases, relative to Case 15, are shown at the bottom of these tables. These results relate to Figure 15-49 of the DSP report, which shows the same results for the lower, median and upper load forecasts.

FIGURE 8.3-14

Cost of Ontario Hydro New Major Supply
 Median Load Growth - Median Cost Estimates
 Cost Calculation Formulas
 Reference: Basic Group Costs (Sections I and II)
 \$1989 Million (PV) allocated to 1994-2014

Cost Component	Case 23	Case 22	Case 15	Case 24	Case 26
Nuclear					
Capital	+G104	+K104	+O104	+S104	+W104
OM&A	+G105	+K105	+O105	+S105	+W105
Fossil					
Capital	+G113	+K113	+O113	+S113	+W113
OM&A	+G114	+K114	+O114	+S114	+W114
Fuel Related Costs associated with Growth beyond 1993	+G106+G115+G124+G129+G180	+K106+K115+K124+K129+K180	+O106+O115+O124+O129+O180	+S106+S115+S124+S129+S180	+W106+W115+W124+W129+W180
Bulk Transmission Cost Difference from Case 15	+G140+G142-(O140+O142)	+K140+K142-(O140+O142)	+O140+O142-(O140+O142)	+S140+S142-(O140+O142)	+W140+W142-(O140+O142)
TOTAL	SUM OF ABOVE	SUM OF ABOVE	SUM OF ABOVE	SUM OF ABOVE	SUM OF ABOVE
Difference from Case 15	TOTAL MINUS CASE 15'S	TOTAL MINUS CASE 15'S	BASE	TOTAL MINUS CASE 15'S	TOTAL MINUS CASE 15'S

FIGURE 3-1
Cost of Ontario Hydro New Major Supply
Median Load Forecast - Median Cost Estimates

\$1989 Million (PV) allocated to 1994-2014

Cost Component	Case 23	Case 22	Case 15	Case 24	Case 26
Nuclear					
Capital	5,165	3,382	2,189	1,639	0
OM&A	2,553	1,675	1,083	810	0
Fossil					
Capital	92	208	517	908	1,926
OM&A	0	25	73	262	847
Fuel-Related Costs associated with Growth beyond 1993	(961)	(77)	936	1,387	2,897
Bulk Transmission Cost Difference from Case 15	287	101	0	0	(40)
TOTAL	7,137	5,314	4,798	5,006	5,630
Difference from Case 15	2,339	516	BASE	208	832

FIGURE 8.3-16
Cost of Ontario Hydro New Major Supply
Branch Upper Load Forecast - Median Cost Estimates

\$1989 Million (PV) allocated to 1994-2014

Cost Component	Case 23	Case 22	Case 15	Case 24	Case 26
Nuclear					
Capital	6,060	3,997	2,963	2,072	0
OM&A	3,003	1,984	1,472	1,027	0
Fossil					
Capital	107	512	798	1,383	2,689
OM&A	2	86	122	423	1,156
Fuel-Related Costs associated with Growth beyond 1993	86	1,336	2,322	2,993	5,125
Bulk Transmission Cost Difference from Case 15	249	82	0	33	0
TOTAL	9,507	7,996	7,677	7,931	8,971
Difference from Case 15	1,830	319	BASE	254	1,294

FIGURE 8.3-17

Cost of Ontario Hydro New Major Supply
Upper Load Forecast - Median Cost Estimates

\$1989 Million (PV) allocated to 1994-2014

Cost Component	Case 23	Case 22	Case 15	Case 24	Case 26
Nuclear					
Capital	5,946	4,127	3,438	2,515	0
OM&A	2,946	2,048	1,708	1,263	0
Fossil					
Capital	889	1,216	1,360	2,001	3,592
OM&A	327	382	410	713	1,609
Fuel-Related Costs associated with Growth beyond 1993	3,072	4,513	5,276	5,920	8,204
Bulk Transmission Cost Difference from Case 15	176	72	0	0	0
TOTAL	13,355	12,358	12,191	12,412	13,405
Difference from Case 15	1,164	167	BASE	221	1,214

FIGURE 8.3-18

Cost of Ontario Hydro New Major Supply
Branch Lower Load Forecast - Median Cost Estimates

\$1989 Million (PV) allocated to 1994-2014

Cost Component	Case 23	Case 22	Case 15	Case 24	Case 26
Nuclear					
Capital	4,573	2,529	1,956	1,723	0
OM&A	2,257	1,139	867	753	0
Fossil					
Capital	92	218	266	440	1,441
OM&A	0	27	33	114	661
Fuel-Related Costs associated with Growth beyond 1993	(1,867)	(940)	(535)	(353)	849
Bulk Transmission Cost Difference from Case 15	326	46	0	3	(86)
TOTAL	5,381	3,019	2,588	2,681	2,865
Difference from Case 15	2,794	432	BASE	93	277

FIGURE 8.3-19

Cost of Ontario Hydro New Major Supply
Lower Load Forecast - Median Cost Estimates

\$1989 Million (PV) allocated to 1994-2014

Cost Component	Case 23	Case 22	Case 15	Case 24	Case 26
Nuclear					
Capital	2,861	1,212	624	510	0
OM&A	1,404	597	305	249	0
Fossil					
Capital	102	129	222	290	612
OM&A	1	6	28	65	247
Fuel-Related Costs associated with Growth beyond 1993	(229)	456	970	1,053	1,516
Bulk Transmission Cost Difference from Case 15	164	62	0	0	(39)
TOTAL	4,303	2,463	2,149	2,166	2,336
Difference from Case 15	2,154	314	BASE	17	187

8.3.4 Total Cost of New Demand/Supply Options and Operating the Existing System

In the DSP Report, Figure 15-47 shows the total cost of new demand/supply options and operating the existing system for the median load forecast for the five cases. Figure 8.3-20 shows how these values are determined from the cost values in Figures 8.3-11 and 8.3-13.

Figures 8.3-21 through 8.3-25 show the total cost of new demand/supply options and operating the existing system under the five load forecast paths.

FIGURE 8.3-20

Total Cost of New Demand/Supply Options and Operating the Existing System
Median Load Forecast - Median Cost Estimates
Calculation Formulas
Reference: Basic Group Costs (Sections I & II)
\$1989 Million (PV)

		Case 23	Case 22	Case 15	Case 24	Case 26
Cost of New D/S Options Allocated to 1994-2014						
Nuclear	Capital	+G104	+K104	+O104	+S104	+W104
	OM&A	+G105	+K105	+O105	+S105	+W105
Fossil	Capital	+G113	+K113	+O113	+S113	+W113
	OM&A	+G114	+K114	+O114	+S114	+W114
Acid Gas Controls		+G122;G123	+K122;K123	+O122;O123	+S122;S123	+W122;W123
Merchants Purchase		+G178;G131	+K178;K131	+O178;O131	+S178;S131	+W178;W131
Hydraulic	Capital	+G127	+K127	+O127	+S127	+W127
	OM&A	+G128	+K128	+O128	+S128	+W128
Load Reducing Options DM & LD-NUGs		+G163	+K163	+O163	+S163	+W163
Purchase NUGs		+G157	+K157	+O157	+S157	+W157
Transmission		+G140;G142	+K140;K142	+O140;O142	+S140;S142	+W140;W142
Distribution		+G149	+K149	+O149	+S149	+W149
Total Cost of New D/S		SUM OF ABOVE	SUM OF ABOVE	SUM OF ABOVE	SUM OF ABOVE	SUM OF ABOVE
Fuel - Related Costs 1989-2014						
Cost associated with Existing Demand		+C51-C80	+C51-C80	+C51-C80	+C51-C80	+C51-C80
Cost associated with Growth beyond 1993		+G106;G115;G124;G129-G180	+G106;G115;G124;G129-G180	+O106;O115;O124;O129-O180	+G106;G115;G124;G129-G180	+G106;G115;G124;G129-G180
Total Fuel		SUM OF FUEL COSTS	SUM OF FUEL COSTS	SUM OF FUEL COSTS	SUM OF FUEL COSTS	SUM OF FUEL COSTS
Cost of Existing System - allocated to 1994-2014		+C51;C14;C23;C28;C36;C37; C39;C45;C46;C48;C54;C56;C59; C60;C62;C65;C66;C68	+C51;C14;C23;C28;C36;C37; C39;C45;C46;C48;C54;C56;C59; C60;C62;C65;C66;C68	+C51;C14;C23;C28;C36;C37; C39;C45;C46;C48;C54;C56;C59; C60;C62;C65;C66;C68	+C51;C14;C23;C28;C36;C37; C39;C45;C46;C48;C54;C56;C59; C60;C62;C65;C66;C68	+C51;C14;C23;C28;C36;C37; C39;C45;C46;C48;C54;C56;C59; C60;C62;C65;C66;C68
Total Cost of New D/S Options and operating the Existing System		GRAND TOTAL	GRAND TOTAL	GRAND TOTAL	GRAND TOTAL	GRAND TOTAL
Cost Differences from Case 15		ABOVE TOTAL MINUS CASE 15'S	ABOVE TOTAL MINUS CASE 15'S	BASE	ABOVE TOTAL MINUS CASE 15'S	ABOVE TOTAL MINUS CASE 15'S

FIGURE 8.3-21

Total Cost of New Demand/Supply Options and Operating the Existing System
 Median Load Forecast - Median Cost Estimates
 \$1989 Million Present Value

		Case 23	Case 22	Case 15	Case 24	Case 26
<u>Cost of New D/S Options</u> - allocated to 1994-2014						
Nuclear	Capital	5,165	3,382	2,189	1,639	0
	OM&A	2,553	1,675	1,083	810	0
Fossil	Capital	92	208	517	908	1,926
	OM&A	0	25	73	262	847
Acid Gas Controls		441	441	441	441	441
Manitoba Purchase		1,331	1,331	1,331	1,331	1,331
Hydraulic	Capital	1,189	1,189	1,189	1,189	1,189
	OM&A	200	200	200	200	200
Load Reducing Options DM & LD-NUGS		3,094	3,094	3,094	3,094	3,094
Purchase Nugs		1,619	1,619	1,619	1,619	1,619
Transmission		1,665	1,479	1,378	1,378	1,338
Distribution		2,998	2,998	2,998	2,998	2,998
<u>Total</u>		<u>20,347</u>	<u>17,641</u>	<u>16,111</u>	<u>15,868</u>	<u>14,982</u>
<u>Fuel - Related Costs 1989-2014</u>						
Cost Associated with Existing Demand		14,046	14,046	14,046	14,046	14,046
Net Cost associated with Growth beyond 1993		(961)	(77)	936	1,387	2,897
<u>Total</u>		<u>13,085</u>	<u>13,969</u>	<u>14,982</u>	<u>15,433</u>	<u>16,943</u>
<u>Cost of Existing System</u> - allocated to 1989-2014		<u>42,898</u>	<u>42,898</u>	<u>42,898</u>	<u>42,898</u>	<u>42,898</u>
<u>Total Cost of New D/S Options</u> <u>& operating the Existing System</u>		<u>76,330</u>	<u>74,507</u>	<u>73,991</u>	<u>74,199</u>	<u>74,823</u>
<u>Cost Differences from Case 15</u>		<u>2,339</u>	<u>516</u>	<u>BASE</u>	<u>208</u>	<u>832</u>

FIGURE 8.3-22

Total Cost of New Demand/Supply Options and Operating the Existing System
Branch Upper Load Forecast - Median Cost Estimates
\$1989 Million Present Value

		Case 23	Case 22	Case 15	Case 24	Case 26
<u>Cost of New D/S Options</u> - allocated to 1994-2014						
Nuclear	Capital	6,060	3,997	2,963	2,072	0
	OM&A	3,003	1,984	1,472	1,027	0
Fossil	Capital	107	512	798	1,383	2,689
	OM&A	2	86	122	423	1,156
Acid Gas Controls		717	717	717	717	717
Manitoba Purchase		1,331	1,331	1,331	1,331	1,331
Hydraulic	Capital	1,189	1,189	1,189	1,189	1,189
	OM&A	200	200	200	200	200
Load Reducing Options:						
DM & LD-NUGS		3,489	3,489	3,489	3,489	3,489
Purchase Nugs		1,824	1,824	1,824	1,824	1,824
Transmission		2,067	1,900	1,818	1,851	1,819
Distribution		3,277	3,277	3,277	3,277	3,277
<u>Total</u>		<u>23,265</u>	<u>20,505</u>	<u>19,199</u>	<u>18,782</u>	<u>17,639</u>
<u>Fuel - Related Costs 1989-2014</u>						
Cost Associated with Existing Demand		14,046	14,046	14,046	14,046	14,046
Net Cost associated with Growth beyond 1993		86	1,336	2,322	2,993	5,125
<u>Total</u>		<u>14,132</u>	<u>15,382</u>	<u>16,368</u>	<u>17,039</u>	<u>19,172</u>
<u>Cost of Existing System</u> - allocated to 1989-2014		<u>42,898</u>	<u>42,898</u>	<u>42,898</u>	<u>42,898</u>	<u>42,898</u>
<u>Total Cost of New D/S Options & operating the Existing System</u>		<u>80,294</u>	<u>78,784</u>	<u>78,464</u>	<u>78,719</u>	<u>79,756</u>
<u>Cost Differences from Case 15</u>		<u>1,830</u>	<u>319</u>	<u>BASE</u>	<u>254</u>	<u>1,294</u>

FIGURE 8.3-23

Total Cost of New Demand/Supply Options and Operating the Existing System
Upper Load Forecast - Median Cost Estimates
\$1989 Million Present Value

		Case 23	Case 22	Case 15	Case 24	Case 26
<u>Cost of New D/S Options</u> <u>- allocated to 1994-2014</u>						
Nuclear	Capital	5,946	4,127	3,438	2,515	0
	OM&A	2,946	2,048	1,708	1,263	0
Fossil	Capital	889	1,216	1,360	2,001	3,592
	OM&A	327	382	410	713	1,609
Acid Gas Controls		1,135	1,135	1,135	1,135	1,135
Manitoba Purchase		1,331	1,331	1,331	1,331	1,331
Hydraulic	Capital	1,189	1,189	1,189	1,189	1,189
	OM&A	200	200	200	200	200
Load Reducing Options						
DM & LD-NUGS		4,421	4,421	4,421	4,421	4,421
Purchase Nugs		2,032	2,032	2,032	2,032	2,032
Transmission		2,391	2,287	2,215	2,215	2,215
Distribution		3,607	3,607	3,607	3,607	3,607
Total		26,413	23,974	23,044	22,621	21,330
<u>Fuel - Related Costs 1989-2014</u>						
Cost Associated with Existing Demand		14,046	14,046	14,046	14,046	14,046
Net Cost associated with Growth beyond 1993		3,072	4,513	5,276	5,920	6,204
Total		17,118	18,559	19,322	19,966	22,250
<u>Cost of Existing System</u> <u>- allocated to 1989-2014</u>		42,898	42,898	42,898	42,898	42,898
<u>Total Cost of New D/S Options</u> <u>& operating the Existing System</u>		86,428	85,431	85,264	85,485	86,477
<u>Cost Differences from Case 15</u>		1,164	167	BASE	221	1,214

FIGURE 8.3-24

Total Cost of New Demand/Supply Options and Operating the Existing System
Branch Lower Load Forecast - Median Cost Estimates
\$1989 Million Present Value

		Case 23	Case 22	Case 15	Case 24	Case 25
Cost of New D/S Options - allocated to 1994-2014						
Nuclear	Capital	4,573	2,529	1,956	1,723	0
	OM&A	2,257	1,139	867	753	0
Fossil	Capital	92	218	266	440	1,441
	OM&A	0	27	33	114	661
Acid Gas Controls		441	441	441	441	441
Manitoba Purchase		1,331	1,331	1,331	1,331	1,331
Hydraulic	Capital	1,189	1,189	1,189	1,189	1,189
	OM&A	200	200	200	200	200
Load Reducing Options DM & LD-NUGS		2,670	2,670	2,670	2,670	2,670
Purchase Nugs		1,094	1,094	1,094	1,094	1,094
Transmission		1,284	1,004	958	961	872
Distribution		2,704	2,704	2,704	2,704	2,704
Total		17,835	14,545	13,709	13,620	12,602
Fuel - Related Costs 1989-2014						
Cost Associated with Existing Demand		14,046	14,046	14,046	14,046	14,046
Net Cost associated with Growth beyond 1993		(1,867)	(940)	(535)	(353)	849
Total		12,179	13,106	13,511	13,693	14,895
Cost of Existing System - allocated to 1989-2014		42,898	42,898	42,898	42,898	42,898
Total Cost of New D/S Options & operating the Existing System		72,912	70,549	70,118	70,211	70,395
Cost Differences from Case 15		2,794	432	BASE	93	277

FIGURE 8.3-25

Total Cost of New Demand/Supply Options and Operating the Existing System
Lower Load Forecast - Median Cost Estimates
\$1989 Million Present Value

		Case 23	Case 22	Case 15	Case 24	Case 26
<u>Cost of New D/S Options - allocated to 1994-2014</u>						
Nuclear	Capital	2,861	1,212	624	510	0
	OM&A	1,404	597	305	249	0
Fossil	Capital	102	129	222	290	612
	OM&A	1	6	28	65	247
Acid Gas Controls		227	227	227	227	227
Manitoba Purchase		1,265	1,265	1,265	1,265	1,265
Hydraulic	Capital	1,189	1,189	1,189	1,189	1,189
	OM&A	200	200	200	200	200
Load Reducing Options						
DM & LD-NUGS		1,391	1,391	1,391	1,391	1,391
Purchase Nugs		229	229	229	229	229
Transmission		1,002	901	839	839	800
Distribution		3,184	3,184	3,184	3,184	3,184
<u>Total</u>		<u>13,054</u>	<u>10,530</u>	<u>9,702</u>	<u>9,637</u>	<u>9,343</u>
<u>Fuel - Related Costs 1989-2014</u>						
Cost Associated with Existing Demand		10,506	10,506	10,506	10,506	10,506
Net Cost associated with Growth beyond 1993		(229)	456	970	1,053	1,516
<u>Total</u>		<u>10,278</u>	<u>10,962</u>	<u>11,476</u>	<u>11,559</u>	<u>12,022</u>
<u>Cost of Existing System - allocated to 1989-2014</u>		<u>42,354</u>	<u>42,354</u>	<u>42,354</u>	<u>42,354</u>	<u>42,354</u>
<u>Total Cost of New D/S Options & operating the Existing System</u>		<u>65,686</u>	<u>63,846</u>	<u>63,532</u>	<u>63,549</u>	<u>63,719</u>
<u>Cost Differences from Case 15</u>		<u>2,154</u>	<u>314</u>	<u>BASE</u>	<u>17</u>	<u>187</u>

8.3.5 Extension of the Study Period

To analyze the impact of the study period length, the evaluation period was extended ten, twenty, and thirty years. The resulting cost differences are listed here in Figure 8.3-26.

The approach followed in extending the evaluation period is essentially based on the following two simple assumptions:

- The system's structure of the case in question remains the same as of year 2014. For example, if the four generating units of a nuclear plant are in operation by the end of year 2014, then the same plant configuration remains operational during the extended period.
- The operational characteristics of the generating plant remain unchanged throughout the extension period. As well, the load, supply, and other demand factors are kept at the same level forecast for year 2014.

There are other alternative approaches. The method used was selected because of its simplicity and because it avoids having to speculate further on uncertain factors and policies beyond the original study period.

Figure 8.3-26

Cost Differences to 2014 and Beyond Relative to Case 15
Median Load Forecast
1989 \$ Billion

	<u>To 2104</u>	<u>To 2024</u>	<u>To 2034</u>	<u>To 2044</u>
Case 23	2.3	3.5	4.4	5.1
Case 22	0.5	0.7	0.8	0.9
Case 15	Base	Base	Base	Base
Case 24	0.2	0.5	0.6	0.7
Case 26	0.8	2.0	2.7	3.0

8.4 SENSITIVITY ANALYSIS

8.4.1 Examining Range of Costs in the Cases

Over a 25-year timeframe, actual costs and differences between cases will likely be different than the original most likely predictions. Hydro addresses these anticipated changes by determining total cost for all customers under a range of conditions. In doing so, Hydro determines the degree to which any case could differ from its most likely cost.

8.4.2 Cost Estimate Bands

Generation options have three major cost components; Capital, OM&A and Fuel; each of which can vary significantly, leading to a:

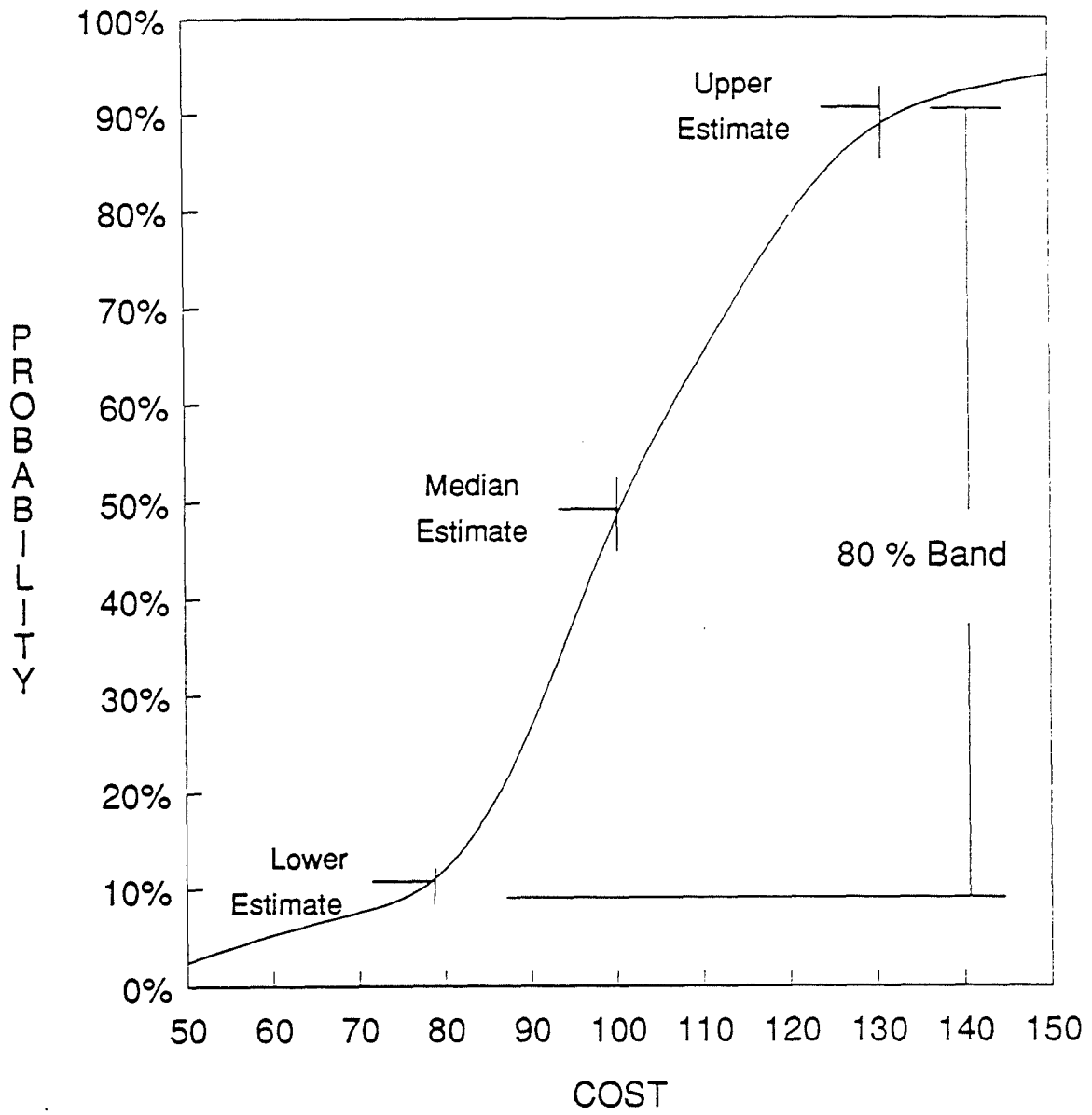
- (1) large difference in a case's cost
- (2) notable difference in cost between cases

Since the extremes of a cost estimate for these components tend to distort total case cost results, Hydro focuses on the confidence band--the 80% of a range between the high and low extreme estimates. Discrete values, selected on the basis of past experience and estimates of future conditions, define the low, median and upper points of a range. Figure 8.4-1 shows how these three points define the 80% "confidence band". Costs are measured along the bottom of the graph. A cost curve can be drawn through the low estimate of \$80, median estimate of \$100 and upper estimate of \$130, since costs can fall anywhere between the estimates.

Cost estimates have components with different degrees of uncertainty. In order to have a single range for each cost estimate within the costing model, specific range predictions for each cost component were weighted by the components contribution to the option's life cycle costs developed in the ONCI and TCR. These combined ranges for capital cost, capital modifications, and OMA, were used in RAM. The RAM also uses the additional 80% confidence band estimates for the economic factors and the fuel prices, when calculating the range of present value costs for each case.

The RAM present value costs include those investments made by the municipal utilities and the customers, thereby encompassing total electricity service costs. The RAM present value calculations for costs other than Hydro's components are escalated and discounted by Hydro's financial indicators and their cost bands. Since these costs are common to all cases they do not affect the differences in the present value cost.

Three Point Approximation For Cost Confidence Band



— Cost Curve

FIGURE 8.4-1

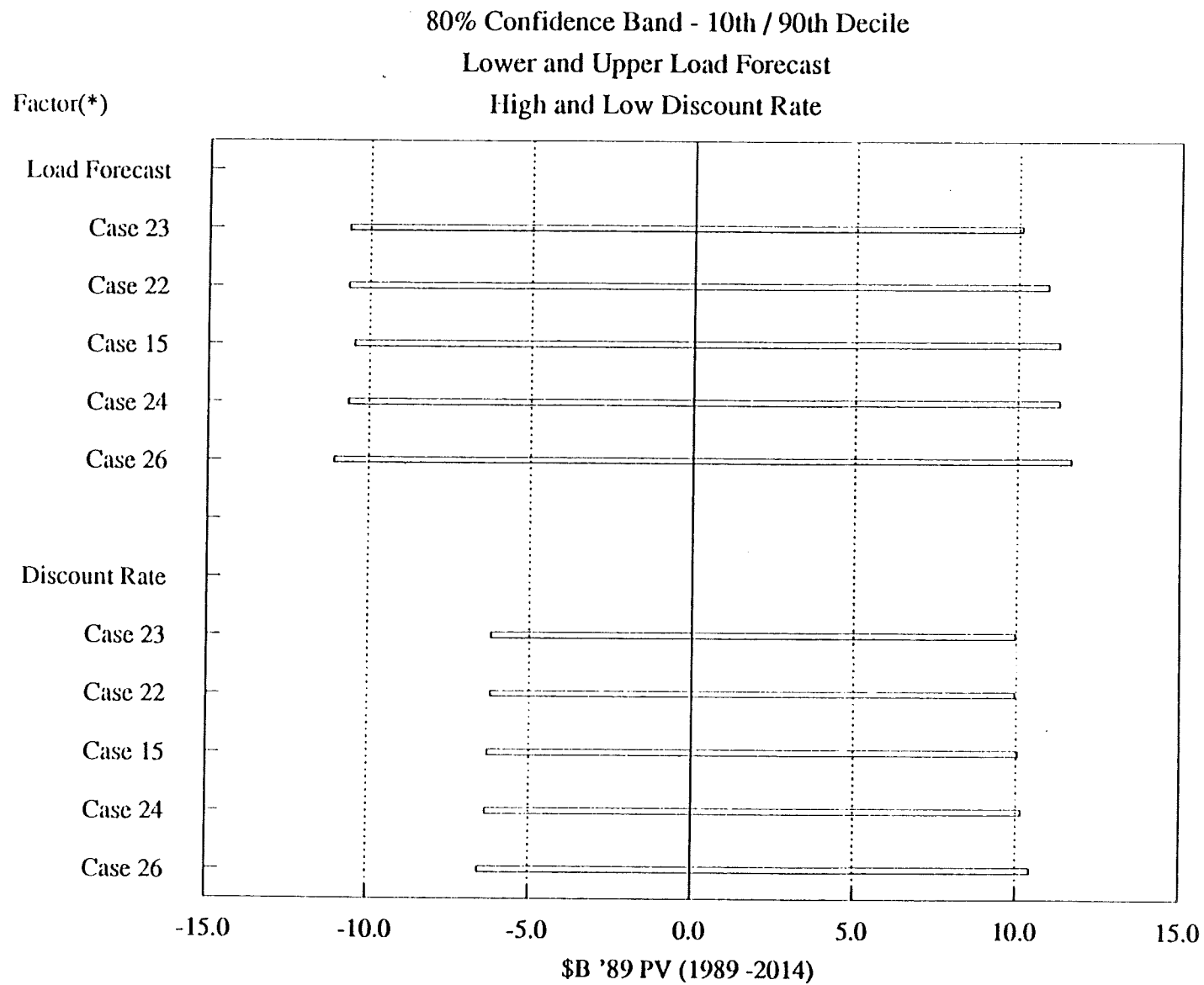
8.4.3 Cost Estimate Impacts On Case Costs

The factors requiring further study were established by examining the cost differences between cases caused by varying each individual factor independently. The RAM model was used to calculate how present value costs change in response to the cost estimate bands. The results were plotted on bar charts. When case cost components are very similar, there is very little difference in the resulting range of costs. While the length of the range can be significant, indicating an uncertainty common to all cases, the difference between cases can be insignificant.

Figure 8.4-2 shows the present value cost sensitivity to Load Forecast. The Lower and Upper load forecasts reflect the different amounts of energy to be supplied. The \$20 Billion range reflects the differences in capital and operating costs necessary to meet these two load paths. While cost factors, fuel prices and economic factors may differ under different load paths, these were fixed at their median value so that the resulting range of costs represented only load path uncertainty.

Figure 8.4-2 also shows the significant difference in present value costs when the Corporate Discount rate is varied. In order to provide real discount rate changes RAM recalculates the present value by changing the nominal discount rate by its predicted range while keeping the escalation fixed.

The significance of the discount rate to present value calculations is critical, especially when high capital options are built and financed over a long construction schedule with a high real cost of borrowing. These investments are made based on the assumption that the higher capital cost plant will provide greater operating efficiencies, resulting in lower operating costs and system peaking fuel savings. While the future system benefits may occur, their resulting "present value" cost savings may be significantly different from those assumed in the cost evaluations.



(*) Other Factors Fixed at Median

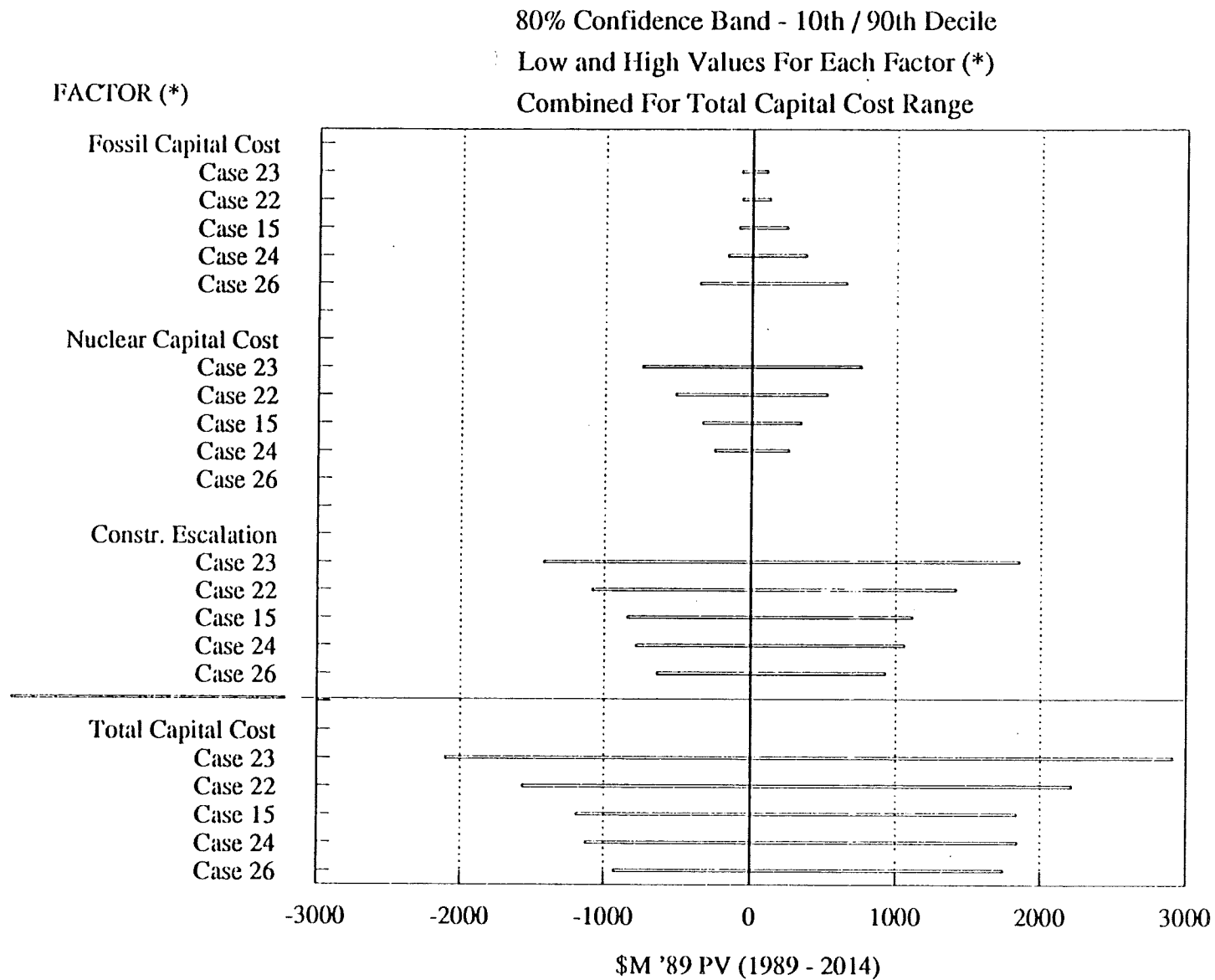
FIGURE 8.4-2

Figure 8.4-3 shows the sensitivity of base costs to the nuclear and fossil capital cost estimate bands and their construction cost escalators. In order to maintain a level of economic consistency and calculation efficiency, these cost estimates were combined. These combinations also provided a better indication of the more extreme differences between cases.

Many major components are common to all new generating options and their uncertainty is not dependent on the fuel type. For example if the nuclear option under construction were to experience higher capital costs then it is likely that similar cost pressures would also be applicable to the fossil options. Therefore, when the lower estimate for nuclear capital was used in RAM, the lower estimate for the fossil option was also used. In addition, both the nuclear and fossil construction cost escalators have many common elements such as Hydro labour and construction materials. Therefore, each options final construction costs would have similar escalation cost pressures regardless of the station type.

Figure 8.4-3 also shows the combined factor called Total Capital Costs. This range shows the cost range resulting when the three upper estimates are combined and when the three lower estimates are combined for the three components.

The uncertainty surrounding the capital cost of each option may differ, depending on a variety of factors such as newness of the technology, potential future environmental impact mitigation possibilities, Hydro past cost experience, etc. While the uncertainties have been linked, the cases have different levels of nuclear and fossil options. Their differences in response to capital and construction cost uncertainties are still captured by the degree to which each option constitutes a portion of the allocated present value costs.



(*) Other Factors Fixed at Median

FIGURE 8.4-3

Figure 8.4-4 shows the fossil and nuclear fuel cost ranges. The magnitude of these system fuel costs is highly dependent the new generating options in each case. The fossil fuel cost range reflects the significant difference in the amount of fossil fuel used by the system in each case.

Fuelling cost for nuclear options are less than for fossil options. Their cost uncertainty range is smaller, reflecting the lesser cost impact of system nuclear fuel cost within each case. While global energy pressures could cause fuel substitution, the fuel ranges are considered independent with the possibility that fossil prices can be higher while the nuclear fuel prices can be lower.

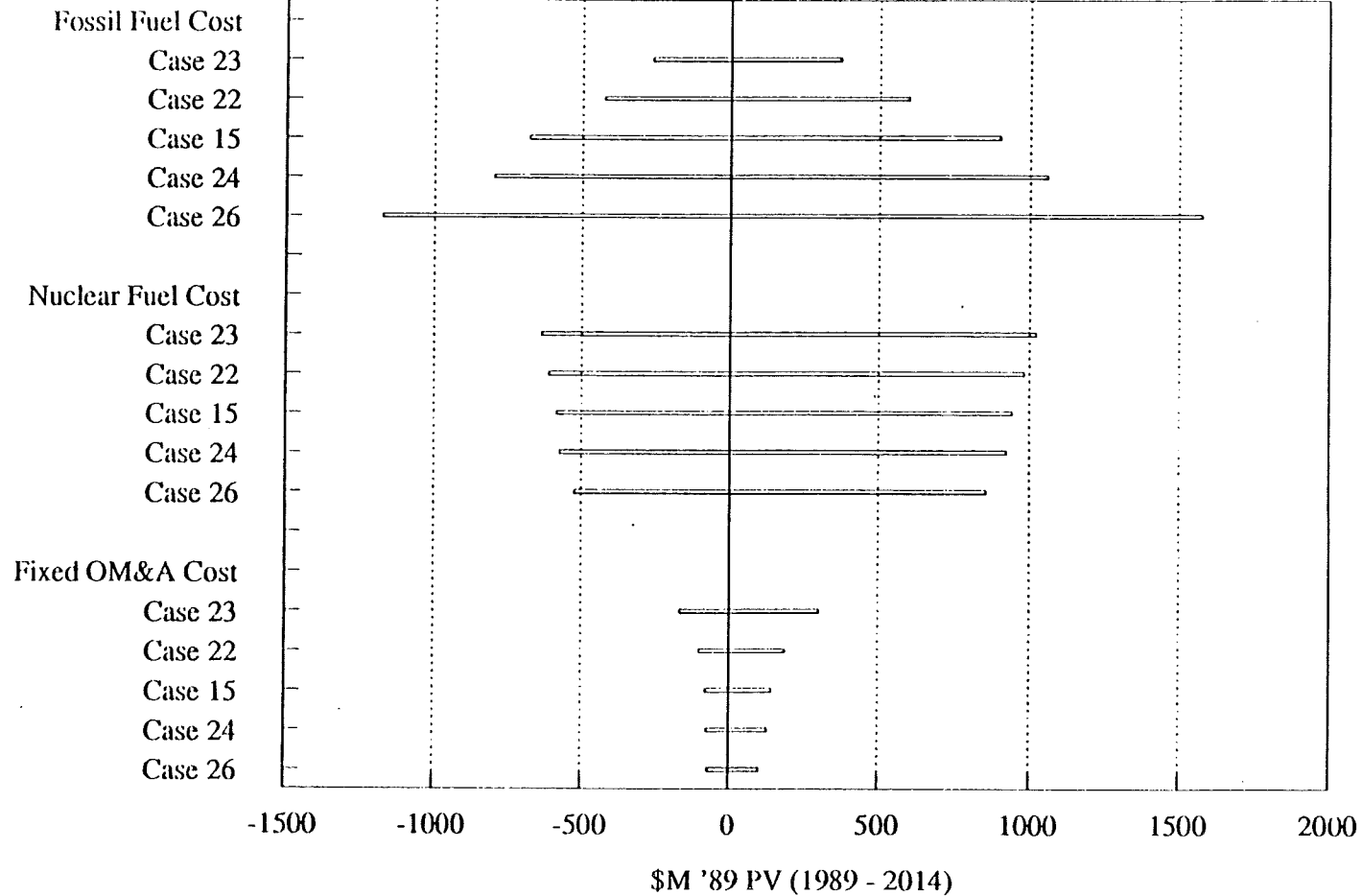
Figure 8.4-4 also indicates Fixed OMA costs uncertainty associated with the new options. These cost reflect the fixed labour and material cost for the operation and maintenance of the stations. The differences between cases reflect the higher OMA costs of the nuclear option. Many of the fixed OMA costs components are common to all Hydro generating stations therefore their uncertainty on the cost differences between cases would not be significant.

The five factors identified as having the greatest present value impact and worthy of further study with probabilistic methods were:

1. Load Forecast
2. Capital Construction Costs
3. Fossil Fuel Costs
4. Nuclear Fuel Costs
5. Cost of money (Real discount rate)

FIGURE 8.4-4
 80% Confidence Band - 10th / 90th Decile
 Low and High Values for Each Factor (*)
 Total System Fueling Costs for Each Case
 Operating and Maintenance for New System

FACTOR (*)



(*) Other Factors Fixed at Median

8.5 PROBABILISTIC ANALYSIS

8.5.1 Uncertainty - Expected Costs

Probabilistic cost evaluations recognize and deal with the uncertainties surrounding the major cost factors within each case. Uncertainty introduces financial risks into the planning process. Minimizing risks generally results in an increase in costs, and minimizing costs often increases risks. One of the tools used by decision makers to balance risks with costs is the expected cost concept.

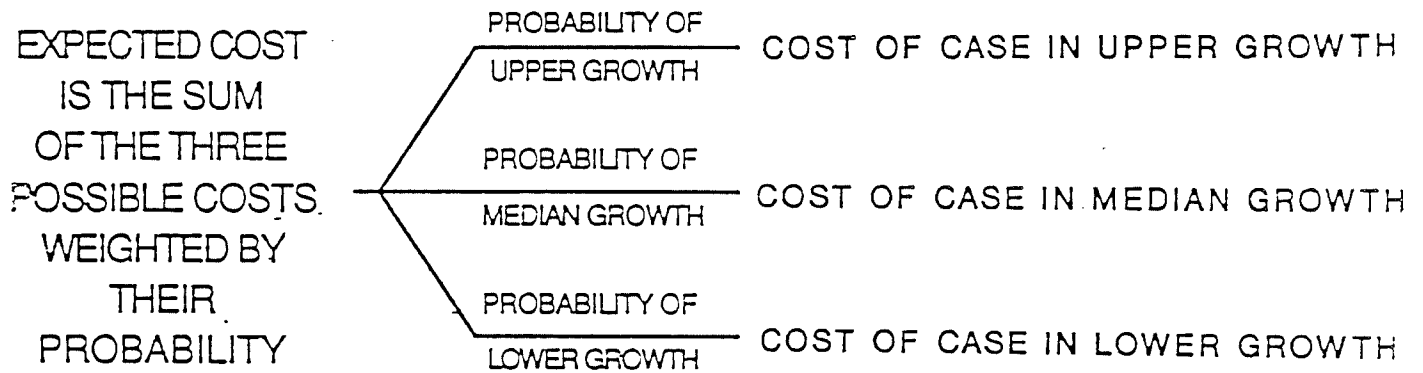
The expected cost of a case is the total cost of a case multiplied by the probability of the case's outcome. For example, Case A will have different costs depending on the load forecast. Under the median load forecast, the cost of Case A may be \$20 billion. With the upper load forecast, the cost of Case A may rise to \$30 billion. In the lower forecast, Case A may cost \$15 billion.

To determine the expected cost of Case A, recognizing load forecast uncertainty, the cost of Case A for the various forecasts is multiplied by the probability of the forecast. For example, if it is assumed that there is a 50% probability of median load forecast and a 25% probability of either the upper or lower forecasts, then the expected cost of Case A would be calculated as shown in Figure 8.5-1.

The resulting outcome would therefore provide Hydro with an expected cost of Case A under all three load forecast scenarios. The method can be extended to account for uncertainties in fuel costs, construction costs and discount rates, etc.

Figure 8.5-1

EXPECTED COST OF DEMAND/SUPPLY CASES



EXPECTED COST =

$$0.25 \times 30 + 0.5 \times 20 + 0.25 \times 15$$

= \$ 21.25 BILLION

```
graph LR; A[0.25] --- B[$ 30 BILLION]; A --- C[0.5]; C --- D[$ 20 BILLION]; C --- E[0.25]; E --- F[$ 15 BILLION]
```

0.25 \$ 30 BILLION

0.5 \$ 20 BILLION

0.25 \$ 15 BILLION

8.5.2 Load Forecasts

The probabilities assigned to each one of the five load forecasts were derived from the ranges provided by the 1989 Basic Load Forecast. To these forecasts a wide range of load possibilities and likelihood are associated.

For this analysis, five load regions were determined by identifying the midpoints found between adjacent load paths. Each one of the load regions thus created contained one of the five load paths and had a probability associated with it. That probability was attributed to the corresponding load path.

The results of this analysis showed that the probabilities of each path tend to become steady by the year 2006, by which time most major capital will have been committed and spent. Those probabilities were chosen and are:

<u>Load Forecast</u>	<u>Probability</u>
Upper	17%
Branch Upper	20%
Median	26%
Branch Lower	20%
Lower	17%
Overall	100%

Other methods and subjective considerations may yield different measures of likelihood. Consequently, sensitivity to changes in the probabilities chosen were evaluated to check for possible impact on the ranking of Cases based on the load forecast paths alone. The results in Figure 8.5-2 show no impact on cost preference among Cases when likelihood of load forecasts is modified.

FIGURE 8.5-2

PLAN COSTS BASED ON LOAD PATH ONLY
(Millions of 1989\$, Present Value)

	<u>Case 23</u>	<u>Case 22</u>	<u>Case 15</u>	<u>Case 24</u>	<u>Case 26</u>
Load Path					
Upper	86428	85431	85264	85485	86477
Branch Upper	80294	78784	78464	78719	79758
Median	76330	74507	73991	74199	74823
Branch Lower	72912	70549	70118	70211	70395
Lower	65686	63846	63532	63549	63719

EXPECTED COST DIFFERENCES RELATIVE TO CASE 15
USING LOAD FORECAST PROBABILITIES
(Millions of 1989\$, Present Value)

<u>LOAD</u>	<u>PROB</u>	<u>CASE 23</u>	<u>CASE 22</u>	<u>CASE 15</u>	<u>CASE 24</u>	<u>CASE 26</u>
Upper	17%	198	28	BASE	38	206
Branch Upper	20%	366	64	BASE	51	259
Median	26%	608	134	BASE	54	216
Branch Lower	20%	559	86	BASE	19	55
Lower	17%	366	53	BASE	3	32
Expected Cost Differences		<u>2097</u>	<u>366</u>	<u>BASE</u>	<u>164</u>	<u>769</u>

DIFFERENCES WITH EQUAL PROBABILITY FOR LOAD PATHS
(Millions of 1989\$, Present Value)

<u>LOAD</u>	<u>PROB</u>	<u>CASE 23</u>	<u>CASE 22</u>	<u>CASE 15</u>	<u>CASE 24</u>	<u>CASE 26</u>
Upper	20%	233	33	BASE	44	243
Branch Upper	20%	366	64	BASE	51	259
Median	20%	468	103	BASE	42	166
Branch Lower	20%	559	86	BASE	19	55
Lower	20%	431	63	BASE	3	37
Expected Cost Differences		<u>2056</u>	<u>350</u>	<u>BASE</u>	<u>159</u>	<u>761</u>

8.5.3 Probabilities For The High, Median and Low Cost Estimates

Since there is no detailed probability distribution for each cost component, an approximation is necessary based on the lower, medium and upper estimates. This was obtained by connecting the estimates from the ONCI, TCR, and the prediction ranges in the Sept 1988 Economic Outlook.

As shown in Figure 8.5-3, the lower, median and upper estimates correspond to the 10%, 50% and 90% points along the cumulative probability distribution. In order to complete the probability distributions, the following assumption were made:

- (1) the 10% estimate is representative of the 0-20% region of the cumulative probability distribution curve;
- (2) the 90% estimate is representative of the 80-100% region of the curve; and
- (3) the 50% estimate is representative of the remainder of the curve:

Thus, the three probabilities associated with the three available estimates are as follows:

<u>Estimate</u>	<u>Probability</u>
Upper	20%
Median	60%
Lower	20%

Probabilities Assigned To
Low, Median and Upper Estimates
Representing Cost Band

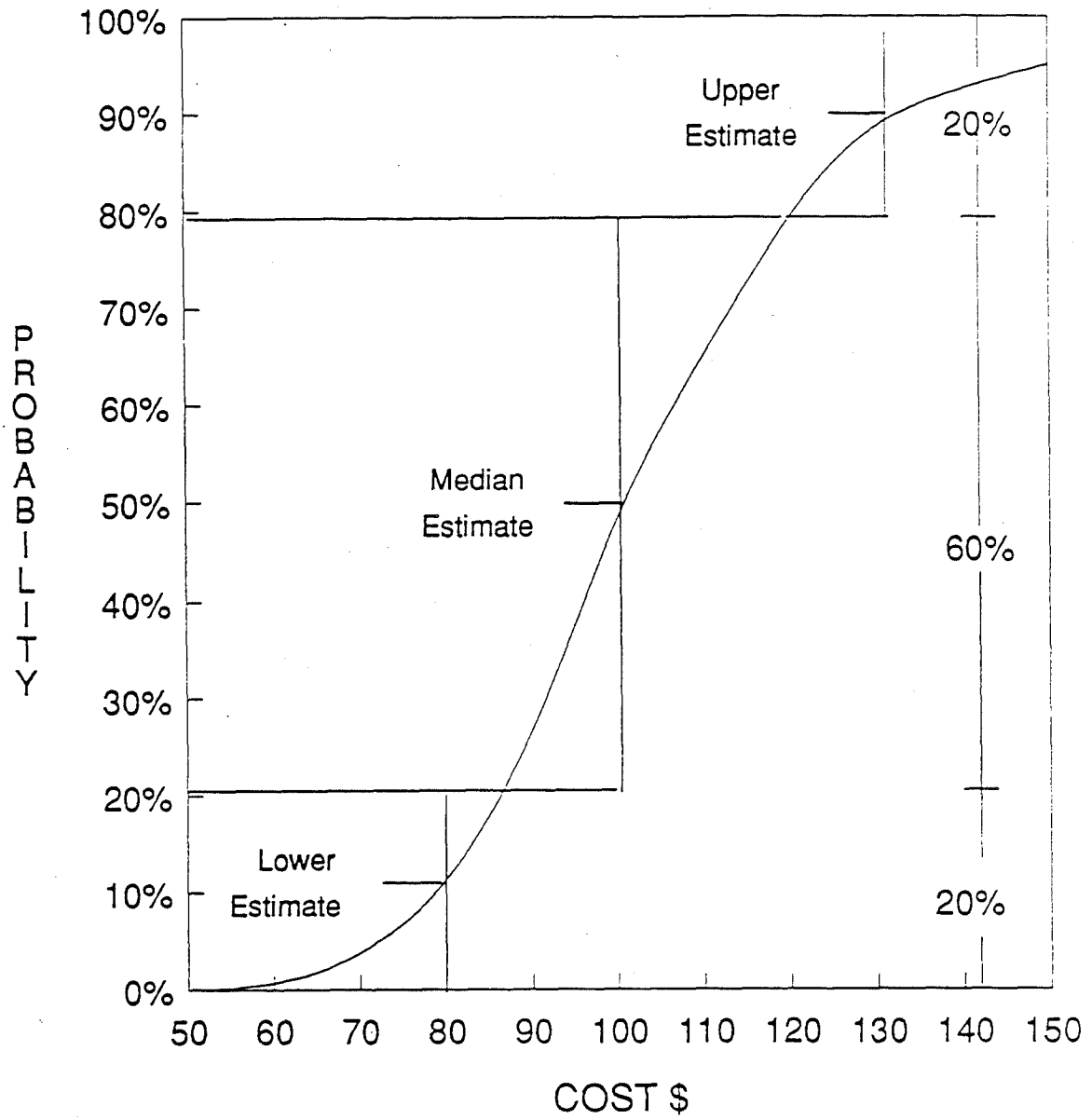


FIGURE 8.5-3

8.5.4 Combining the Cost Estimates and Their Probabilities

Combining the three cost estimates for the key cost components with the five possible load forecasts results in 405 ($5 * 3 * 3 * 3 * 3 = 405$) different possible combinations of estimates, resulting in an equal number of present value cost outcomes. Figure 8.5-4 illustrates how the 405 outcomes could occur. Since each component is considered independent, the path from the Load to the Capital Cost estimate could take any of the five possibilities. Similarly the path from cost component to cost component can take any of the three possibilities, resulting in the 405 possible paths.

If Case 15 is run through two different paths, as shown in Figure 8.5-5, the final expected present value costs would be different, unless by some small chance, different cost estimates resulted in exactly the same final costs.

The chance of any outcome occurring is the product of the probabilities for each path. For example, following are the probabilities associated with the path that begins with upper load forecast in Figure 8.5-5.

Probability (upper load)	= 17%
Probability (high capital cost)	= 20%
Probability (median nuclear fuel cost)	= 60%
Probability (low fossil fuel cost)	= 20%
Probability (high discount rate)	= 20%

$$\text{Cumulative Probability} = .17 * .20 * .60 * .20 * .20 = .000816 = .0816\%$$

Load and Cost Estimate Probabilities And Their Possible Outcomes

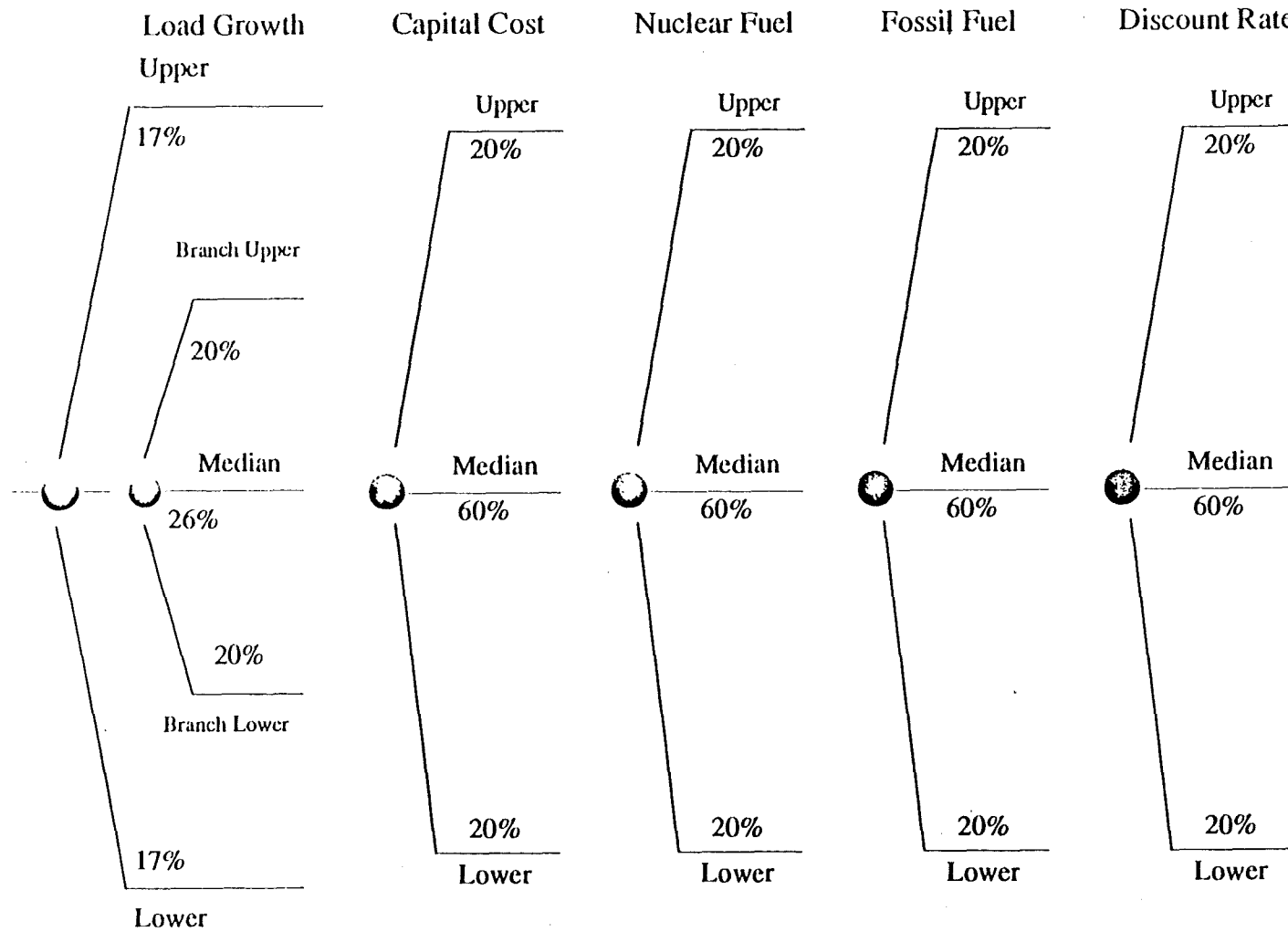


FIGURE 8.5-4

4
0
5
P
A
T
H
S



8.5.5 Expected Cost Results

While a path may have only a small probability, its final costs may be significantly different than the median cost. Therefore, every path in the tree is important. Figure 8.5-6 through Figure 8.5-10 shows the complete expansion of Case 15s 405 paths. At each end point is the present value cost of the RAM when the conditions on the path are modelled.

The 405 outcomes are used to determine the expected cost of the case. This is done by multiplying each outcome by the corresponding probability and then adding the results. Both the expected cost and full range of costs are considered in the evaluation of cases. Figure 8.5-11 indicates the expected values for all five cases for all five load paths. Differences from Case 15s expected cost shows its cost effectiveness under all load forecast paths. Making the load forecast probabilities equal shows no significant change in the expected cost differences.

FIGURE 8.5-6

TREE PATHS FOR UPPER LOAD FORECAST

PATH #	LOAD	CAPCOST	NUCFUEL	FOSSFUEL	DISCRATE	ENDPOINT PROBABILITY	CASE 15 EXPECTED	
							ENDPOINT '89\$M PV	ENDPOINT (SM PV)
1					----- HIGH	0.0272%	83335	23
2				---- HIGH --	---- MEDIAN	0.0816%	91005	74
3					----- LOW	0.0272%	103368	28
4					----- HIGH	0.0816%	81934	67
5			---- HIGH --	---- MEDIAN -	---- MEDIAN	0.2448%	89443	219
6					----- LOW	0.0816%	101549	83
7					----- HIGH	0.0272%	80764	22
8				----- LOW -	---- MEDIAN	0.0816%	88137	72
9					----- LOW	0.0272%	100024	27
10					----- HIGH	0.0816%	82449	67
11				---- HIGH --	---- MEDIAN	0.2448%	90006	220
12					----- LOW	0.0816%	102190	83
13					----- HIGH	0.2448%	81048	198
14		---- HIGH --	---- MEDIAN -	---- MEDIAN -	---- MEDIAN	0.7344%	88445	650
15					----- LOW	0.2448%	100371	246
16					----- HIGH	0.0816%	79878	65
17				----- LOW -	---- MEDIAN	0.2448%	87138	213
18					----- LOW	0.0816%	98846	81
19					----- HIGH	0.0272%	81901	22
20				---- HIGH --	---- MEDIAN	0.0816%	89386	73
21					----- LOW	0.0272%	101453	28
22					----- HIGH	0.0816%	80501	66
23			----- LOW -	---- MEDIAN -	---- MEDIAN	0.2448%	87824	215
24					----- LOW	0.0816%	99634	81
25					----- HIGH	0.0272%	79330	22
26				----- LOW -	---- MEDIAN	0.0816%	86517	71
27					----- LOW	0.0272%	98110	27
28					----- HIGH	0.0816%	80455	66
29				---- HIGH --	---- MEDIAN	0.2448%	87824	215
30					----- LOW	0.0816%	99677	81
31					----- HIGH	0.2448%	79054	194
32			---- HIGH --	---- MEDIAN -	---- MEDIAN	0.7344%	86262	634
33					----- LOW	0.2448%	97858	240
34					----- HIGH	0.0816%	77884	64
35				----- LOW -	---- MEDIAN	0.2448%	84956	208
36					----- LOW	0.0816%	96333	79
37					----- HIGH	0.2448%	79569	195
38				---- HIGH --	---- MEDIAN	0.7344%	86825	638
39					----- LOW	0.2448%	98499	241
40					----- HIGH	0.7344%	78168	574
41	UPPER -	---- MEDIAN -	---- MEDIAN -	---- MEDIAN -	---- MEDIAN	2.2032%	85264	1879
42					----- LOW	0.7344%	96680	710
43					----- HIGH	0.2448%	76998	188
44				----- LOW -	---- MEDIAN	0.7344%	83957	617
45					----- LOW	0.2448%	95155	233
46					----- HIGH	0.0816%	79021	64
47				---- HIGH --	---- MEDIAN	0.2448%	86204	211
48					----- LOW	0.0816%	97762	80
49					----- HIGH	0.2448%	77621	190
50			----- LOW -	---- MEDIAN -	---- MEDIAN	0.7344%	84643	622
51					----- LOW	0.2448%	95943	235
52					----- HIGH	0.0816%	76450	62
53				----- LOW -	---- MEDIAN	0.2448%	83336	204
54					----- LOW	0.0816%	94419	77
55					----- HIGH	0.0272%	78637	21
56				---- HIGH --	---- MEDIAN	0.0816%	85830	70
57					----- LOW	0.0272%	97384	26
58					----- HIGH	0.0816%	77237	63
59			---- HIGH --	---- MEDIAN -	---- MEDIAN	0.2448%	84269	206
60					----- LOW	0.0816%	95565	78
61					----- HIGH	0.0272%	76067	21
62				----- LOW -	---- MEDIAN	0.0816%	82962	68
63					----- LOW	0.0272%	94040	26
64					----- HIGH	0.0816%	77752	63
65				---- HIGH --	---- MEDIAN	0.2448%	84832	208
66					----- LOW	0.0816%	96206	79
67					----- HIGH	0.2448%	76351	187
68		----- LOW -	---- MEDIAN -	---- MEDIAN -	---- MEDIAN	0.7344%	83270	612
69					----- LOW	0.2448%	94387	231
70					----- HIGH	0.0816%	75181	61
71				----- LOW -	---- MEDIAN	0.2448%	81964	201
72					----- LOW	0.0816%	92862	76
73					----- HIGH	0.0272%	77204	21
74				---- HIGH --	---- MEDIAN	0.0816%	84211	69
75					----- LOW	0.0272%	95469	26
76					----- HIGH	0.0816%	75803	62
77			----- LOW -	---- MEDIAN -	---- MEDIAN	0.2448%	82649	202
78					----- LOW	0.0816%	93650	76
79					----- HIGH	0.0272%	74633	20
80				----- LOW -	---- MEDIAN	0.0816%	81343	66
81					----- LOW	0.0272%	92125	25

FIGURE 8.5-7

TREE PATHS FOR BRANCH UPPER LOAD FORECAST

TREE PATHS FOR BRANCH UPPER LOAD FORECAST							CASE 15	EXPECTED
PATH #	LOAD	CAPCOST	NUCFUEL	FOSSFUEL	DISCRATE	ENDPOINT PROBABILITY	ENDPOINT '89\$M PV	ENDPOINT (5M PV)
82					----- HIGH	* 0.0320%	75974	24
83				--- HIGH --	--- MEDIAN	* 0.0960%	83198	80
84					----- LOW	* 0.0320%	94820	30
85					----- HIGH	* 0.0960%	74932	72
86			--- HIGH --	--- MEDIAN -	--- MEDIAN	* 0.2880%	82023	236
87					----- LOW	* 0.0960%	93436	90
88					----- HIGH	* 0.0320%	74127	24
89				--- LOW -	--- MEDIAN	* 0.0960%	81114	78
90					----- LOW	* 0.0320%	92361	30
91					----- HIGH	* 0.0960%	75108	72
92				--- HIGH --	--- MEDIAN	* 0.2880%	82221	237
93					----- LOW	* 0.0960%	93669	90
94					----- HIGH	* 0.2880%	74065	213
95		--- HIGH --	--- MEDIAN -	--- MEDIAN -	--- MEDIAN	* 0.8640%	81047	700
96					----- LOW	* 0.2880%	92285	266
97					----- HIGH	* 0.0960%	73261	70
98				--- LOW -	--- MEDIAN	* 0.2880%	80138	231
99					----- LOW	* 0.0960%	91210	88
100					----- HIGH	* 0.0320%	74573	24
101				--- HIGH --	--- MEDIAN	* 0.0960%	81616	78
102					----- LOW	* 0.0320%	92950	30
103					----- HIGH	* 0.0960%	73530	71
104			--- LOW -	--- MEDIAN -	--- MEDIAN	* 0.2880%	80441	232
105					----- LOW	* 0.0960%	91566	88
106					----- HIGH	* 0.0320%	72726	23
107				--- LOW -	--- MEDIAN	* 0.0960%	79532	76
108					----- LOW	* 0.0320%	90491	29
109					----- HIGH	* 0.0960%	73659	71
110				--- HIGH --	--- MEDIAN	* 0.2880%	80614	232
111					----- LOW	* 0.0960%	91782	88
112					----- HIGH	* 0.2880%	72616	209
113			--- HIGH --	--- MEDIAN -	--- MEDIAN	* 0.8640%	79440	686
114					----- LOW	* 0.2880%	90398	260
115					----- HIGH	* 0.0960%	71812	69
116				--- LOW -	--- MEDIAN	* 0.2880%	78531	226
117					----- LOW	* 0.0960%	89323	86
118					----- HIGH	* 0.2880%	72793	210
119				--- HIGH --	--- MEDIAN	* 0.8640%	79638	688
120					----- LOW	* 0.2880%	90630	261
121					----- HIGH	* 0.8640%	71750	620
122	-BR UPPER	--- MEDIAN -	--- MEDIAN -	--- MEDIAN -	--- MEDIAN	* 2.5920%	78463	2034
123					----- LOW	* 0.8640%	89246	771
124					----- HIGH	* 0.2880%	70945	204
125				--- LOW -	--- MEDIAN	* 0.8640%	77554	670
126					----- LOW	* 0.2880%	88172	254
127					----- HIGH	* 0.0960%	72258	59
128				--- HIGH --	--- MEDIAN	* 0.2880%	79032	228
129					----- LOW	* 0.0960%	89912	86
130					----- HIGH	* 0.2880%	71215	205
131			--- LOW -	--- MEDIAN -	--- MEDIAN	* 0.8640%	77857	673
132					----- LOW	* 0.2880%	88528	255
133					----- HIGH	* 0.0960%	70411	68
134				--- LOW -	--- MEDIAN	* 0.2880%	76949	222
135					----- LOW	* 0.0960%	87453	84
136					----- HIGH	* 0.0320%	72170	23
137				--- HIGH --	--- MEDIAN	* 0.0960%	78969	76
138					----- LOW	* 0.0320%	88872	29
139					----- HIGH	* 0.0960%	71127	68
140			--- HIGH --	--- MEDIAN -	--- MEDIAN	* 0.2880%	77794	224
141					----- LOW	* 0.0960%	88488	85
142					----- HIGH	* 0.0320%	70323	23
143				--- LOW -	--- MEDIAN	* 0.0960%	76885	74
144					----- LOW	* 0.0320%	87413	28
145					----- HIGH	* 0.0960%	71304	58
146				--- HIGH --	--- MEDIAN	* 0.2880%	77992	225
147					----- LOW	* 0.0960%	88720	85
148					----- HIGH	* 0.2880%	70261	202
149		--- LOW -	--- MEDIAN -	--- MEDIAN -	--- MEDIAN	* 0.8640%	76818	664
150					----- LOW	* 0.2880%	87336	252
151					----- HIGH	* 0.0960%	69456	67
152				--- LOW -	--- MEDIAN	* 0.2880%	75909	219
153					----- LOW	* 0.0960%	86262	83
154					----- HIGH	* 0.0320%	70769	23
155				--- HIGH --	--- MEDIAN	* 0.0960%	77386	74
156					----- LOW	* 0.0320%	88002	28
157					----- HIGH	* 0.0960%	69726	67
158			--- LOW -	--- MEDIAN -	--- MEDIAN	* 0.2880%	76212	219
159					----- LOW	* 0.0960%	86618	83
160					----- HIGH	* 0.0320%	68921	22
161				--- LOW -	--- MEDIAN	* 0.0960%	75303	72
162					----- LOW	* 0.0320%	85543	27

FIGURE 8.5-8

TREE PATHS FOR MEDIAN LOAD FORECAST

PATH #	LOAD	CAPCOST	NUCFUEL	FOSSFUEL	DISCRATE	ENDPOINT PROBABILITY	CASE 15 EXPECTED	
							ENDPOINT '89\$M PV	ENDPOINT (5M PV)
163					----- HIGH	0.0416%	71006	30
164				---- HIGH --	----- MEDIAN	0.1248%	77673	97
165					----- LOW	0.0416%	88371	37
166					----- HIGH	0.1248%	70208	88
167			---- HIGH --	--- MEDIAN -	----- MEDIAN	0.3744%	76771	267
168					----- LOW	0.1248%	87306	109
169					----- HIGH	0.0416%	69609	29
170				----- LOW -	----- MEDIAN	0.1248%	76093	95
171					----- LOW	0.0416%	86502	36
172					----- HIGH	0.1248%	70167	88
173				---- HIGH --	----- MEDIAN	0.3744%	76729	267
174					----- LOW	0.1248%	87261	109
175					----- HIGH	0.3744%	69369	260
176		---- HIGH --	--- MEDIAN -	--- MEDIAN -	----- MEDIAN	1.1232%	75828	652
177					----- LOW	0.3744%	86196	323
178					----- HIGH	0.1248%	68770	86
179				----- LOW -	----- MEDIAN	0.3744%	75149	261
180					----- LOW	0.1248%	85392	107
181					----- HIGH	0.0416%	69651	29
182				---- HIGH --	----- MEDIAN	0.1248%	76145	95
183					----- LOW	0.0416%	86570	36
184					----- HIGH	0.1248%	68852	86
185			----- LOW -	--- MEDIAN -	----- MEDIAN	0.3744%	75244	262
186					----- LOW	0.1248%	85505	107
187					----- HIGH	0.0416%	68253	28
188				----- LOW -	----- MEDIAN	0.1248%	74565	93
189					----- LOW	0.0416%	84701	35
190					----- HIGH	0.1248%	69360	87
191				---- HIGH --	----- MEDIAN	0.3744%	75836	284
192					----- LOW	0.1248%	86212	108
193					----- HIGH	0.3744%	68562	257
194			---- HIGH --	--- MEDIAN -	----- MEDIAN	1.1232%	74934	842
195					----- LOW	0.3744%	85147	319
196					----- HIGH	0.1248%	67963	85
197				----- LOW -	----- MEDIAN	0.3744%	74256	278
198					----- LOW	0.1248%	84343	105
199					----- HIGH	0.3744%	68521	257
200				---- HIGH --	----- MEDIAN	1.1232%	74892	841
201					----- LOW	0.3744%	85102	319
202					----- HIGH	1.1232%	67723	761
203	--- MEDIAN -	--- MEDIAN -	--- MEDIAN -	--- MEDIAN -	----- MEDIAN	3.3696%	73991	2493
204					----- LOW	1.1232%	84037	944
205					----- HIGH	0.3744%	67124	251
206				----- LOW -	----- MEDIAN	1.1232%	73313	823
207					----- LOW	0.3744%	83233	312
208					----- HIGH	0.1248%	68005	85
209				---- HIGH --	----- MEDIAN	0.3744%	74308	278
210					----- LOW	0.1248%	84411	105
211					----- HIGH	0.3744%	67206	252
212			----- LOW -	--- MEDIAN -	----- MEDIAN	1.1232%	73407	825
213					----- LOW	0.3744%	83346	312
214					----- HIGH	0.1248%	66608	83
215				----- LOW -	----- MEDIAN	0.3744%	72729	272
216					----- LOW	0.1248%	82542	103
217					----- HIGH	0.0416%	68277	28
218				---- HIGH --	----- MEDIAN	0.1248%	74641	93
219					----- LOW	0.0416%	84829	35
220					----- HIGH	0.1248%	67478	84
221			---- HIGH --	--- MEDIAN -	----- MEDIAN	0.3744%	73739	276
222					----- LOW	0.1248%	83765	105
223					----- HIGH	0.0416%	66879	28
224				----- LOW -	----- MEDIAN	0.1248%	73061	91
225					----- LOW	0.0416%	82960	35
226					----- HIGH	0.1248%	67438	84
227				---- HIGH --	----- MEDIAN	0.3744%	73697	276
228					----- LOW	0.1248%	83719	104
229					----- HIGH	0.3744%	66639	249
230	----- LOW -	--- MEDIAN -	--- MEDIAN -	--- MEDIAN -	----- MEDIAN	1.1232%	72796	818
231					----- LOW	0.3744%	82655	309
232					----- HIGH	0.1248%	66040	82
233				----- LOW -	----- MEDIAN	0.3744%	72118	270
234					----- LOW	0.1248%	81850	102
235					----- HIGH	0.0416%	66921	28
236				---- HIGH --	----- MEDIAN	0.1248%	73113	91
237					----- LOW	0.0416%	83028	35
238					----- HIGH	0.1248%	66123	83
239			----- LOW -	--- MEDIAN -	----- MEDIAN	0.3744%	72212	270
240					----- LOW	0.1248%	81964	102
241					----- HIGH	0.0416%	65524	27
242				----- LOW -	----- MEDIAN	0.1248%	71534	89
243					----- LOW	0.0416%	81159	34

FIGURE 8.5-9

TREE PATHS FOR BRANCH LOWER LOAD FORECAST

TREE PATHS FOR BRANCH LOWER LOAD FORECAST						CASE 15	EXPECTED	
PATH #	LOAD	CAPCOST	NUCFUEL	FOSSFUEL	DISCRATE	ENDPOINT PROBABILITY	ENDPOINT 1995M PV	ENDPOINT (5M PV)
244					----- HIGH	0.0320%	66901	21
245				---- HIGH --	----- MEDIAN	0.0960%	73037	70
246					----- LOW	0.0320%	82875	27
247					----- HIGH	0.0960%	66374	64
248			---- HIGH --	--- MEDIAN -	----- MEDIAN	0.2880%	72444	209
249					----- LOW	0.0960%	82177	79
250					----- HIGH	0.0320%	65977	21
251				----- LOW -	----- MEDIAN	0.0960%	71996	69
252					----- LOW	0.0320%	81649	26
253					----- HIGH	0.0960%	66084	63
254				---- HIGH --	----- MEDIAN	0.2880%	72120	208
255					----- LOW	0.0960%	81798	79
256					----- HIGH	0.2880%	65557	189
257		---- HIGH --	--- MEDIAN -	--- MEDIAN -	----- MEDIAN	0.8640%	71526	618
258					----- LOW	0.2880%	81099	234
259					----- HIGH	0.0960%	65161	63
260				----- LOW -	----- MEDIAN	0.2880%	71079	205
261					----- LOW	0.0960%	80571	77
262					----- HIGH	0.0320%	65582	21
263				---- HIGH --	----- MEDIAN	0.0960%	71553	69
264					----- LOW	0.0320%	81128	26
265					----- HIGH	0.0960%	65055	62
266			----- LOW -	--- MEDIAN -	----- MEDIAN	0.2880%	70959	204
267					----- LOW	0.0960%	80429	77
268					----- HIGH	0.0320%	64658	21
269				----- LOW -	----- MEDIAN	0.0960%	70512	68
270					----- LOW	0.0320%	79901	26
271					----- HIGH	0.0960%	65639	63
272				---- HIGH --	----- MEDIAN	0.2880%	71629	206
273					----- LOW	0.0960%	81222	78
274					----- HIGH	0.2880%	65112	188
275			---- HIGH --	--- MEDIAN -	----- MEDIAN	0.8640%	71035	614
276					----- LOW	0.2880%	80523	232
277					----- HIGH	0.0960%	64715	62
278				----- LOW -	----- MEDIAN	0.2880%	70588	203
279					----- LOW	0.0960%	79995	77
280					----- HIGH	0.2880%	64822	187
281				---- HIGH --	----- MEDIAN	0.8640%	70711	611
282					----- LOW	0.2880%	80144	231
283					----- HIGH	0.8640%	64295	556
284	-BR LOWER	--- MEDIAN -	--- MEDIAN -	--- MEDIAN -	----- MEDIAN	2.5920%	70118	1817
285					----- LOW	0.8640%	79446	686
286					----- HIGH	0.2880%	63899	184
287				----- LOW -	----- MEDIAN	0.8640%	69670	602
288					----- LOW	0.2880%	78917	227
289					----- HIGH	0.0960%	64320	62
290				---- HIGH --	----- MEDIAN	0.2880%	70144	202
291					----- LOW	0.0960%	79474	76
292					----- HIGH	0.2880%	63793	184
293			----- LOW -	--- MEDIAN -	----- MEDIAN	0.8640%	69551	601
294					----- LOW	0.2880%	78776	227
295					----- HIGH	0.0960%	63396	61
296				----- LOW -	----- MEDIAN	0.2880%	69103	199
297					----- LOW	0.0960%	78247	75
298					----- HIGH	0.0320%	64768	21
299				---- HIGH --	----- MEDIAN	0.0960%	70671	68
300					----- LOW	0.0320%	80118	26
301					----- HIGH	0.0960%	64241	62
302			---- HIGH --	--- MEDIAN -	----- MEDIAN	0.2880%	70077	202
303					----- LOW	0.0960%	79420	76
304					----- HIGH	0.0320%	63845	20
305				----- LOW -	----- MEDIAN	0.0960%	69630	67
306					----- LOW	0.0320%	78891	25
307					----- HIGH	0.0960%	63951	61
308				---- HIGH --	----- MEDIAN	0.2880%	59753	201
309					----- LOW	0.0960%	79040	76
310					----- HIGH	0.2880%	63424	193
311		----- LOW -	--- MEDIAN -	--- MEDIAN -	----- MEDIAN	0.8640%	69160	598
312					----- LOW	0.2880%	78342	226
313					----- HIGH	0.0960%	63028	61
314				----- LOW -	----- MEDIAN	0.2880%	68712	198
315					----- LOW	0.0960%	77913	75
316					----- HIGH	0.0320%	63449	20
317				---- HIGH --	----- MEDIAN	0.0960%	69186	66
318					----- LOW	0.0320%	78370	25
319					----- HIGH	0.0960%	62922	60
320			----- LOW -	--- MEDIAN -	----- MEDIAN	0.2880%	68593	198
321					----- LOW	0.0960%	77672	75
322					----- HIGH	0.0320%	62526	20
323				----- LOW -	----- MEDIAN	0.0960%	68145	65
324					----- LOW	0.0320%	77144	25

FIGURE 8.5-10

TREE PATHS FOR LOWER LOAD FORECAST

PATH #	LOAD	CAPCOST	NUCFUEL	FOSSFUEL	DISCRATE	ENDPOINT PROBABILITY	CASE 15 EXPECTED	
							ENDPOINT '896M PV	ENDPOINT (5M PV)
325					----- HIGH	0.02724	59899	16
326				--- HIGH --	----- MEDIAN	0.08164	65551	53
327					----- LOW	0.02724	74563	20
328					----- HIGH	0.08164	59522	49
329			--- HIGH --	- MEDIAN -	----- MEDIAN	0.24484	65114	159
330					----- LOW	0.08164	74031	60
331					----- HIGH	0.02724	59240	16
332				----- LOW -	----- MEDIAN	0.08164	64786	53
333					----- LOW	0.02724	73630	20
334					----- HIGH	0.08164	59144	46
335				--- HIGH --	----- MEDIAN	0.24484	64704	158
336					----- LOW	0.08164	73569	60
337					----- HIGH	0.24484	58767	144
338		--- HIGH --	- MEDIAN -	- MEDIAN -	----- MEDIAN	0.73444	64266	472
339					----- LOW	0.24484	73037	179
340					----- HIGH	0.08164	58485	46
341				----- LOW -	----- MEDIAN	0.24484	63939	157
342					----- LOW	0.08164	72636	59
343					----- HIGH	0.02724	58683	16
344				--- HIGH --	----- MEDIAN	0.08164	64184	52
345					----- LOW	0.02724	72956	20
346					----- HIGH	0.08164	58306	48
347			----- LOW -	- MEDIAN -	----- MEDIAN	0.24484	63747	156
348					----- LOW	0.08164	72423	59
349					----- HIGH	0.02724	58024	16
350				----- LOW -	----- MEDIAN	0.08164	63419	52
351					----- LOW	0.02724	72023	20
352					----- HIGH	0.08164	59237	48
353				--- HIGH --	----- MEDIAN	0.24484	64817	159
354					----- LOW	0.08164	73710	60
355					----- HIGH	0.24484	58860	144
356			--- HIGH --	- MEDIAN -	----- MEDIAN	0.73444	64379	473
357					----- LOW	0.24484	73177	179
358					----- HIGH	0.08164	58579	48
359				----- LOW -	----- MEDIAN	0.24484	64051	157
360					----- LOW	0.08164	72777	59
361					----- HIGH	0.24484	58482	143
362				--- HIGH --	----- MEDIAN	0.73444	63970	470
363					----- LOW	0.24484	72716	178
364					----- HIGH	0.73444	58105	427
365	- LOWER -	- MEDIAN -	- MEDIAN -	- MEDIAN -	----- MEDIAN	2.20324	63532	1400
366					----- LOW	0.73444	72183	530
367					----- HIGH	0.24484	57824	142
368				----- LOW -	----- MEDIAN	0.73444	63204	464
369					----- LOW	0.24484	71783	176
370					----- HIGH	0.08164	58022	47
371				--- HIGH --	----- MEDIAN	0.24484	63450	155
372					----- LOW	0.08164	72102	59
373					----- HIGH	0.24484	57644	141
374			----- LOW -	- MEDIAN -	----- MEDIAN	0.73444	63013	463
375					----- LOW	0.24484	71570	175
376					----- HIGH	0.08164	57363	47
377				----- LOW -	----- MEDIAN	0.24484	62685	153
378					----- LOW	0.08164	71169	58
379					----- HIGH	0.02724	58788	16
380				--- HIGH --	----- MEDIAN	0.08164	64325	52
381					----- LOW	0.02724	73148	20
382					----- HIGH	0.08164	58411	48
383			--- HIGH --	- MEDIAN -	----- MEDIAN	0.24484	63887	156
384					----- LOW	0.08164	72615	59
385					----- HIGH	0.02724	58129	16
386				----- LOW -	----- MEDIAN	0.08164	63559	52
387					----- LOW	0.02724	72215	20
388					----- HIGH	0.08164	58033	47
389				--- HIGH --	----- MEDIAN	0.24484	63477	155
390					----- LOW	0.08164	72154	59
391					----- HIGH	0.24484	57656	141
392		----- LOW -	- MEDIAN -	- MEDIAN -	----- MEDIAN	0.73444	63040	463
393					----- LOW	0.24484	71621	175
394					----- HIGH	0.08164	57374	47
395				----- LOW -	----- MEDIAN	0.24484	62712	154
396					----- LOW	0.08164	71221	58
397					----- HIGH	0.02724	57572	16
398				--- HIGH --	----- MEDIAN	0.08164	62958	51
399					----- LOW	0.02724	71541	19
400					----- HIGH	0.08164	57195	47
401			----- LOW -	- MEDIAN -	----- MEDIAN	0.24484	62520	153
402					----- LOW	0.08164	71008	58
403					----- HIGH	0.02724	56914	15
404				----- LOW -	----- MEDIAN	0.08164	62192	51
405					----- LOW	0.02724	70608	19

TOTAL TREE EXPECTED COST

100%

75258

FIGURE 8.5-11

CASE COSTS BASED ON ALL PATHS IN TREE
(Millions of 1989\$, Present Value)

<u>Load Path</u>	<u>PROB</u>	<u>Case 23</u>	<u>Case 22</u>	<u>Case 15</u>	<u>Case 24</u>	<u>Case 26</u>
Upper	17%	87675	86667	86497	86747	87842
Branch Upper	20%	81427	79911	79597	79889	81019
Median	26%	77354	75502	74995	75230	75916
Branch Lower	20%	73853	71447	71011	71116	71352
Lower	17%	66504	64632	64315	64335	64527
Expected Cost		<u>77378</u>	<u>75623</u>	<u>75258</u>	<u>75445</u>	<u>76115</u>

EXPECTED COST DIFFERENCES RELATIVE TO CASE 15
USING LOAD FORECAST PROBABILITIES
(Millions of 1989\$, Present Value)

<u>PROB</u>		<u>Case 23</u>	<u>Case 22</u>	<u>Case 15</u>	<u>Case 24</u>	<u>Case 26</u>
Upper	17%	200	29	BASE	43	229
Branch Upper	20%	366	63	BASE	58	284
Median	26%	613	132	BASE	61	239
Branch Lower	20%	568	87	BASE	21	68
Lower	17%	372	54	BASE	4	36
Expected Cost Differences		<u>2120</u>	<u>365</u>	<u>BASE</u>	<u>187</u>	<u>857</u>

DIFFERENCES WITH EQUAL PROBABILITY FOR LOAD PATHS
(Millions of 1989\$, Present Value)

<u>PROB</u>		<u>Case 23</u>	<u>Case 22</u>	<u>Case 15</u>	<u>Case 24</u>	<u>Case 26</u>
Upper	20%	236	34	BASE	50	269
Branch Upper	20%	366	63	BASE	58	284
Median	20%	472	101	BASE	47	184
Branch Lower	20%	568	87	BASE	21	68
Lower	20%	438	64	BASE	4	42
Expected Cost Differences		<u>2080</u>	<u>349</u>	<u>BASE</u>	<u>181</u>	<u>848</u>

8.5.6 Cumulative Probability Distributions Explained

The total cost range for each case, representing all 405 possible outcomes, can be shown in a cumulative probability distribution graph. Cumulative probability distributions represent the probability of each possible outcome, starting from the lowest cost and ending with the highest cost. Cumulative probability distributions are derived by sorting all applicable outcomes of the probability tree and accumulating the probabilities as you move up the sorted outcomes. For example, the top chart in Figure 8.5-12 shows there is a 20% probability of the cost of Case 15 being up to \$67.5 billion.

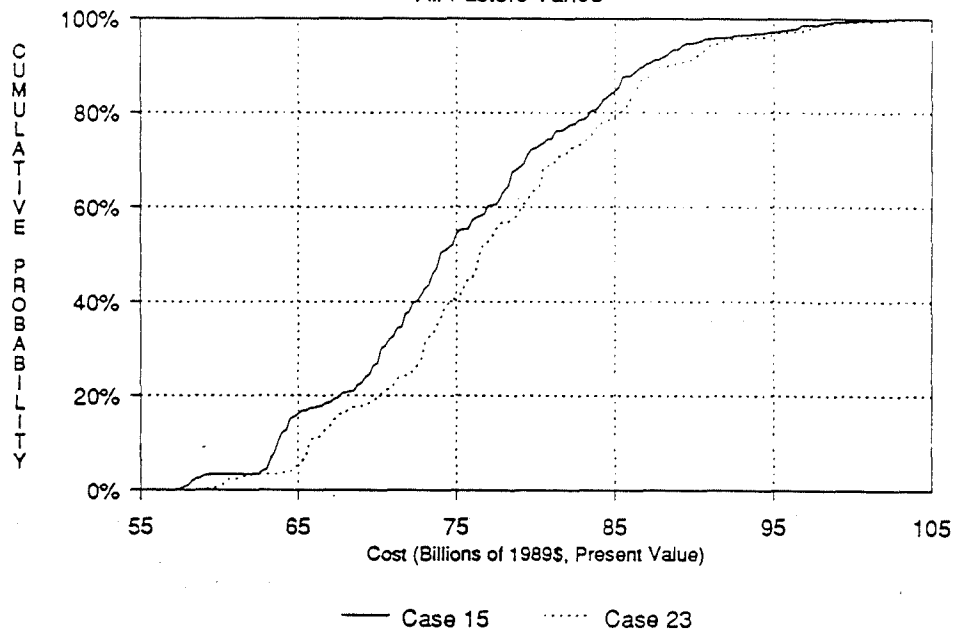
If the distribution of costs for one case is always to the left of the others, then it is considered the leading case, since always has a greater probability of costing less than the other cases.

In evaluating cases it is important to examine the differences between one case, for example Case 15 and all other cases. The bottom chart in Figure 8.5-12 plots the differences between each case and Case 15 for each of the 405 outcomes. These differences relative to Case 15 were taken for each of the 405 outcomes. The differences were then sorted and their associated probabilities were accumulated to produce the cumulative probability distributions. When the distribution line is to the left of 0, it indicates the probability of the case costing less than Case 15; if it is to the right, it indicates the probability of the case costing more than Case 15. The bottom chart in Figure 8.5-12 shows that there is only about 1% probability that Case 23 will cost the same or less than Case 15 when all factors are varied.

Generally, if one case dominates another by having less costly outcomes more frequently, this will be reflected when the case differences are plotted. The cumulative distributions for case costs and differences in costs are the results of different sorting operations. The two charts are also plotted on a different scale, therefore they are not directly comparable.

In addition to varying all factors, the complete probabilistic analysis involved fixing one factor while varying all the others. The three estimates for the four cost factors, Capital Cost, Nuclear Fuel, Fossil Fuel and Discount Rate, were modelled for the 5 load forecast paths producing 17 specific conditions. For example, Figure 8.5-13 shows how two Cases, 15 and 26, respond under the Branch Lower load forecast, while all other factors vary. The top chart shows the dominance of Case 15 over Case 26 while the bottom chart shows there is a 20% probability that Case 26 could be less than or equal to Case 15.

Illustration of Case 15 and Case 23
Probabilistic Cost Distributions
All Factors Varied



All Factors Varied
Cost Differences Relative to Case 15 (Base)

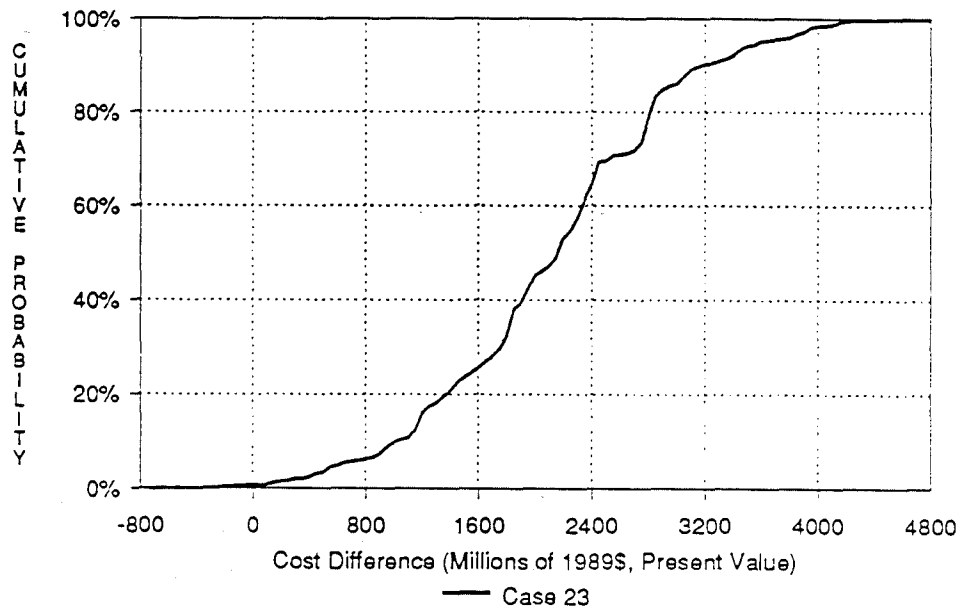


FIGURE 8.5-12

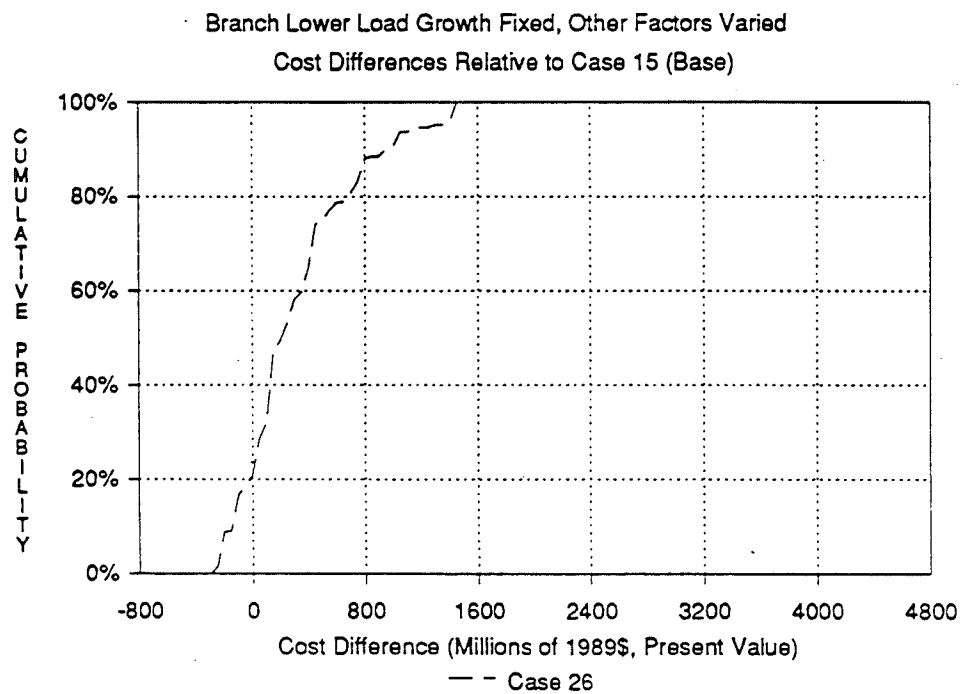
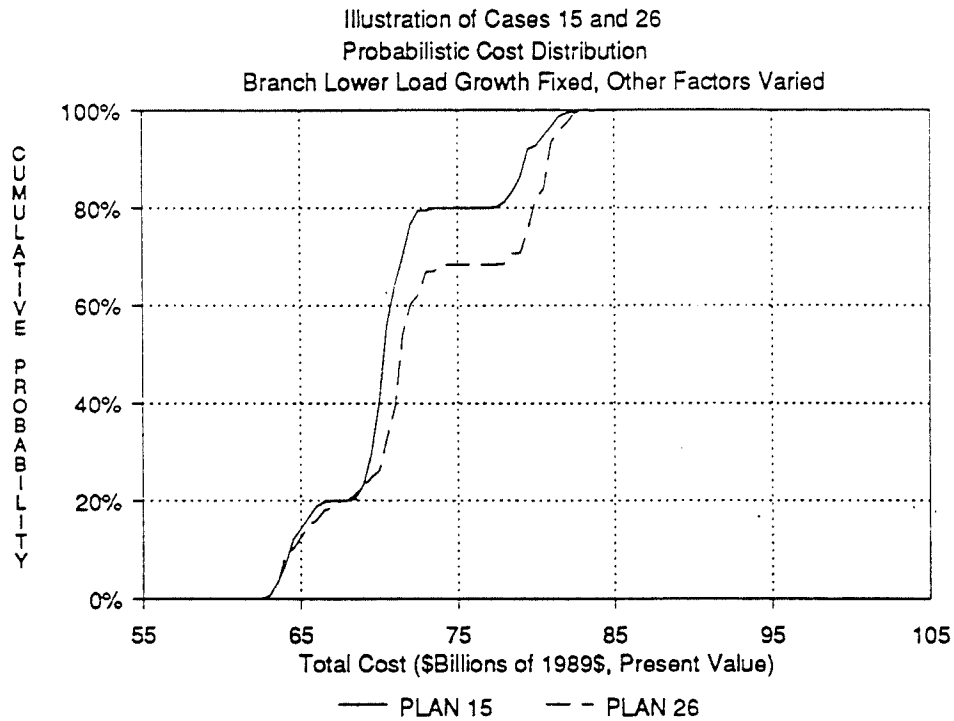


FIGURE 8.5-13

8.5.7 Cumulative Probabilistic Results

Figure 8.5-14 shows the cumulative probability distributions for each case when all five load forecasts and all cost estimates are considered. The top chart shows that Case 15 is the dominant case with lower expected costs. The bottom chart highlights the differences in costs more clearly. It shows the Case 15 only has a 8% probability of costing more than any of the other cases, when all factors are varied.

Figure 8.5-15 through Figure 8.5-31 shows how the cases respond when fixing each of the 17 specific conditions described in the last paragraph of 8.5.6. while varying all the others. Under almost all combinations of conditions, there is less than 20% probability that any case would have lower expected costs than Case 15. These occur under certain combinations of conditions which have a low probability. In addition, as cost conditions become known the actual plan could be adjusted.

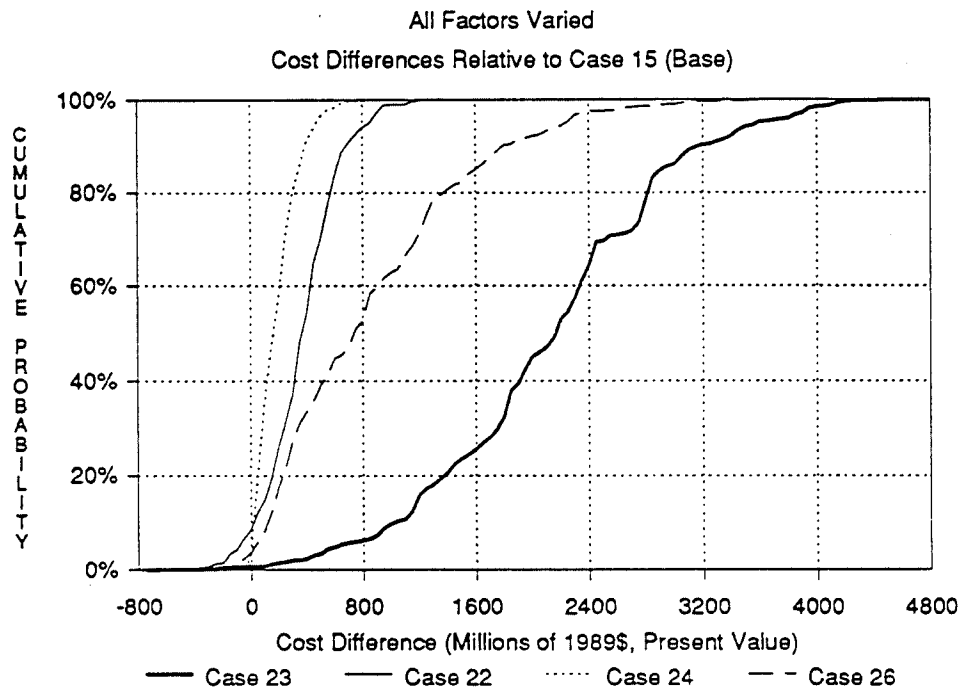
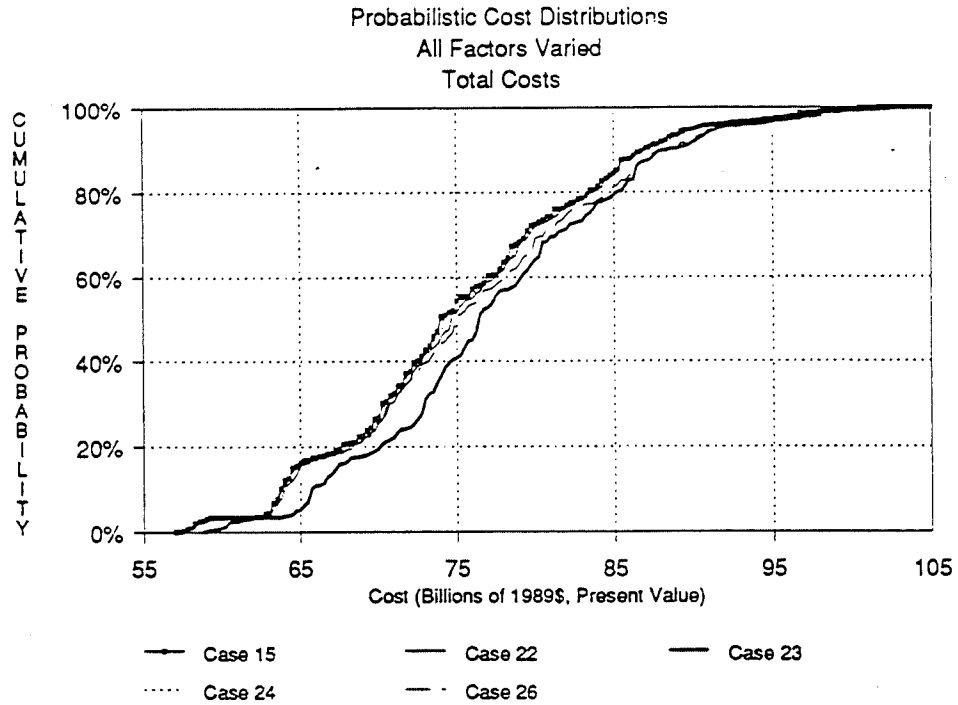
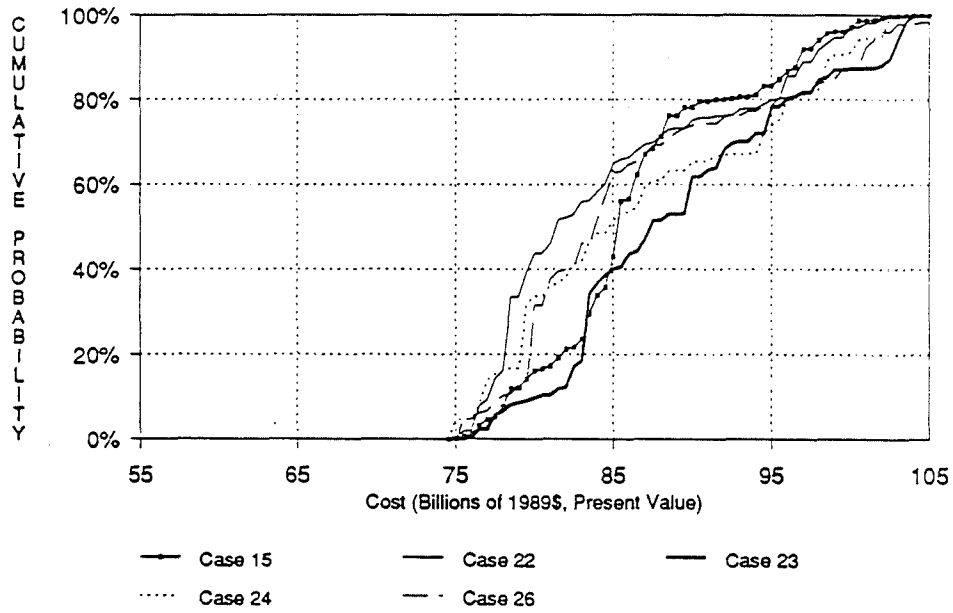


FIGURE 8.5-14

Probabilistic Cost Distributions
Upper Load Growth, Other Factors Varied
Total Costs



Upper Load Growth Fixed, Other Factors Varied
Cost Differences Relative to Case 15 (Base)

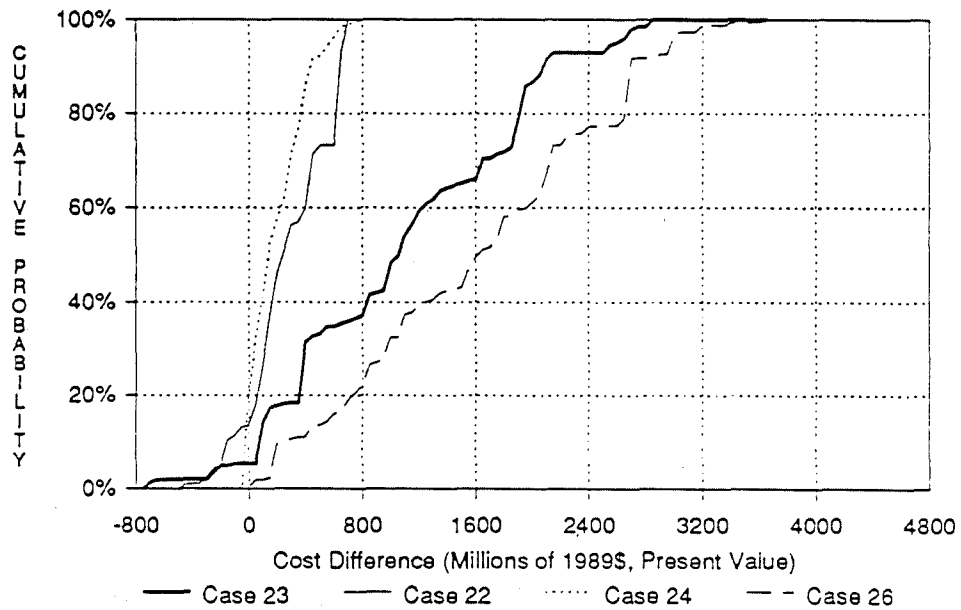


FIGURE 8.5-15

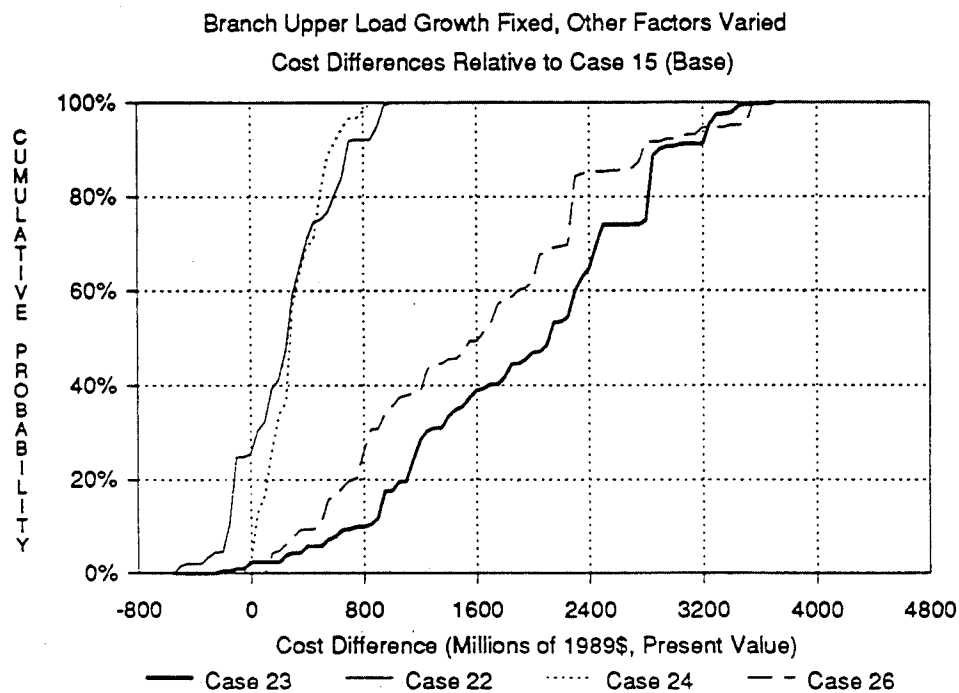
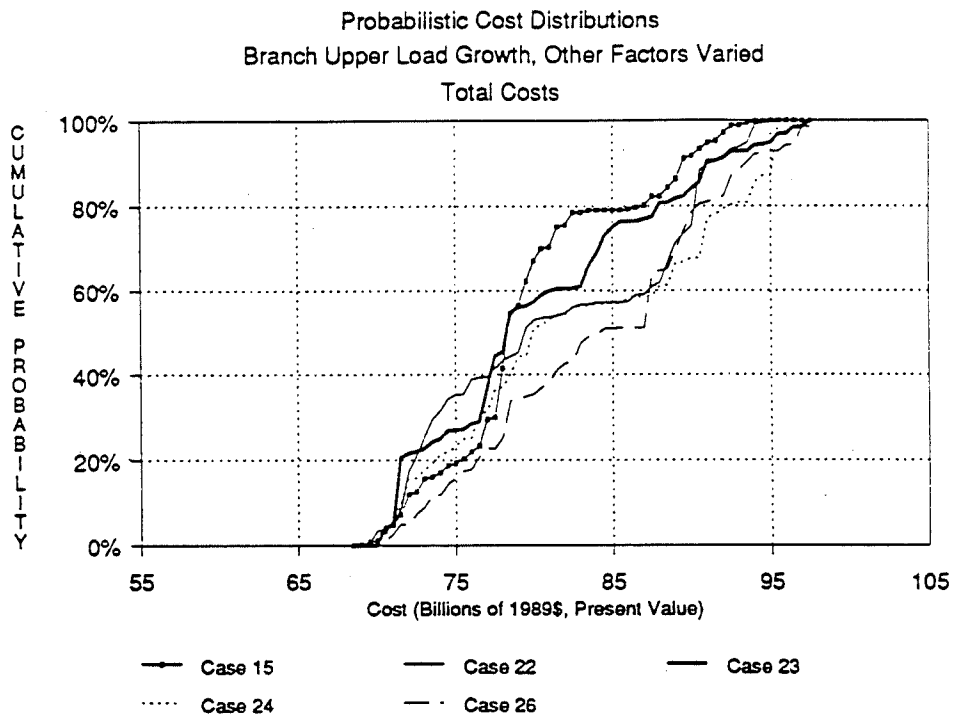


FIGURE 8.5-16

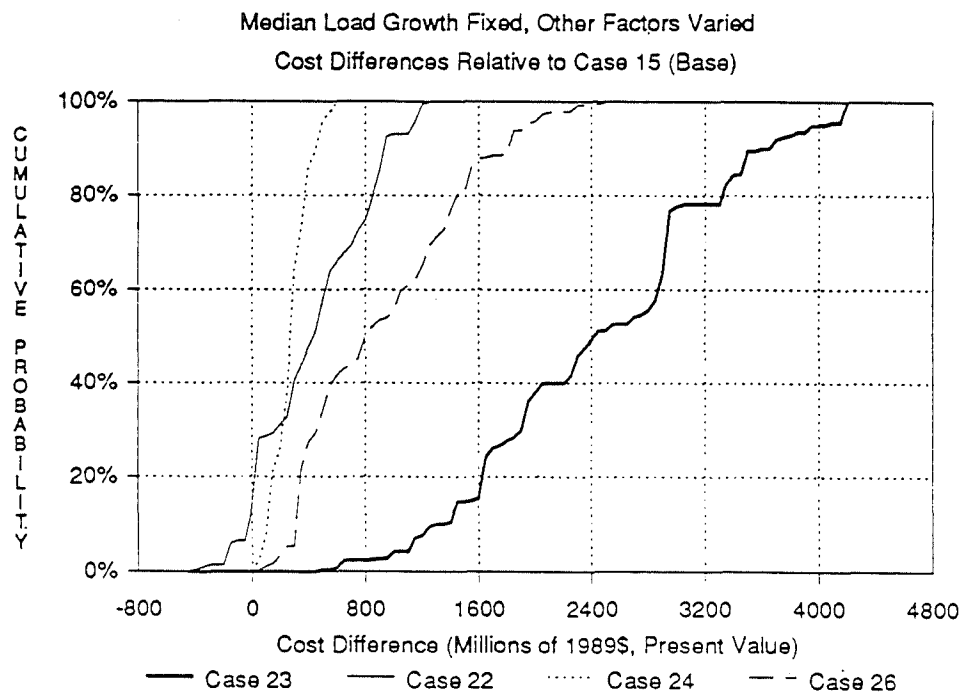
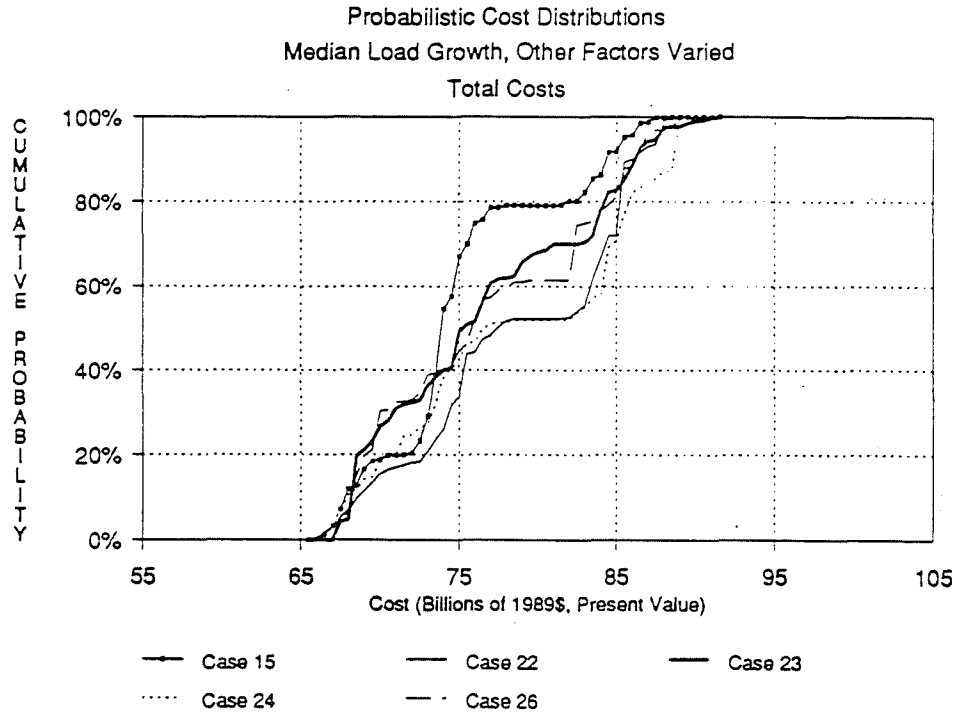
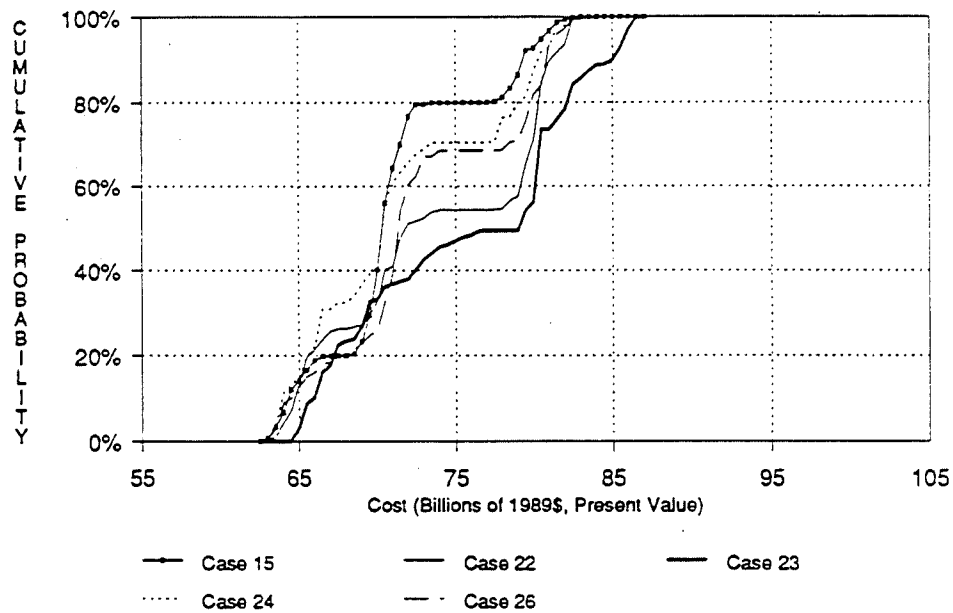


FIGURE 8.5-17

Probabilistic Cost Distributions
Branch Lower Load Growth, Other Factors Varied
Total Costs



Branch Lower Load Growth Fixed, Other Factors Varied
Cost Differences Relative to Case 15 (Base)

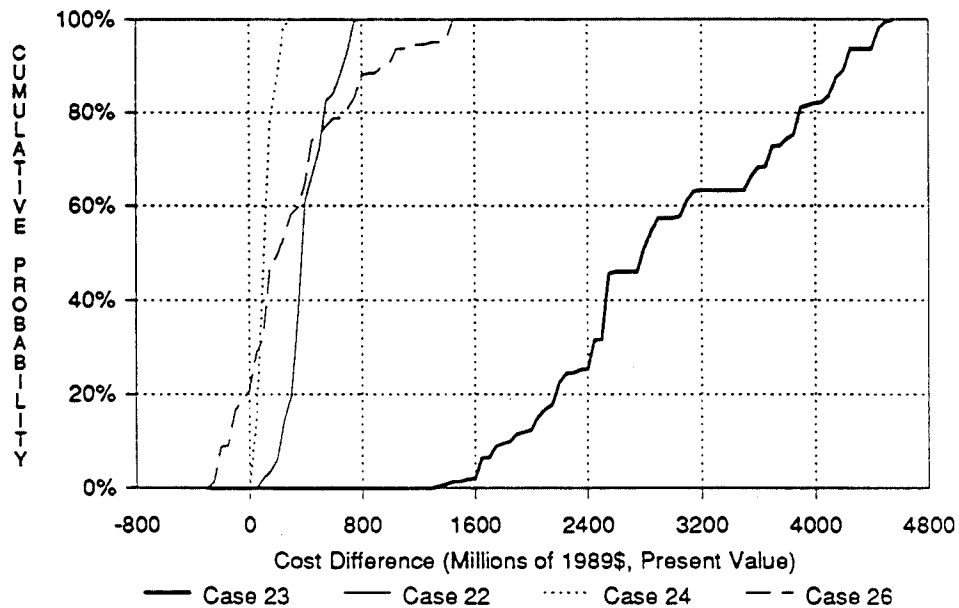


FIGURE 8.5-18

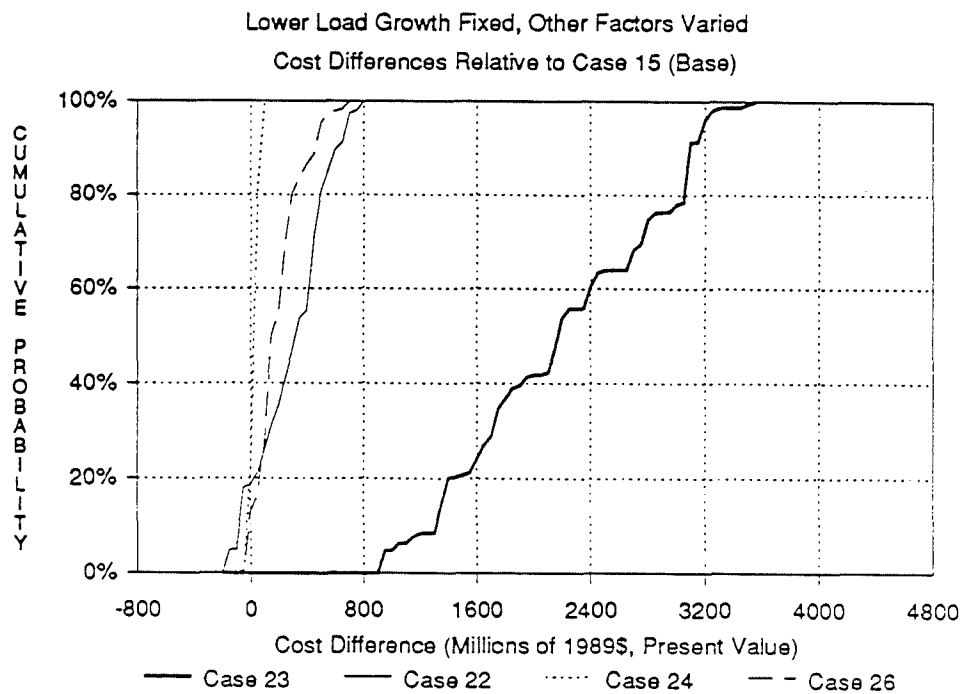
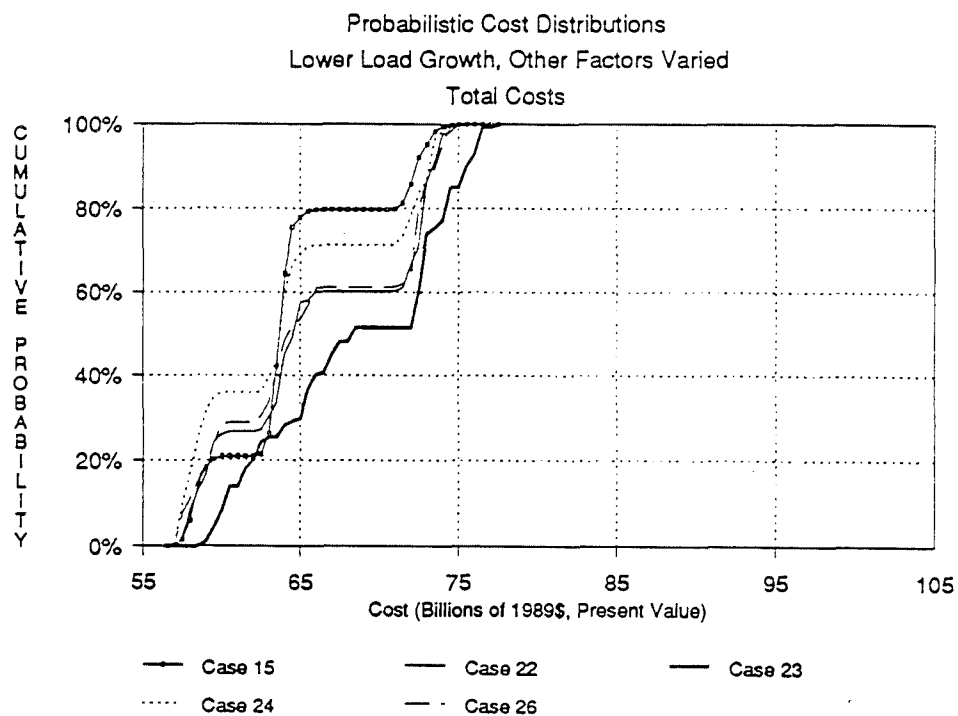


FIGURE 8.5-19

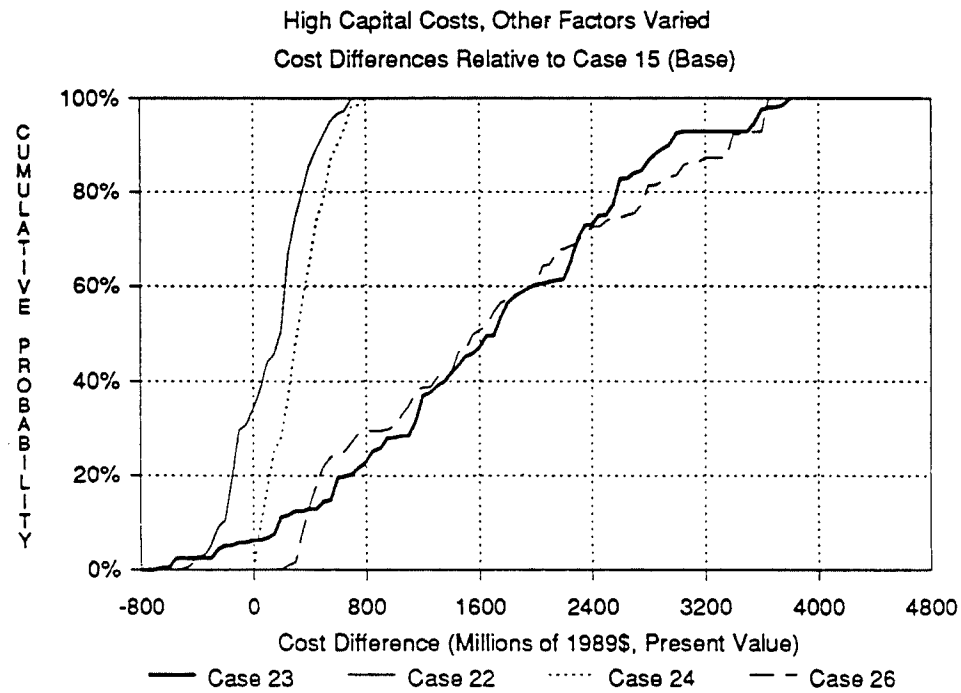
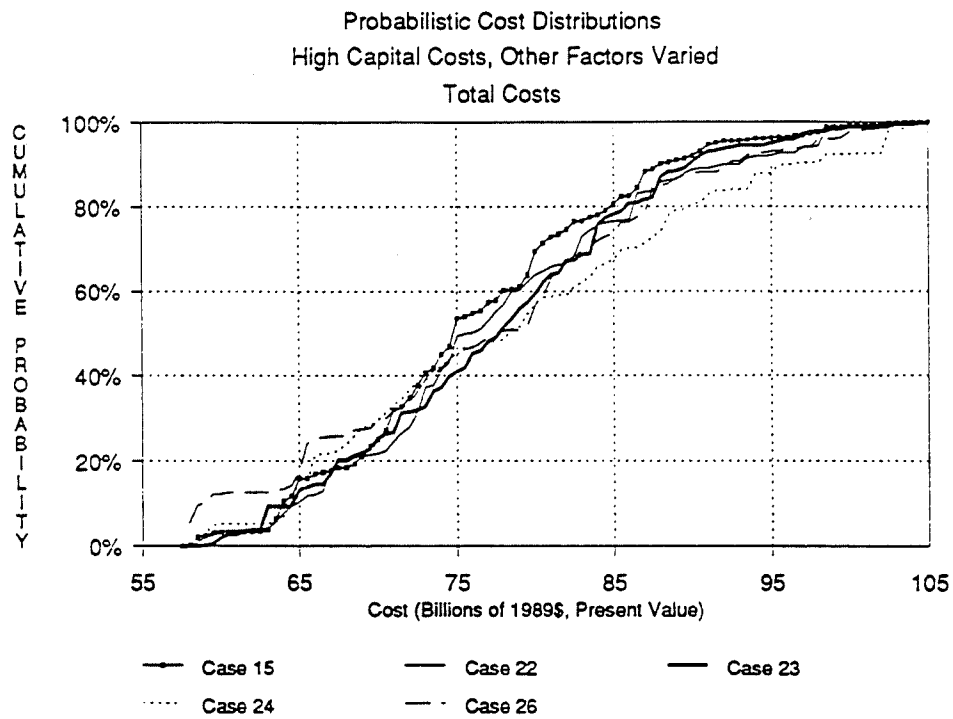


FIGURE 8.5-20

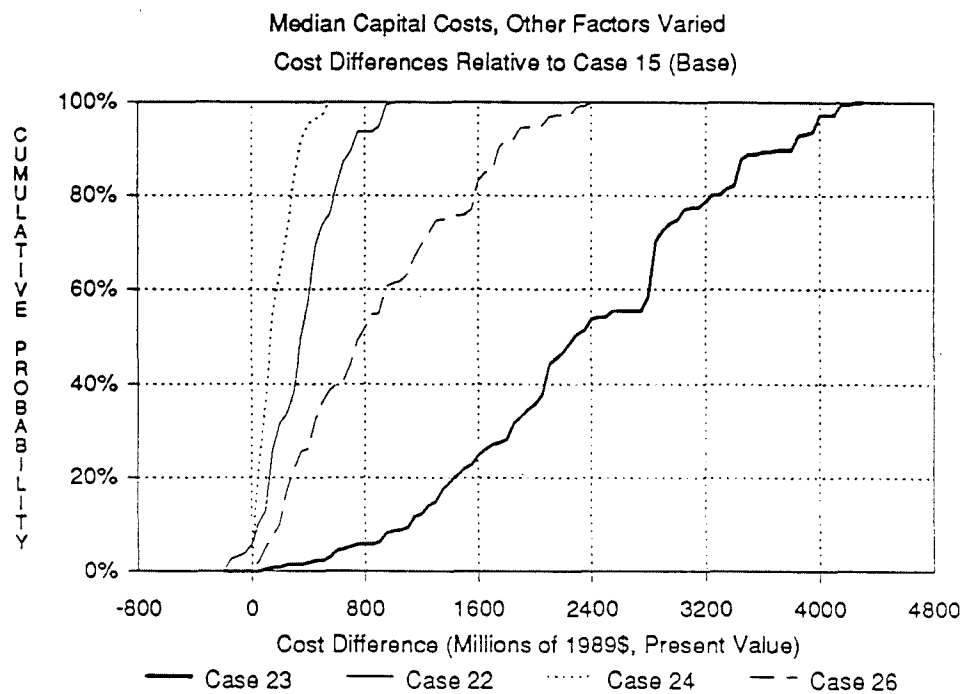
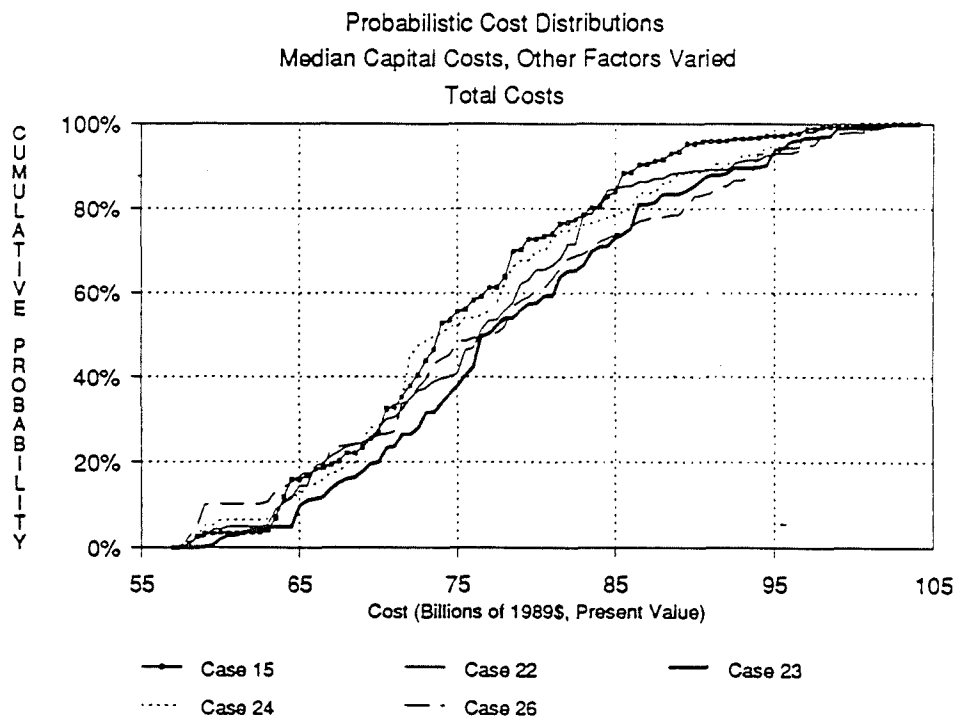
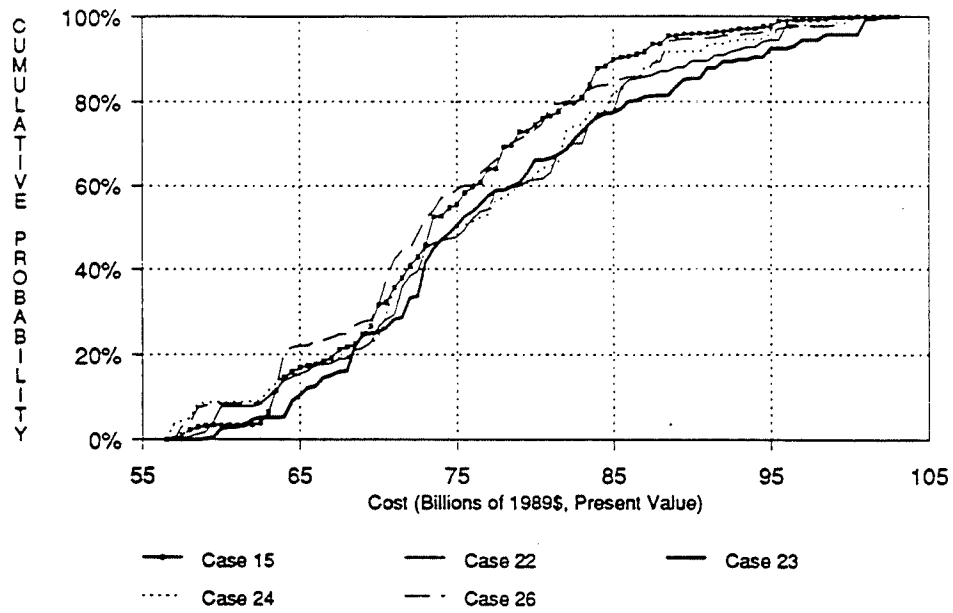


FIGURE 8.5-21

Probabilistic Cost Distributions
Low Capital Costs, Other Factors Varied
Total Costs



Low Capital Costs, Other Factors Varied
Cost Differences Relative to Case 15 (Base)

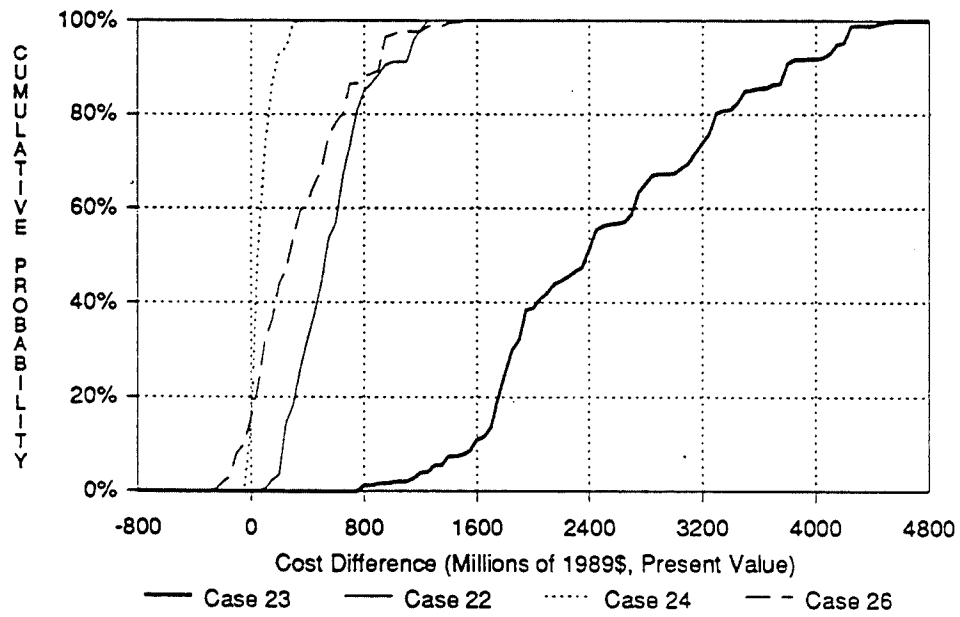


FIGURE 8.5-22

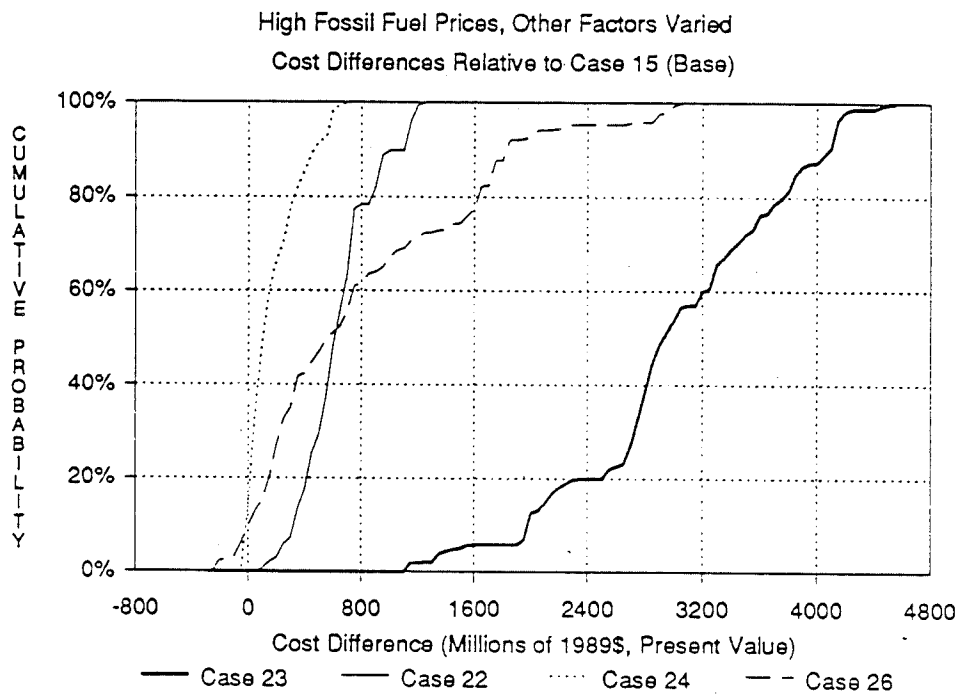
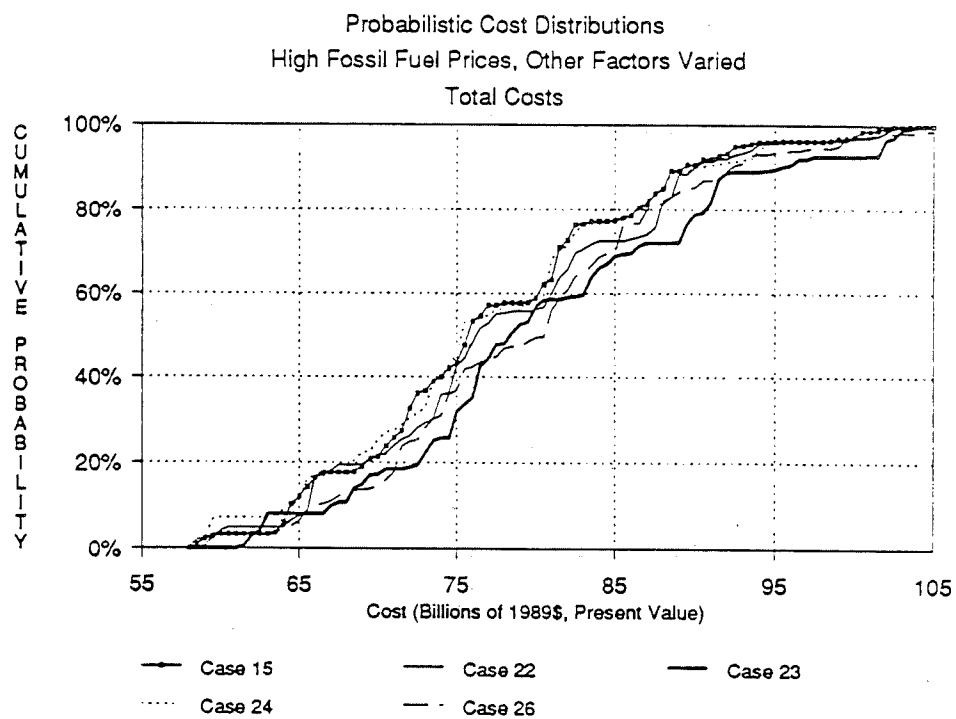


FIGURE 8.5-23

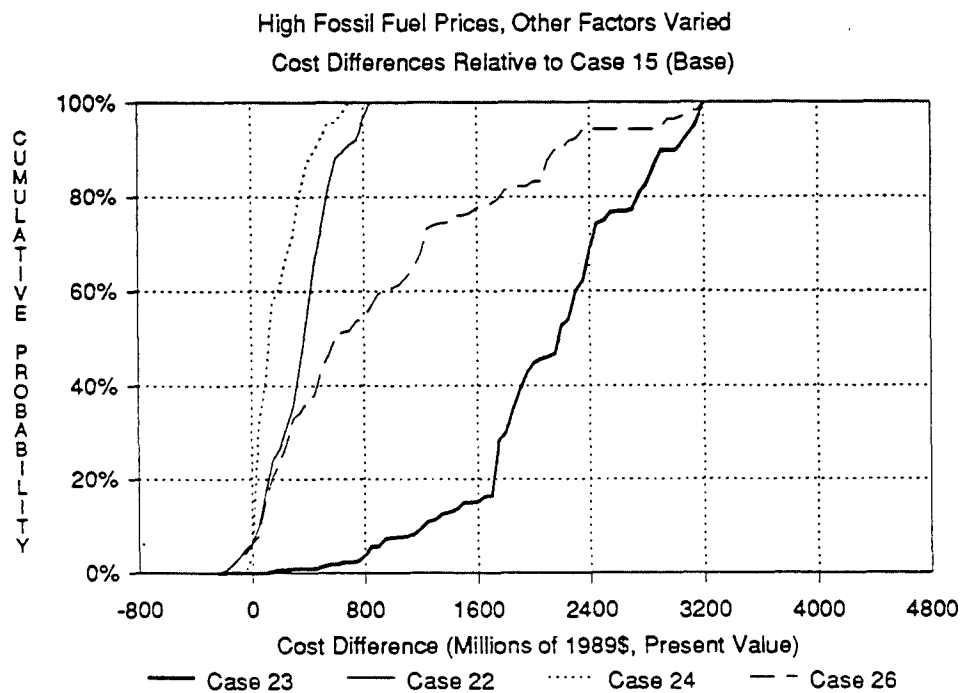
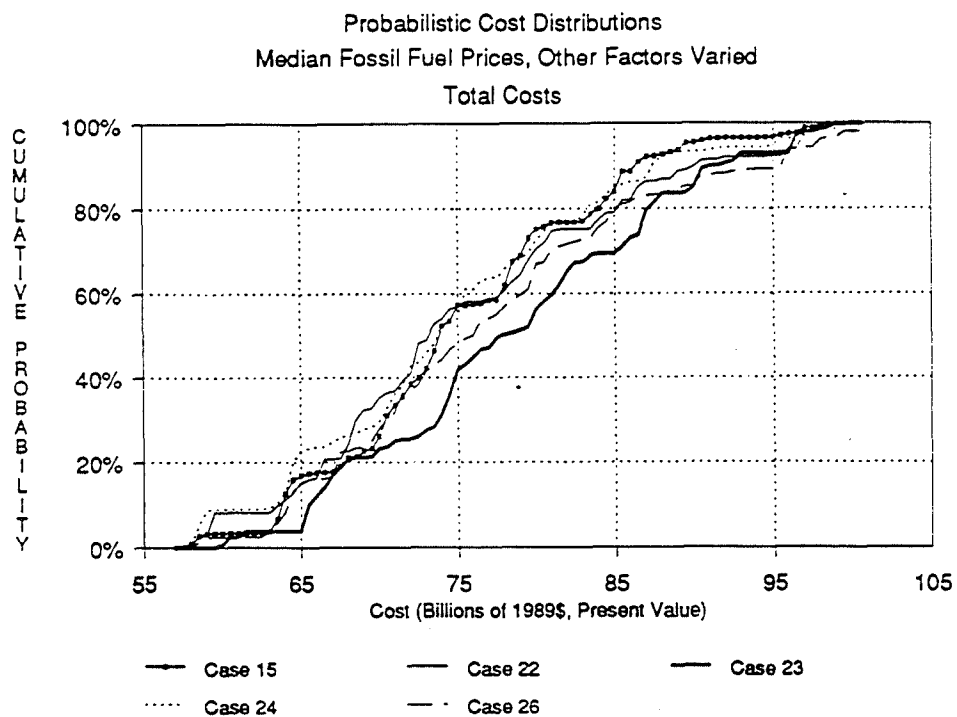


FIGURE 8.5-24

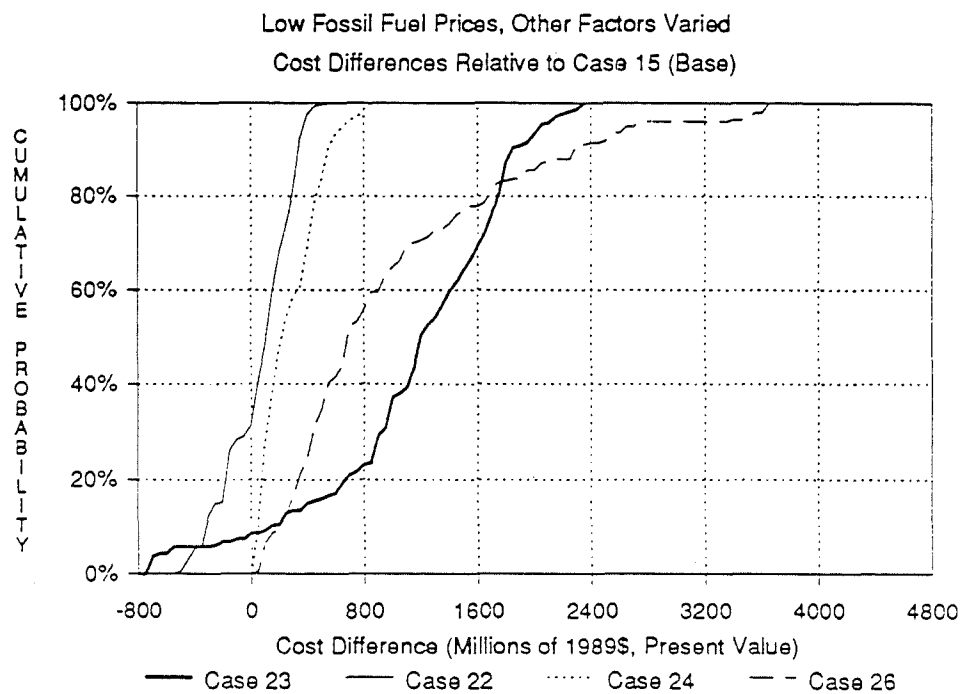
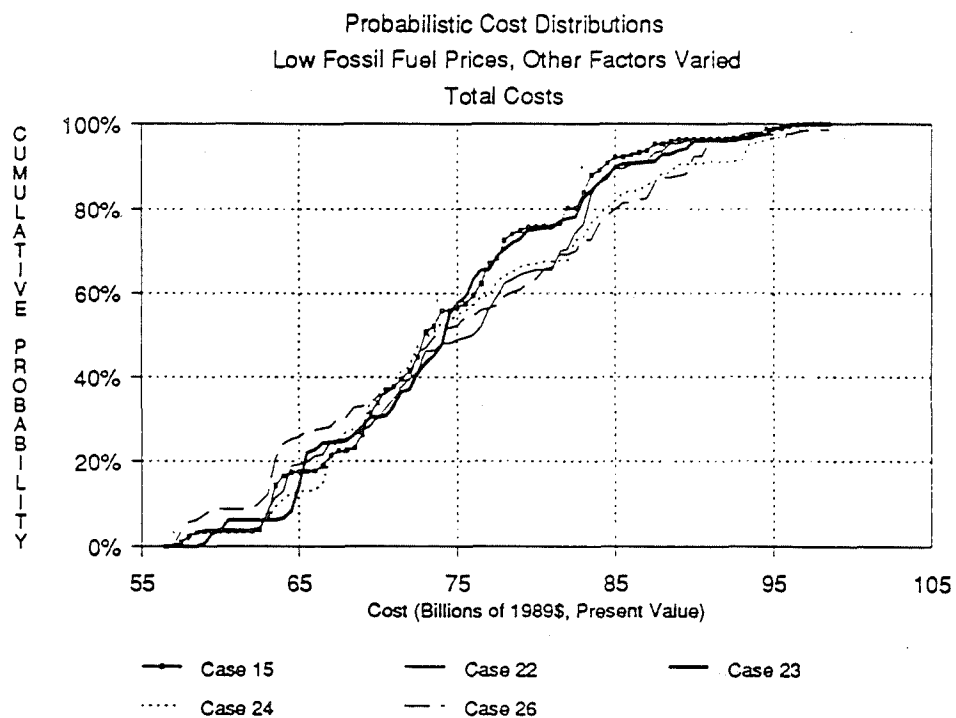
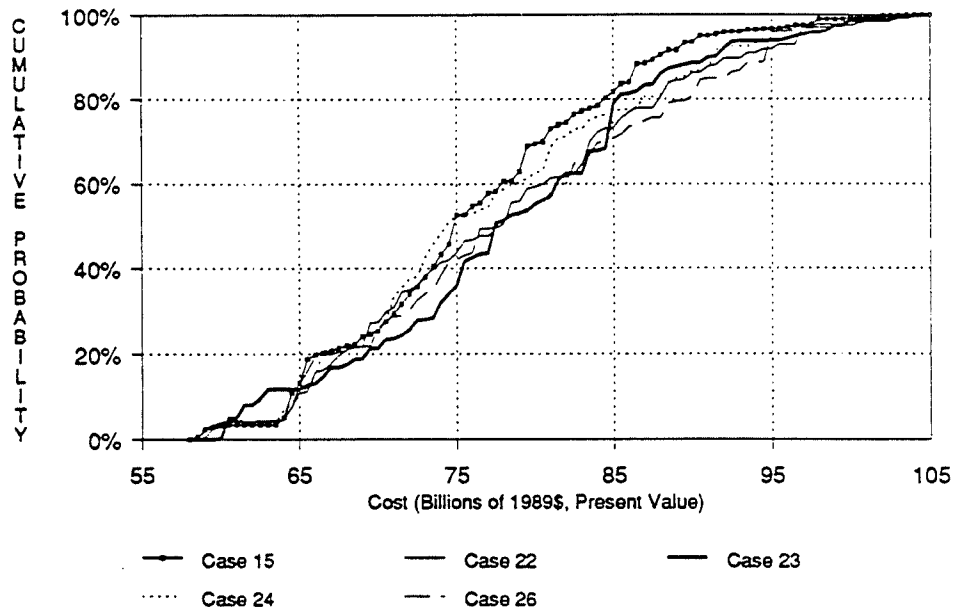


FIGURE 8.5-25

Probabilistic Cost Distributions
High Nuclear Fuel Prices, Other Factors Varied
Total Costs



High Nuclear Fuel Prices, Other Factors Varied
Cost Differences Relative to Case 15 (Base)

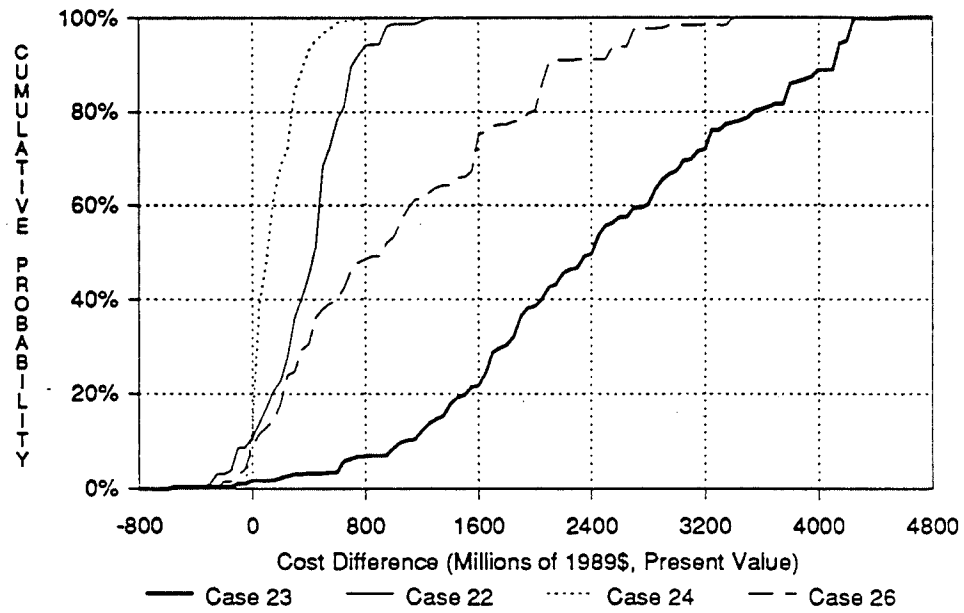


FIGURE 8.5-26

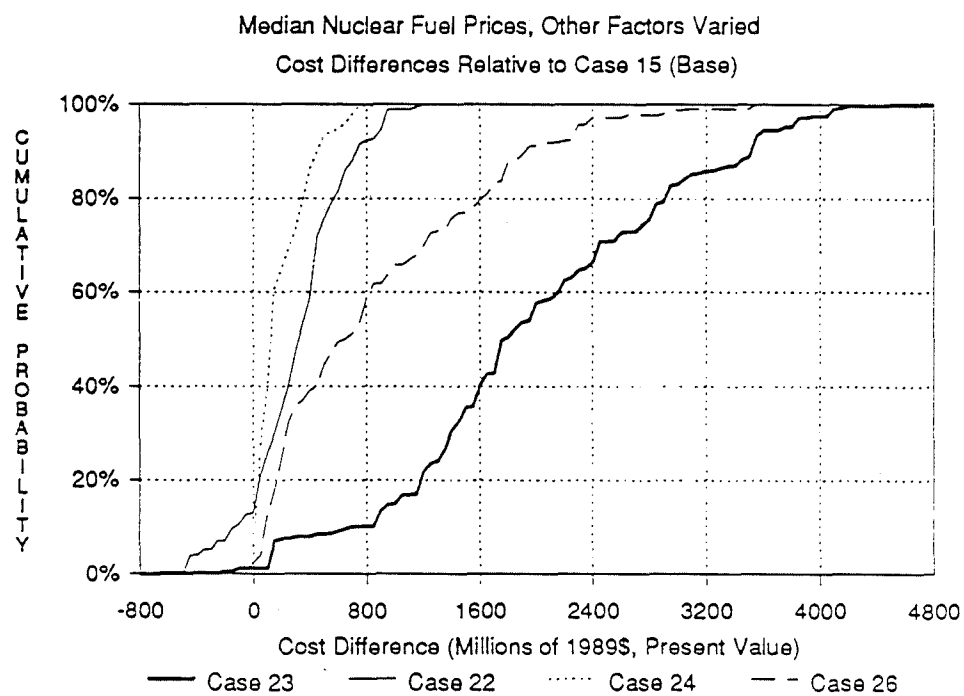
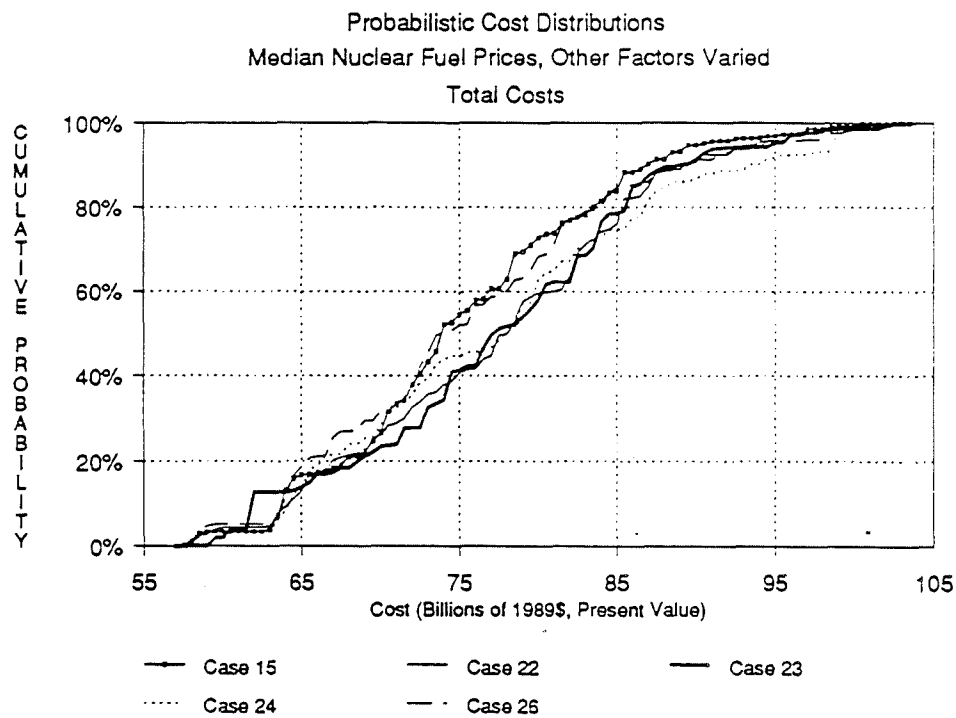


FIGURE 8.5-27

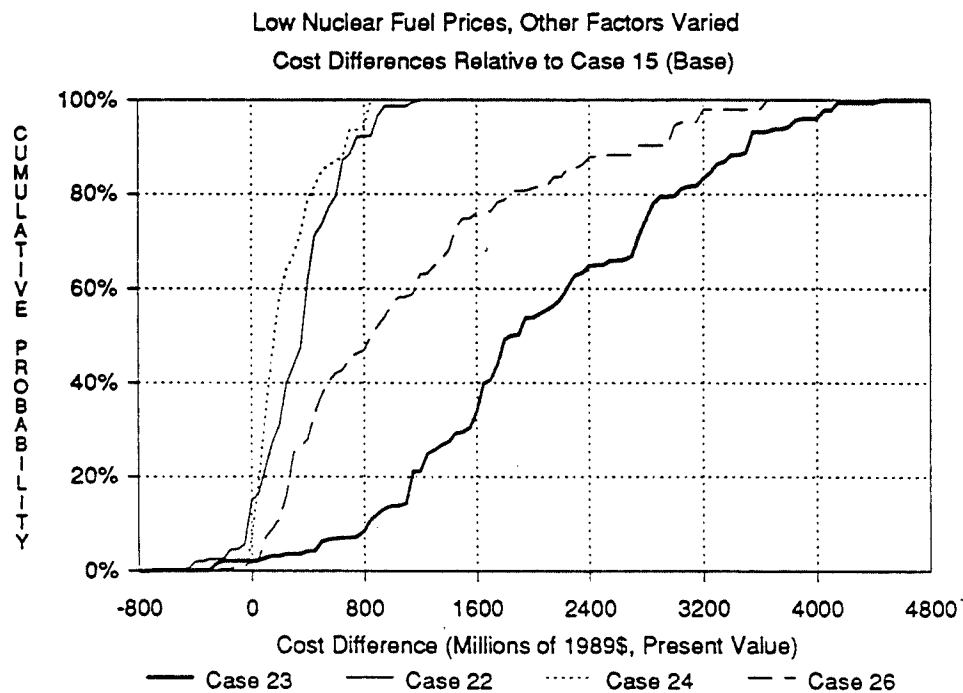
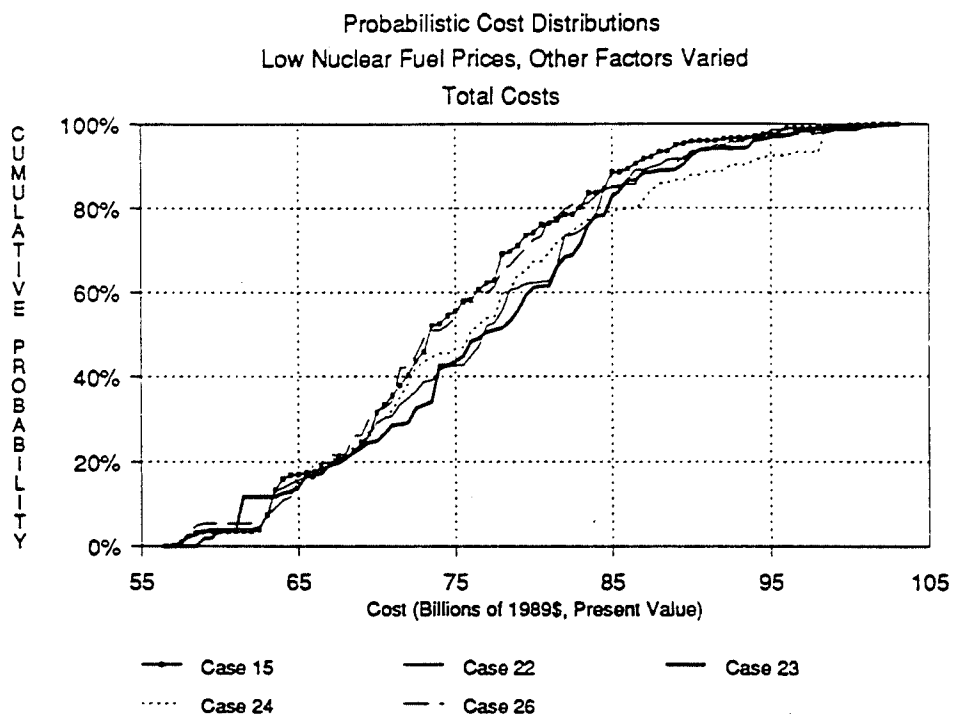


FIGURE 8.5-28

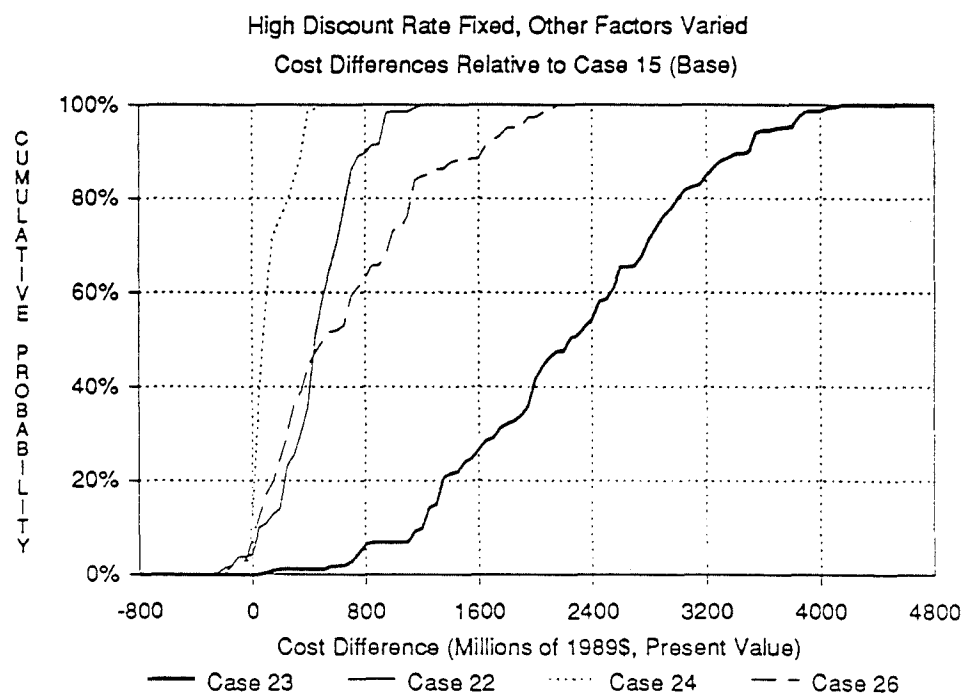
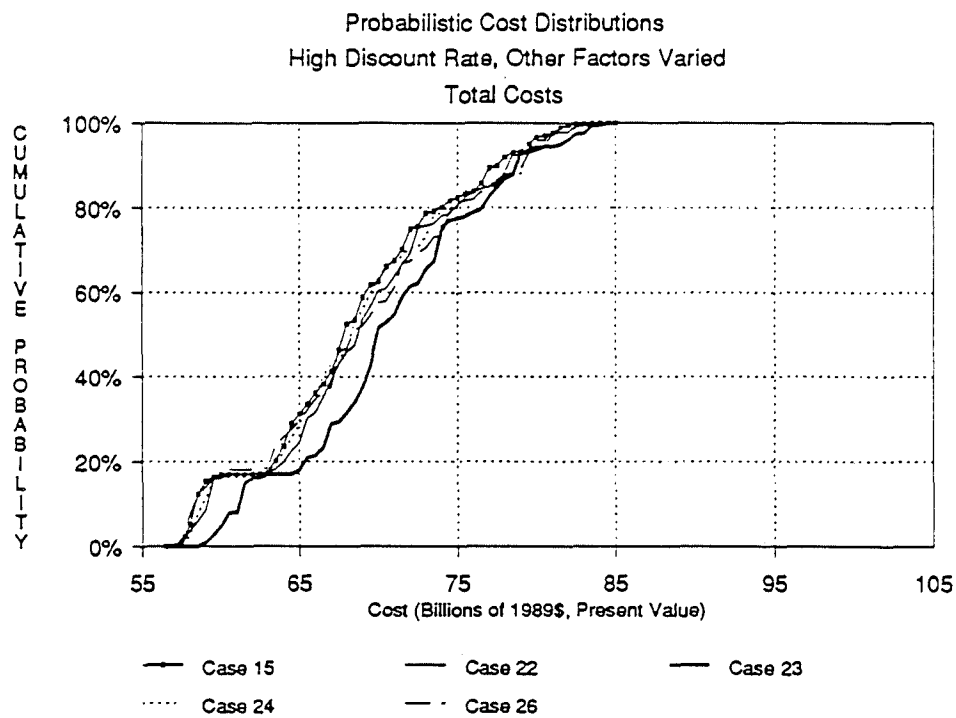


FIGURE 8.5-29

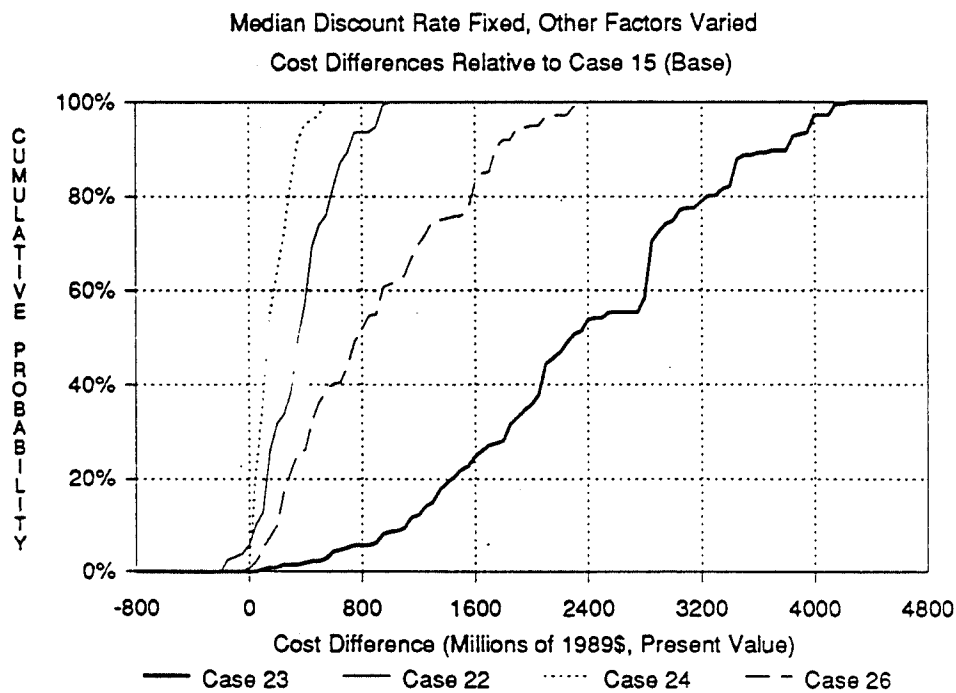
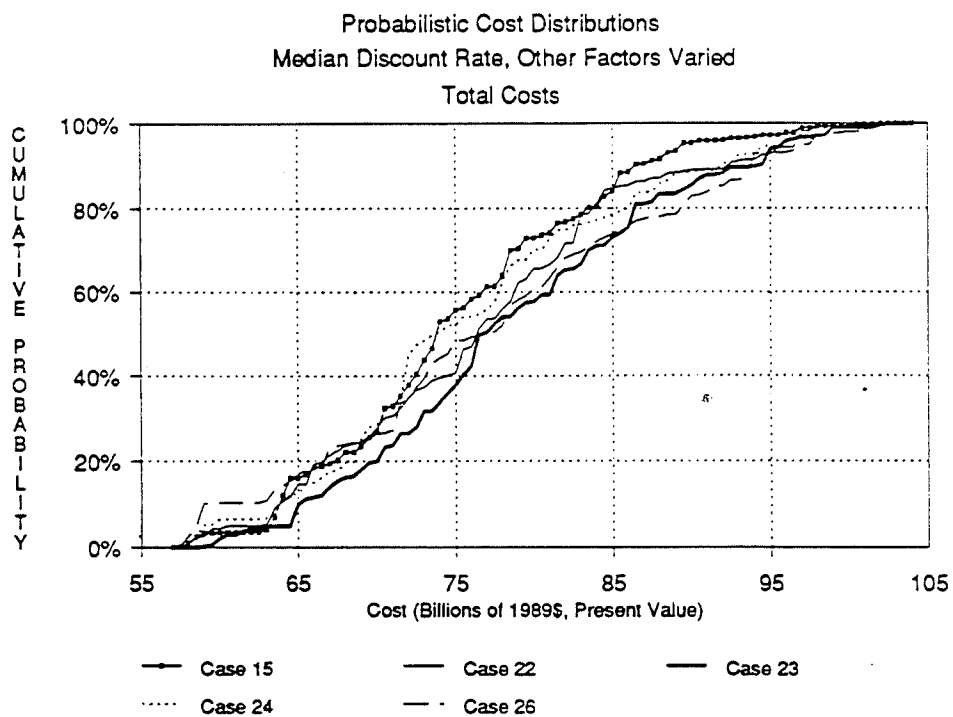


FIGURE 8.5-30

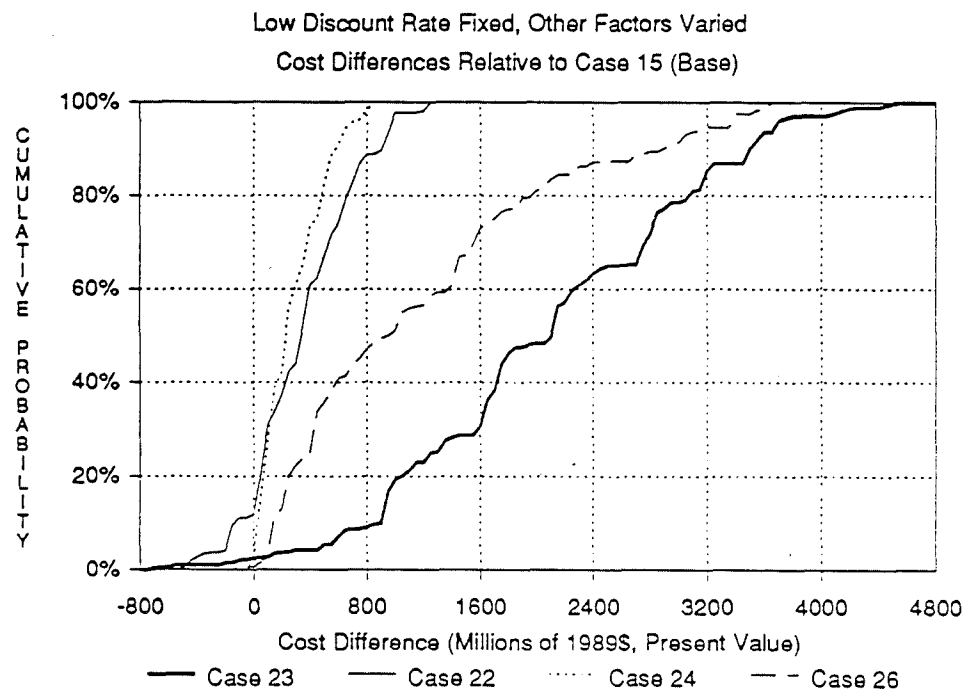
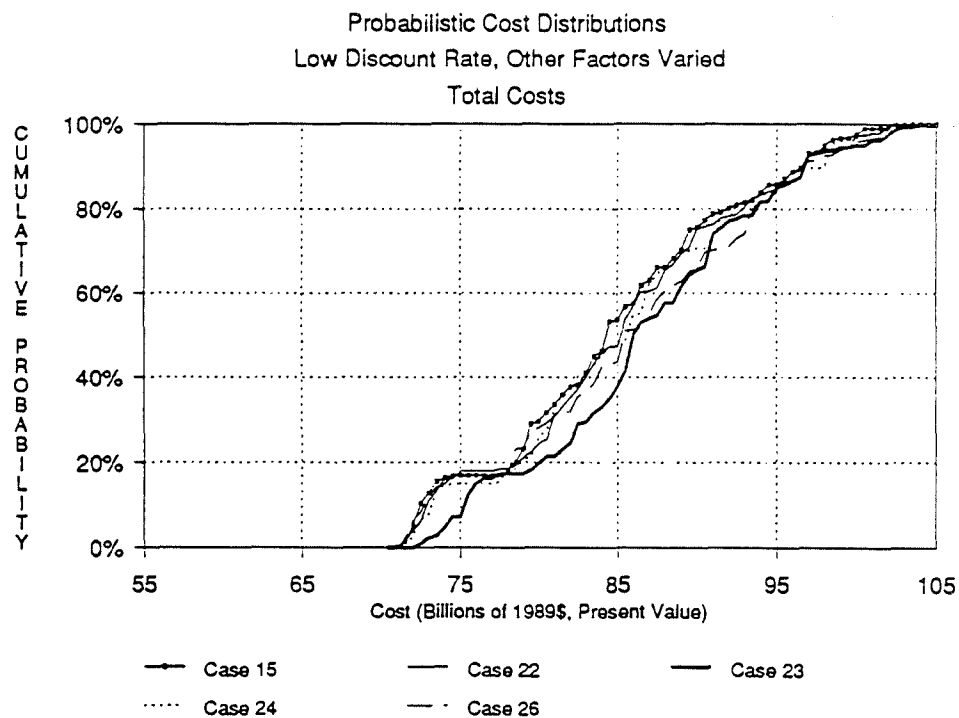


FIGURE 8.5-31

8.5.8 Taking Dependencies Into Account

Among 405 paths, there are some combinations of factors that have a lower probability than was assumed, because one factor is unlikely to lead to another--high capital costs would usually not result when discount rate are low. Conversely, some combinations have a higher probability than was assumed, because of dependency between factors. For example, both load forecast and discount rates are dependent on economic activity--hence a change in economic activity would lead to a corresponding change in both load forecast and discount rates.

Figure 8.5-32 shows how probabilities could change when dependencies are taken into account. Under upper load forecast, for example, the upper, median and lower probabilities for fossil fuel prices were assumed to change from 20/60/20 to 90/10/0. These changes were used to recalculate the expected costs. Case 15 was still cost effective when ranking the cases only their expected cost differences changed.

Figure 8.5-33 shows the distributions for the original independent probabilities (BASE) and the results when the probabilities for fossil fuel and the discount rate depend on the load forecast path. The results show the continued cost effectiveness of Case 15.

8.5.9 Summary of Risk Analysis

Figure 8.5-34 summarizes the results of the sensitivity and probabilistic analysis. The highest and lowest present value costs that occur irrespective of their probability are shown. The range between the highest and lowest shows the difference in variability within each case. The differences in the range sizes relative to Case 15 are shown. Expected cost differences relative to Case 15 and their 80% confidence band are also shown.

Illustration of Possible Dependent Probabilities for Fossil Fuel and Discount Rate

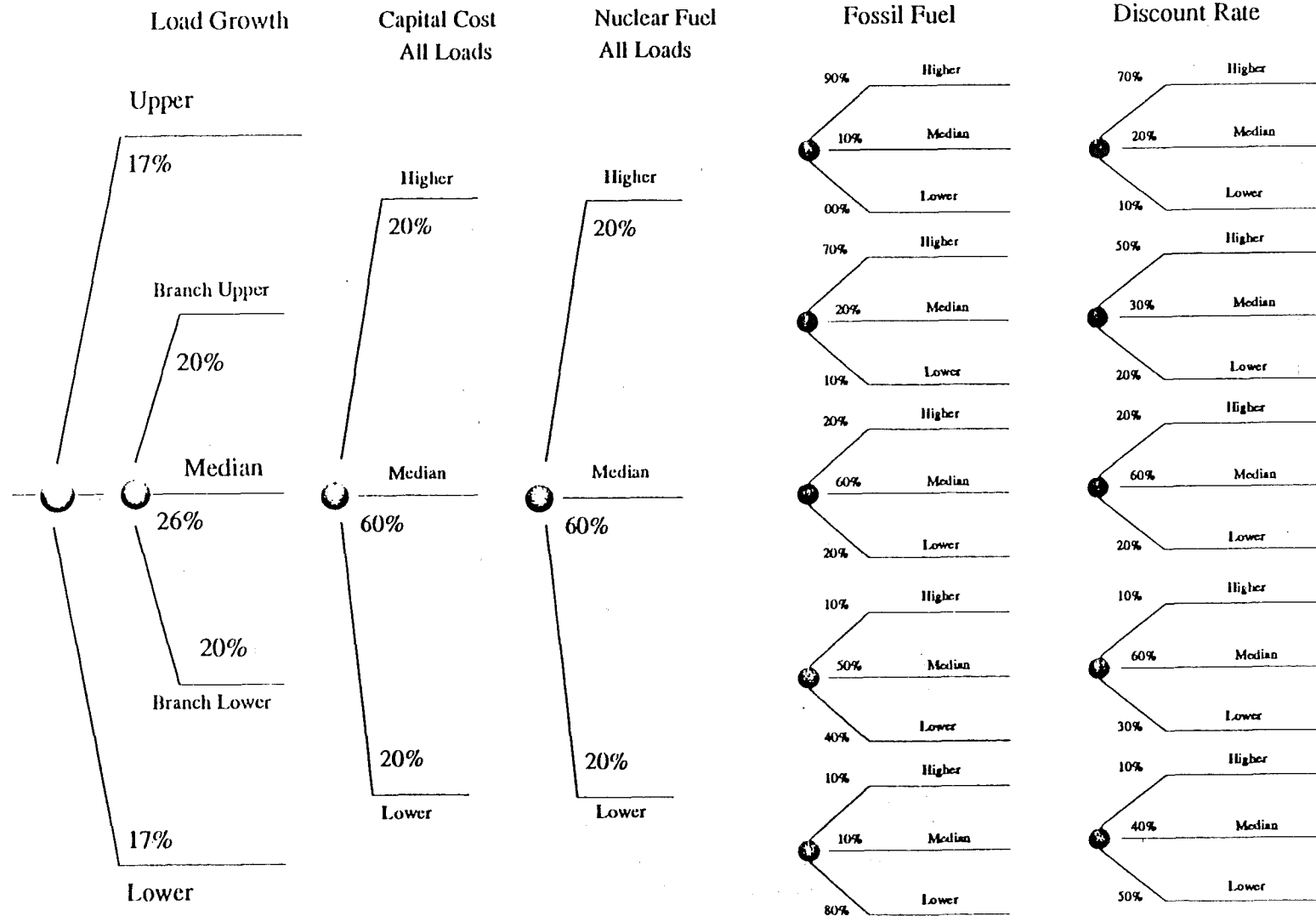


FIGURE 8.5-32

FIGURE 8.5-33
Fossil Fuel Prices and Discount Rate Interdepend on Load
Comparison to Independent Cost Difference Curves
Cost Differences Relative to Case 15 (Base)

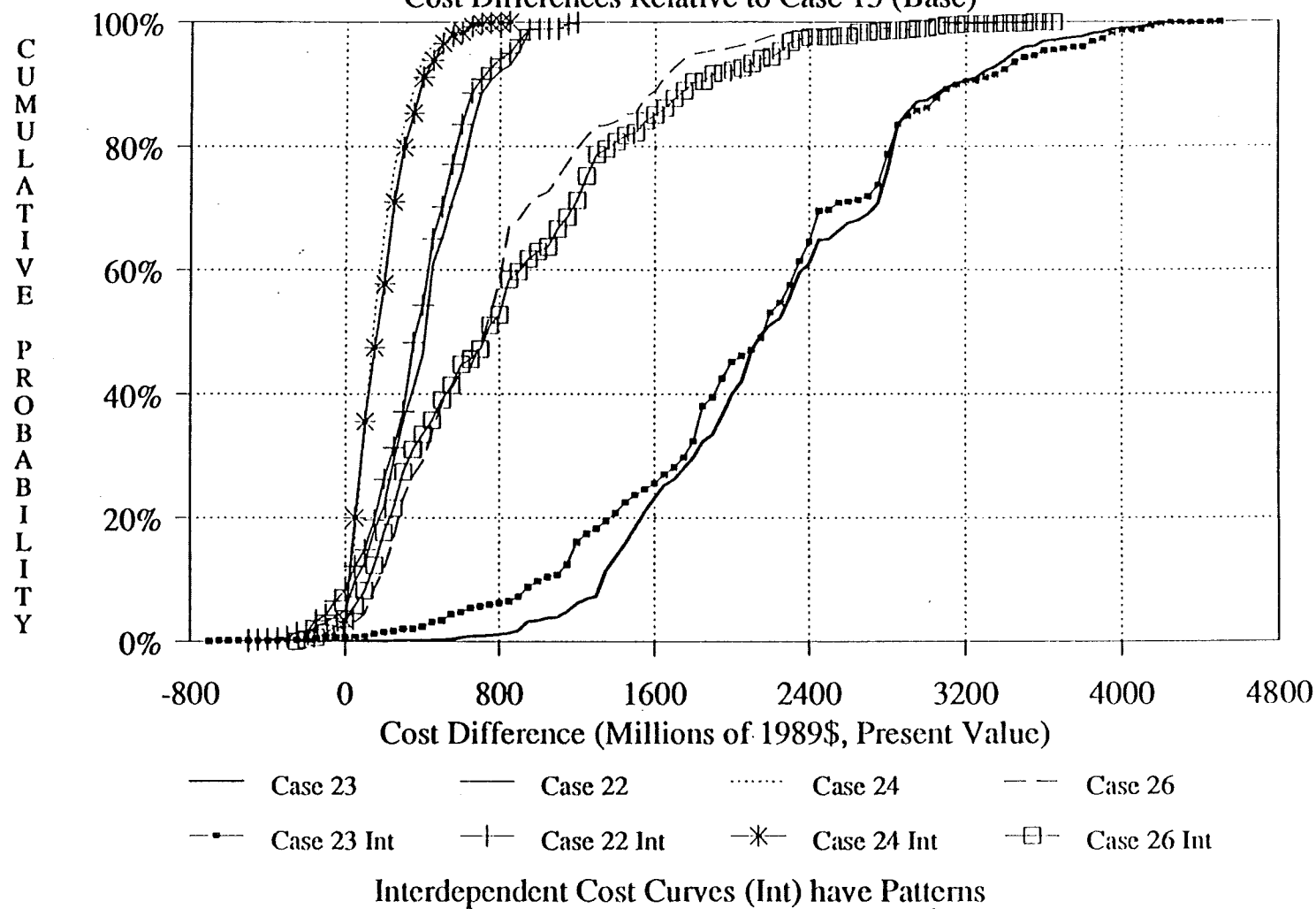


FIGURE 8.5-34

\$ Million 1989 Present Value

	<u>Case 23</u>	<u>Case 22</u>	<u>Case 15</u>	<u>Case 24</u>	<u>Case 26</u>
Highest Cost	104677	103488	103368	103908	106065
Lowest Cost	58673	57175	56914	56923	57013
Range Size	46004	46313	46454	46985	49052

Differences Relative to Case 15

Range Differences	-450	-141	BASE	531	2598
Expected Cost					
Difference	2120	365	BASE	187	857
80% Confidence Band					
for Difference	1020-3195	30-690	BASE	30-390	120-1770

While Figure 8.5-34 shows that the range of outcomes for Case 22 and Case 23 may be less than Case 15, however these cases have much higher expected costs. All Cases have a higher expected cost than Case 15. Even when examining the 80% confidence bands, the expected cost for Case 15 is less than the confidence bands of all the other Cases.

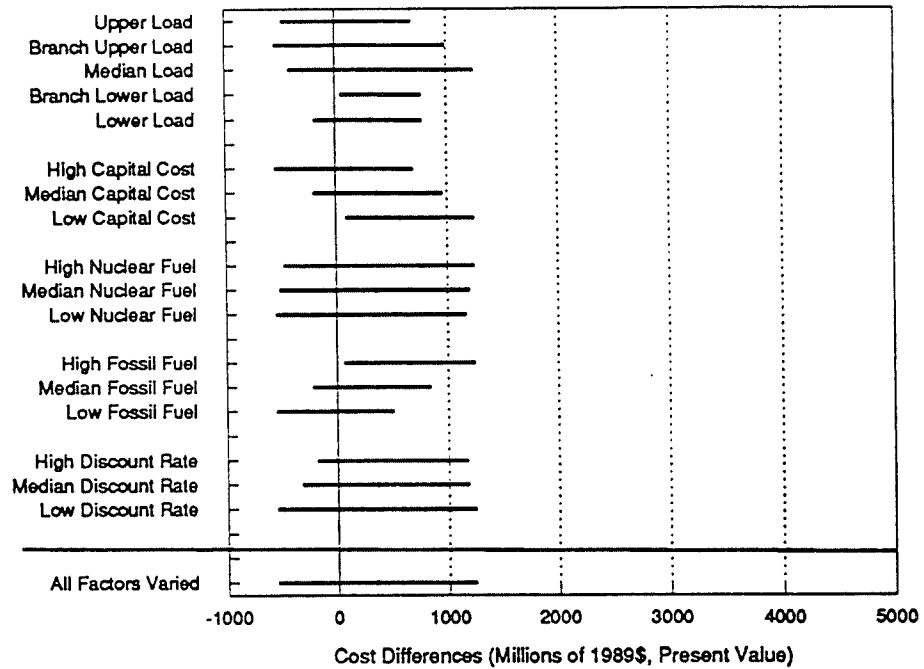
Bar charts can be used to summarize the information shown in the cumulative distribution graphs. The highest and lowest cost differences to Case 15 under each of the 17 specific conditions, outlined in 8.5.6, and the 80% confidence bands which eliminate the extreme results at each end of the ranges were plotted.

Figure 8.5-35 through Figure 8.5-38 compare the each case to Case 15 under the 17 specific conditions, while varying all the other factors. The top charts, indicating the full range of differences show that Case 15 can cost more under some combination of conditions. The lower charts for the 80% confidence band of the ranges show that the number of times when Case 15 costs more is greatly reduced. The cost penalties for Case 15, shown by the size of the few remaining ranges to the left of the 0 base line, are very small.

FIGURE 8.5-35

Full Cost Differences Between Cases 15 and 22

Highest and Lowest Present Value Costs



80% Cost Confidence Bands
Cost Differences Between Cases 15 and 22

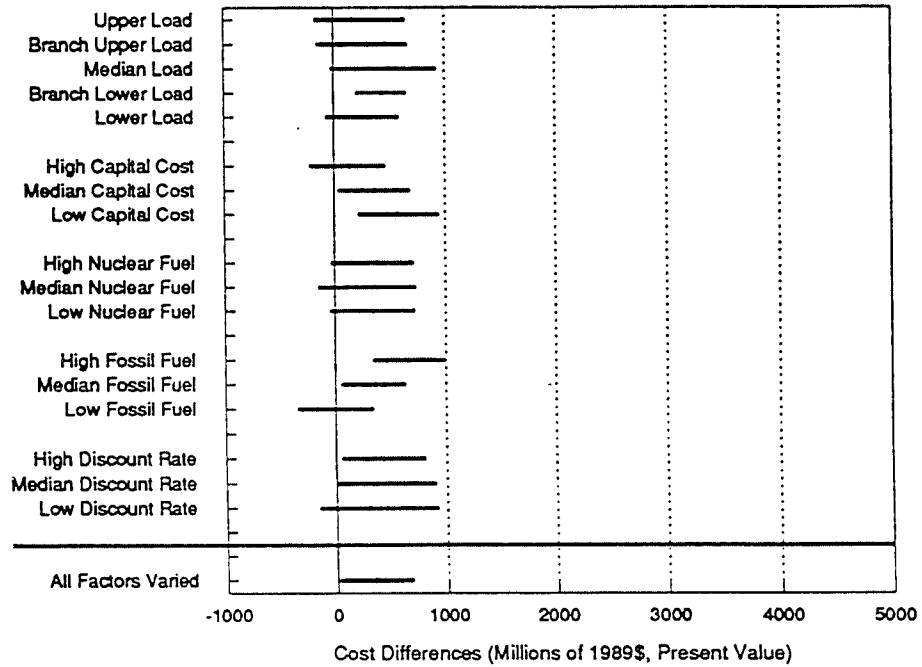


FIGURE 8.5-36

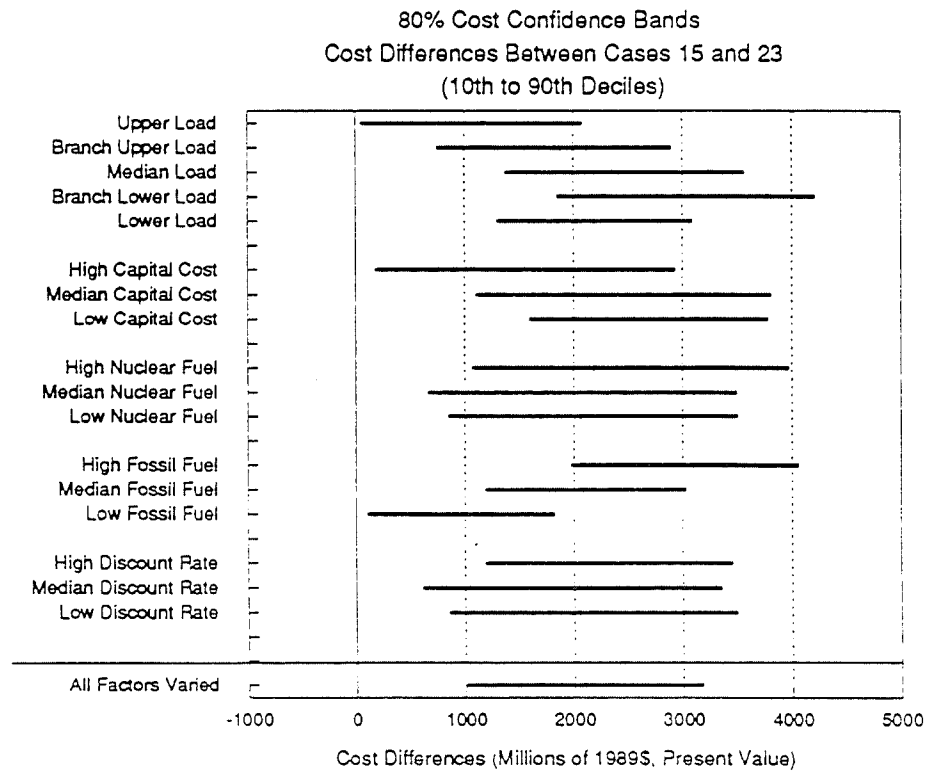
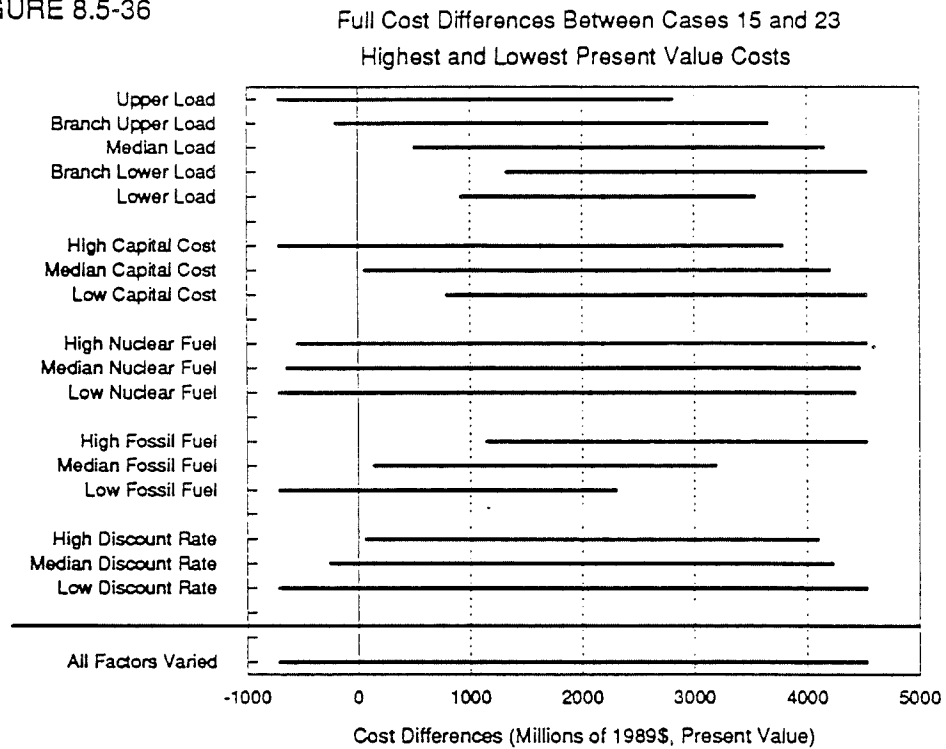
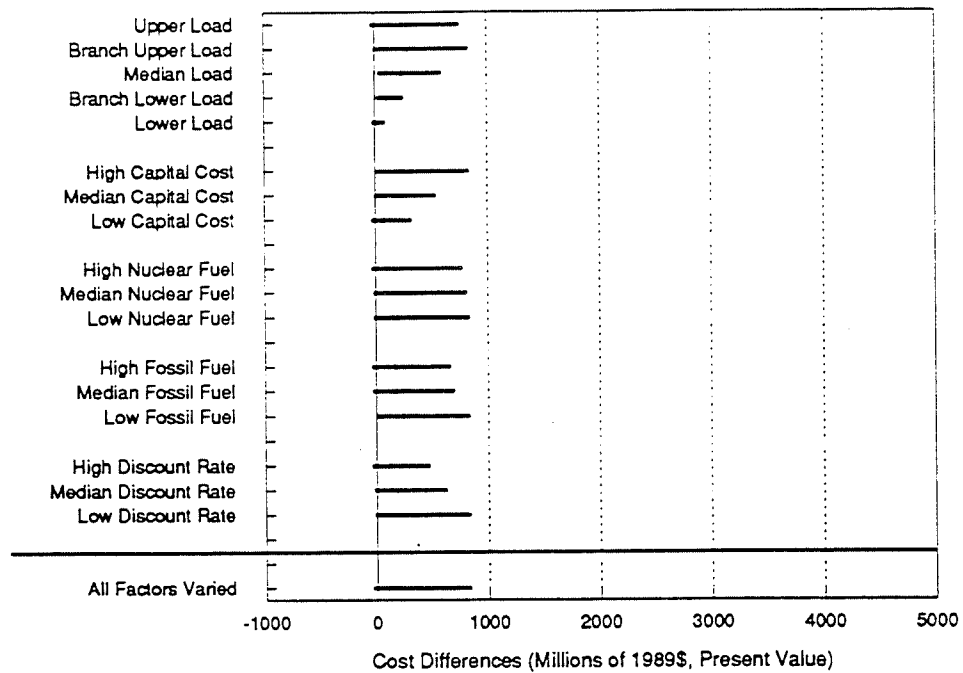


FIGURE 8.5-37

Full Cost Differences Between Cases 15 and 24
Highest and Lowest Present Value Costs



80% Cost Confidence Bands
Cost Differences Between Cases 15 and 24
(10th to 90th Deciles)

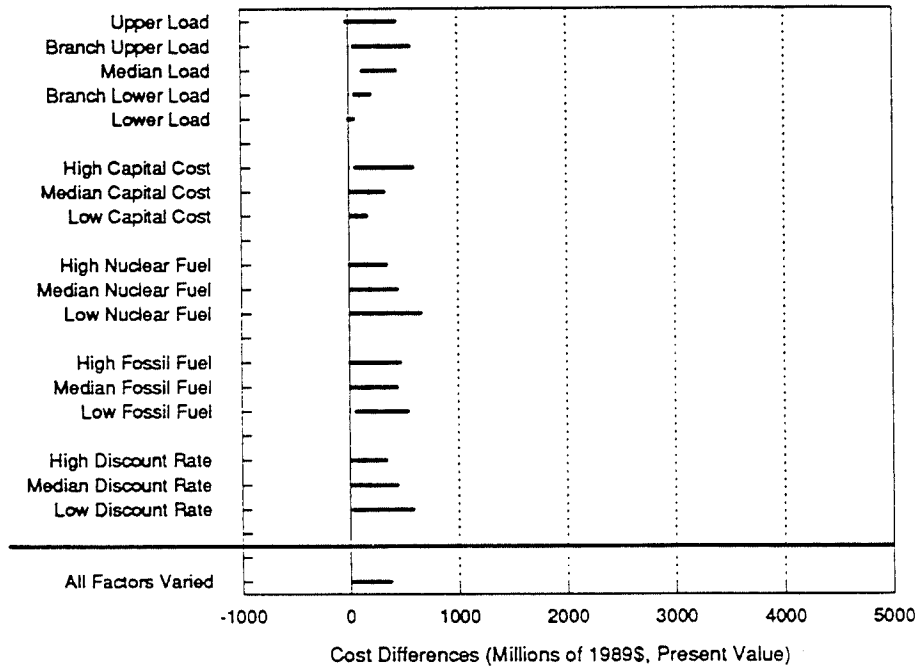
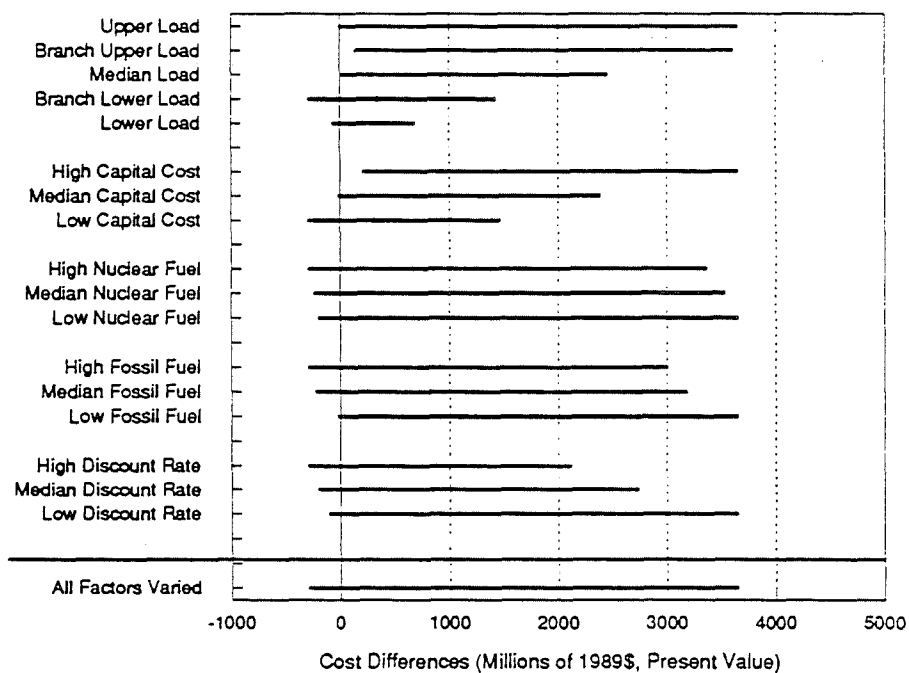
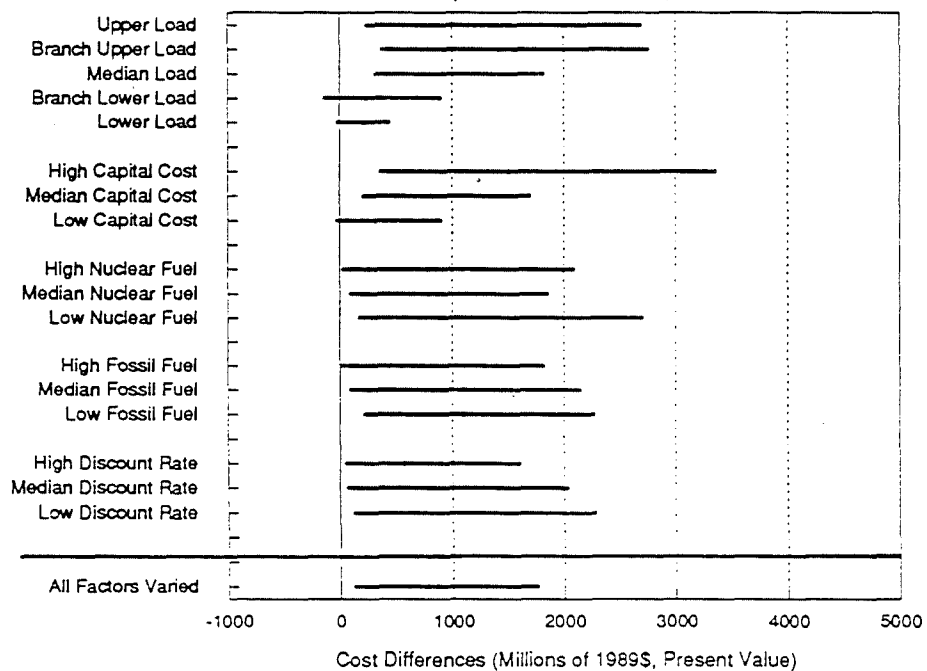


FIGURE 8.5-38

Full Cost Differences Between Cases 15 and 26
Highest and Lowest Present Value Costs



80% Cost Confidence Bands
Cost Differences Between Cases 15 and 26
(10th to 90th Deciles)



As noted previously, the probabilistic paths were modelled to their conclusion with no feedback loop to make corrections as unreasonable costs or fuel prices are experienced. The risk analysis concentrated on the results using extreme conditions, such as the estimates following their high or low values for the entire study period and linking the capital costs and the construction escalation, the uncertainty differences in the new major supply components in each case were emphasized. Case 15 continued to show its cost effectiveness under nearly all conditions and clearly resulted in the lowest expected costs.

8.6 REVIEW

For each case under each of the five load paths, there is a unique application of the Risk Assessment Model (RAM), which integrates economic values (escalation and discount rates) and cost data for the options in the supply cases.

To compare plans that have different patterns of expenditures for capital, OM&A and fuel costs, present value costs are employed. Since some options have an operating life that extends beyond the planning period, a portion of all fixed costs in some options is allocated to the study period.

Much of the cost analysis focuses on the difference in cost between plans and the decisions that drive those differences.

Since actual costs and differences between cases will likely be different than projected, Hydro determines total cost for customers under a range of conditions.

To determine what factors have the most impact on costs, Hydro examines the differences caused when individual factors are varied independently. The five factors identified as having the most impact include load forecast, capital construction costs, fossil fuel costs, nuclear fuel costs and cost of money (real discount rate).

Because of the uncertainties surrounding load growth and the major cost factors, probabilities are assigned to each of the five load paths and the lower, medium and cost estimates. Combining the three costs estimates for the key cost components with the five load forecasts produces 405 possible estimates and an equal number of present value cost outcomes. Multiplying these outcomes by their corresponding probability produces the expected cost of a case.

The total cost range of a case is presented on a cumulative probability distribution graph. Differences between one case, Case 15, and all other cases, are also presented on cumulative probability distribution graphs.

When one or all factors are varied, Case 15 is the dominant case -- it has less costly outcomes more frequently than the other cases. This did not change when Hydro took into account that some combinations of factors have a higher or lower probability than was originally assigned.

9. FINANCIAL IMPACT ASSESSMENT

9.0 INTRODUCTION

9.1 ELECTRICITY PRICES

9.2 BORROWING

9.3 FINANCIAL PERFORMANCE

9.4 REVIEW

9.0 INTRODUCTION

This chapter provides additional information on the impacts of the various Cases in the Demand/Supply Plan on electricity prices, borrowing requirements, and financial performance.

9.1 ELECTRICITY PRICES

Figure 15-52 in the Plan report illustrates the impacts on electricity prices (in percentage terms) of the various Cases, relative to Case 15, for the upper, median and lower forecasts. The values used to graph the impacts are shown in Figure 9-1.

For the first decade of the study period, there are essentially no differences in prices between the Cases (ie, price difference are generally 1% or less). From 2000 to 2009, electricity prices for Cases 22, 24 and 26 are generally within $\pm 3\%$ of Case 15. These differences are not considered significant, given the uncertainty inherent in estimating impacts 10 to 20 years in the future. The outlook is considerably less favourable under Case 23, with prices projected to be as much as 10 to 15% higher than Case 15.

Electricity prices charged to Ontario Hydro's primary customers are established so that total revenues, including revenues from secondary sales, recover costs and provide for a planned level of net income. In forecast terminology, the revenue to be collected from primary customers is called the "revenue requirement" (see formula below), and is defined as being equal to total costs, including net income, less secondary revenue.

$$\text{Revenue requirement} = \text{OM\&A} + \text{Fuel} + \text{Provincial Government levies} + \text{Depreciation} \\ + \text{Interest and foreign exchange} + \text{Net income} - \text{Secondary revenue}$$

The percentage difference in electricity price between any two Cases in a given year is equal to the percentage difference in annual revenue requirement. (This statement is only true when comparing Cases within a particular load forecast, as projected electricity prices are also affected by load.) Differences in annual revenue requirement between the various Cases and Case 15 are provided in Figure 9-2. The impacts are expressed in 1989 dollars, which are derived from nominal dollars by dividing by an inflation index (the Ontario Consumer Price Index).

Figure 9-1 Impacts on electricity prices relative to Case 15

(%)	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009
Upper																					
Case 22	0	0	0	0	0	0	0	0	0	0	1	1	2	1	1	1	1	2	2	1	0
Case 23	0	0	0	0	0	0	0	0	1	2	4	6	6	4	4	5	5	5	3	2	1
Case 24	0	0	0	1	1	1	1	1	1	0	0	0	(1)	0	(1)	(1)	(1)	(2)	(2)	(2)	(1)
Case 26	0	0	0	1	1	1	1	1	1	1	1	0	(2)	(2)	(2)	(1)	(2)	(2)	(3)	(3)	(2)
Median																					
Case 22	0	0	0	0	0	0	(1)	(1)	(1)	0	0	2	3	3	3	2	1	0	3	4	3
Case 23	0	0	0	(1)	(1)	(1)	(1)	0	0	2	5	9	10	9	10	11	11	9	7	5	2
Case 24	0	0	0	0	0	0	0	0	0	1	1	0	0	0	0	(1)	0	0	1	(1)	(2)
Case 26	0	0	0	0	0	0	0	0	0	1	1	0	(1)	(2)	(2)	(2)	(2)	(2)	(1)	(2)	(2)
Lower																					
Case 22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	4	6	5
Case 23	0	0	0	0	0	0	0	0	0	1	3	7	10	12	14	13	12	11	9	4	1
Case 24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	(1)	(2)
Case 26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	(1)	(3)	(4)

Figure 9-2 Differences in annual revenue requirements relative to Case 15

(1989\$B)	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009
Upper																					
Case 22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.1	0.1	0.1	0.1	0.2	0.2	0.1	0.0
Case 23	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.5	0.5	0.3	0.4	0.4	0.5	0.4	0.3	0.2	0.1
Case 24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	(0.1)	(0.1)	(0.1)	(0.2)	(0.2)	(0.2)	(0.1)
Case 26	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	(0.1)	(0.2)	(0.2)	(0.1)	(0.2)	(0.2)	(0.3)	(0.3)	(0.2)
Median																					
Case 22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.2	0.2	0.1	0.0	0.2	0.4	0.3
Case 23	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.6	0.7	0.7	0.8	0.9	0.9	0.7	0.6	0.4	0.2
Case 24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	(0.1)	(0.2)
Case 26	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	(0.1)	(0.2)	(0.1)	(0.2)	(0.2)	(0.1)	(0.2)	(0.2)
Lower																					
Case 22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.4	0.3
Case 23	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.4	0.6	0.8	0.9	0.9	0.8	0.7	0.6	0.3	0.1
Case 24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	(0.1)	(0.1)
Case 26	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	(0.2)	(0.3)

The components of the revenue requirement differ between Cases as a result of the different planning assumptions. The main reasons for differences in the revenue requirement components are:

- | | |
|---------------------------|--|
| OM&A | - is dependent on the quantity and type of new generating facilities in service (eg, a nuclear station has higher OM&A costs than a similarly-sized coal station) |
| Fuel | - is dependent on generation mix, which is influenced by the quantity and type of new generating facilities in service (eg, nuclear generation is less expensive than coal generation) |
| Provincial levies | - are dependent on the level of debt outstanding, which is influenced by cumulative capital expenditures and, therefore, by the quantity and type of new facilities in service or under construction (eg, a nuclear station costs more to build than a similarly-sized coal station) |
| Depreciation | - is dependent on the quantity and type of new facilities in service (eg, a nuclear station has higher depreciation than a similarly-sized coal station, as it costs more to build) |
| Interest/Foreign exchange | - reasons for differences are essentially the same as for depreciation, although differences in interest tend to diminish over time, as the remaining book value of the facilities (ie, the undepreciated cost) declines |
| Net income | - is dependent on the level of construction in progress and/or the value of assets in service, which is influenced by the quantity and type of new facilities in service or under construction (see section 9.3 on Financial Performance for a description of planned net income levels) |
| Secondary revenue | - is dependent on the amount of excess nuclear generation available for export, which is influenced by the quantity and type of new generating facilities in service (note: secondary revenues are essentially revenues from export sales) |

9.2 BORROWING

Figure 15-53 in the Plan report shows projected real annual net borrowing levels for the various Cases under upper, median and lower forecasts. The values used to graph the borrowing levels are shown in Figure 9-3. The values are expressed in 1989 dollars.

Figure 9-3 Annual Net Borrowing

(1989\$B)	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009
Upper																					
Case 15	1.1	1.6	1.1	1.2	0.8	0.9	1.1	1.2	1.2	1.4	2.2	3.3	3.4	2.7	2.5	2.2	2.8	3.4	3.7	3.5	2.6
Case 22	1.1	1.6	1.1	1.2	0.8	1.0	1.3	1.5	1.5	1.9	2.6	3.3	3.5	3.0	2.6	2.4	2.5	2.9	3.0	3.1	2.3
Case 23	1.1	1.7	1.2	1.4	1.1	1.5	2.0	2.4	2.5	2.8	3.1	3.5	3.2	2.5	2.4	2.1	2.7	3.0	3.3	3.0	2.3
Case 24	1.1	1.6	1.1	1.2	0.7	0.8	1.0	1.1	1.0	1.3	2.0	3.0	3.1	2.2	1.7	1.3	2.1	3.2	3.7	3.7	3.0
Case 26	1.1	1.6	1.1	1.1	0.7	0.8	0.9	0.8	0.5	0.5	1.0	2.1	2.8	1.9	1.4	0.7	1.2	2.3	3.2	3.2	2.5
Median																					
Case 15	1.2	1.7	1.1	0.9	0.4	0.4	0.6	0.3	0.5	0.9	1.6	2.6	3.0	2.4	1.7	1.2	1.0	1.7	2.9	3.7	3.5
Case 22	1.3	1.8	1.1	0.9	0.5	0.5	0.9	0.8	1.2	1.7	2.3	2.8	2.7	2.1	1.8	1.6	1.8	2.2	2.7	2.7	2.3
Case 23	1.3	1.8	1.2	1.2	0.8	1.1	1.6	1.8	2.2	2.7	3.1	3.4	2.8	1.9	1.4	0.8	0.9	1.6	2.7	3.2	2.8
Case 24	1.2	1.7	1.1	0.9	0.4	0.4	0.6	0.3	0.4	0.8	1.4	2.4	2.9	2.2	1.4	0.7	0.2	0.8	2.1	3.3	3.5
Case 26	1.2	1.7	1.1	0.9	0.4	0.4	0.5	0.2	0.1	0.3	0.6	1.4	2.0	1.7	1.2	0.6	0.4	0.8	2.0	3.0	2.9
Lower																					
Case 15	1.4	1.9	1.2	1.1	0.4	0.4	0.5	0.1	0.0	0.2	0.4	0.9	0.9	0.5	0.5	0.5	0.9	1.8	2.9	3.7	3.5
Case 22	1.4	1.9	1.2	1.1	0.4	0.4	0.5	0.1	0.0	0.2	0.5	1.1	1.3	1.1	1.3	1.4	1.9	2.6	3.0	3.1	2.5
Case 23	1.4	2.0	1.3	1.2	0.8	1.0	1.4	1.3	1.5	1.7	1.7	1.7	1.1	0.3	0.0	(0.2)	0.1	0.9	2.0	3.0	3.4
Case 24	1.4	1.9	1.2	1.1	0.4	0.4	0.5	0.1	0.0	0.2	0.4	0.9	0.9	0.5	0.4	0.3	0.7	1.4	2.4	3.0	2.6
Case 26	1.4	1.9	1.2	1.0	0.4	0.3	0.5	0.1	0.0	0.2	0.4	0.9	0.9	0.4	0.1	(0.2)	(0.1)	0.4	1.6	2.7	2.6

Note: A negative value for annual net borrowing generally indicates that funds from operations (primarily net income and depreciation) exceed capital expenditures, and represents a year-over-year decline in the level of debt outstanding.

Figure 9-4 Cumulative Net Borrowing

(1989\$B)	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009
Upper																					
Case 15	1.1	2.7	3.8	5.0	5.8	6.7	7.8	9.0	10.2	11.6	13.7	17.0	20.4	23.2	25.7	27.9	30.6	34.0	37.8	41.3	43.9
Case 22	1.1	2.8	3.9	5.1	5.9	6.9	8.2	9.7	11.2	13.1	15.6	19.0	22.5	25.5	28.0	30.4	32.9	35.8	38.8	41.9	44.3
Case 23	1.1	2.8	4.0	5.4	6.5	8.0	10.0	12.4	14.9	17.7	20.7	24.2	27.4	29.9	32.3	34.4	37.1	40.1	43.4	46.4	48.7
Case 24	1.1	2.7	3.8	5.0	5.7	6.5	7.6	8.7	9.7	11.0	12.9	16.0	19.1	21.3	23.1	24.4	26.5	29.7	33.4	37.2	40.2
Case 26	1.1	2.7	3.8	4.9	5.6	6.4	7.3	8.0	8.5	9.0	10.0	12.1	14.7	16.6	18.0	18.7	19.9	22.2	25.4	28.5	31.0
Median																					
Case 15	1.2	3.0	4.1	5.0	5.5	5.9	6.5	6.8	7.3	8.2	9.8	12.4	15.3	17.7	19.4	20.6	21.6	23.3	26.2	29.9	33.4
Case 22	1.3	3.0	4.1	5.1	5.5	6.1	7.0	7.8	9.0	10.6	12.9	15.8	18.4	20.5	22.3	23.9	25.7	27.9	30.6	33.3	35.6
Case 23	1.3	3.1	4.3	5.4	6.3	7.4	9.0	10.8	13.0	15.6	18.7	22.1	24.9	26.7	28.1	28.9	29.8	31.4	34.0	37.2	40.0
Case 24	1.2	3.0	4.1	5.0	5.5	5.9	6.5	6.7	7.2	8.0	9.4	11.8	14.7	16.9	18.3	18.9	19.2	20.0	22.1	25.4	28.9
Case 26	1.2	3.0	4.0	4.9	5.3	5.7	6.3	6.4	6.6	6.8	7.5	8.8	10.8	12.6	13.8	14.4	14.9	15.7	17.7	20.7	23.6
Lower																					
Case 15	1.4	3.3	4.5	5.6	6.0	6.4	6.9	7.0	7.0	7.2	7.6	8.5	9.4	10.0	10.5	11.0	11.9	13.7	16.6	20.3	23.8
Case 22	1.4	3.3	4.6	5.6	6.1	6.4	6.9	7.0	7.0	7.2	7.7	8.8	10.0	11.1	12.4	13.8	15.7	18.3	21.3	24.4	26.8
Case 23	1.4	3.4	4.7	5.9	6.7	7.6	9.0	10.3	11.8	13.5	15.1	16.9	18.0	18.3	18.2	18.0	18.1	19.1	21.1	24.1	27.5
Case 24	1.4	3.3	4.5	5.6	6.0	6.4	6.9	7.0	7.0	7.2	7.6	8.5	9.4	9.9	10.3	10.6	11.3	12.7	15.1	18.0	20.6
Case 26	1.4	3.3	4.5	5.5	5.9	6.2	6.7	6.8	6.8	6.9	7.4	8.2	9.1	9.5	9.6	9.3	9.2	9.7	11.2	13.9	16.5

Borrowing levels are expected to peak around the year 2000 and again around 2008, corresponding to the need for major new generating facilities. Annual real net borrowing levels for the various cases are generally within $\pm \$1.5$ billion of those for Case 15.

Real cumulative net borrowing levels over the twenty-year planning period are provided in Figure 9-4. Cumulative borrowings are highest for those Cases having the most nuclear generation, and lowest for those Cases using the most fossil generation, as the capital cost of nuclear generation is higher than that for fossil.

The differences in cumulative real net borrowings between the various Cases and Case 15 over the period to 2009 are:

	<u>Upper</u>		<u>Median</u>		<u>Lower</u>	
	<u>(1989\$B)</u>	<u>(%)</u>	<u>1989\$B)</u>	<u>(%)</u>	<u>(1989\$B)</u>	<u>(%)</u>
Case 22	0.4	1	2.2	7	3.0	13
Case 23	4.8	11	6.6	20	3.7	16
Case 24	(3.7)	(8)	(4.5)	(13)	(3.2)	(13)
Case 26	(12.9)	(29)	(9.8)	(29)	(7.3)	(31)

Real annual gross borrowing levels (net borrowing plus debt retirement) are shown in Figure 9-5. While the various Cases provide a wide range of borrowing requirements, gross annual borrowings have peak requirements that range up to twice current levels (ie, \$6 billion vs \$3 billion). In years when borrowing requirements are high, Ontario Hydro may have to obtain funds at interest rates closer to the upper range considered in the cost confidence analysis, and may have to accept foreign exchange risk.

9.3 FINANCIAL PERFORMANCE

Figure 15-54 in the Plan report illustrates Ontario Hydro's projected debt ratios for the various Cases under upper, median and lower forecasts. The debt ratio measures the extent to which assets are financed by debt, and is defined as:

$$\text{Debt ratio} = \frac{\text{Debt}}{\text{Debt} + \text{Equity}}$$

The values used to graph the debt ratios are presented in Figure 9-6.

Figure 9-5 Annual Gross Borrowing

(1989\$B)	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009
Upper																					
Case 15	2.9	3.6	2.7	2.9	2.9	2.9	2.8	2.9	2.5	3.1	3.9	5.4	5.5	4.5	4.3	4.5	5.3	5.9	6.0	6.2	5.5
Case 22	2.9	3.6	2.7	2.9	2.9	3.0	3.0	3.2	2.8	3.6	4.4	5.6	5.6	4.9	4.5	4.8	5.2	5.5	5.5	6.0	5.4
Case 23	2.9	3.8	2.8	3.1	3.2	3.5	3.7	4.2	3.9	4.6	5.0	5.9	5.7	4.8	4.7	4.8	5.6	5.8	5.9	6.1	5.6
Case 24	2.9	3.8	2.7	2.9	2.9	2.8	2.7	2.8	2.3	3.0	3.7	5.2	5.2	4.0	3.5	3.5	4.6	5.6	5.8	6.1	5.6
Case 26	2.9	3.6	2.6	2.9	2.8	2.7	2.6	2.5	1.6	2.2	2.7	4.2	4.5	3.5	2.9	2.6	3.3	4.4	5.0	5.2	4.5
Median																					
Case 15	3.0	3.9	2.7	2.7	2.6	2.5	2.3	2.1	1.7	2.5	3.3	4.6	4.8	3.8	3.3	3.1	3.2	3.7	4.8	5.9	5.9
Case 22	3.0	3.9	2.7	2.7	2.6	2.6	2.6	2.6	2.4	3.3	4.0	5.0	4.7	3.8	3.5	3.8	4.2	4.3	4.7	5.2	5.1
Case 23	3.0	4.0	2.8	2.9	3.0	3.1	3.4	3.6	3.5	4.4	5.0	5.7	5.1	3.9	3.6	3.4	3.7	4.1	5.0	5.9	5.6
Case 24	3.0	3.9	2.7	2.7	2.6	2.5	2.3	2.0	1.7	2.4	3.1	4.4	4.7	3.7	2.9	2.6	2.4	2.8	3.9	5.4	5.7
Case 26	3.0	3.9	2.7	2.6	2.5	2.4	2.2	1.9	1.3	1.9	2.3	3.4	3.8	3.1	2.6	2.3	2.3	2.5	3.6	4.8	4.9
Lower																					
Case 15	3.1	4.1	2.8	2.8	2.6	2.4	2.3	1.9	1.2	1.8	2.2	3.0	2.7	1.9	1.8	2.1	2.6	3.2	4.1	5.3	5.3
Case 22	3.1	4.1	2.8	2.8	2.6	2.4	2.3	1.9	1.2	1.8	2.2	3.1	3.1	2.5	2.6	3.1	3.7	4.1	4.4	4.9	4.6
Case 23	3.1	4.2	2.9	3.0	2.9	3.0	3.2	3.1	2.8	3.4	3.6	4.1	3.3	2.1	1.8	2.0	2.3	2.8	3.8	5.0	5.5
Case 24	3.1	4.1	2.8	2.8	2.6	2.4	2.3	1.9	1.2	1.8	2.1	3.0	2.7	1.9	1.7	1.9	2.4	2.8	3.5	4.5	4.4
Case 26	3.1	4.1	2.8	2.7	2.5	2.4	2.2	1.9	1.2	1.8	2.1	2.9	2.7	1.7	1.4	1.4	1.6	1.8	2.7	4.1	4.2

Figure 9-6 Debt Ratio

	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009
Upper																					
Case 15	0.81	0.81	0.80	0.80	0.79	0.79	0.78	0.78	0.78	0.78	0.79	0.79	0.80	0.80	0.80	0.80	0.81	0.81	0.81	0.81	0.81
Case 22	0.81	0.81	0.80	0.80	0.79	0.79	0.79	0.79	0.79	0.79	0.79	0.80	0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
Case 23	0.81	0.81	0.80	0.80	0.80	0.79	0.80	0.80	0.80	0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
Case 24	0.81	0.81	0.80	0.80	0.79	0.78	0.78	0.78	0.78	0.78	0.78	0.79	0.80	0.80	0.80	0.80	0.80	0.81	0.81	0.81	0.81
Case 26	0.81	0.81	0.80	0.80	0.79	0.78	0.78	0.78	0.77	0.77	0.76	0.77	0.78	0.78	0.78	0.78	0.78	0.78	0.79	0.80	0.80
Median																					
Case 15	0.82	0.81	0.81	0.81	0.80	0.79	0.79	0.78	0.77	0.77	0.77	0.78	0.79	0.79	0.79	0.79	0.79	0.79	0.80	0.80	0.81
Case 22	0.82	0.81	0.81	0.81	0.80	0.79	0.79	0.79	0.78	0.79	0.79	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.80	0.81	0.81
Case 23	0.82	0.81	0.81	0.81	0.81	0.80	0.80	0.80	0.80	0.81	0.81	0.81	0.81	0.81	0.81	0.80	0.80	0.80	0.80	0.80	0.80
Case 24	0.82	0.81	0.81	0.81	0.80	0.79	0.79	0.78	0.77	0.77	0.77	0.78	0.79	0.79	0.79	0.79	0.78	0.78	0.78	0.79	0.80
Case 26	0.82	0.81	0.81	0.81	0.80	0.79	0.79	0.78	0.77	0.76	0.76	0.76	0.77	0.77	0.77	0.77	0.76	0.76	0.77	0.78	0.79
Lower																					
Case 15	0.82	0.82	0.82	0.82	0.82	0.81	0.80	0.79	0.78	0.78	0.77	0.77	0.77	0.76	0.76	0.76	0.75	0.76	0.77	0.78	0.79
Case 22	0.82	0.82	0.82	0.82	0.82	0.81	0.80	0.79	0.78	0.78	0.77	0.77	0.77	0.77	0.77	0.77	0.78	0.79	0.79	0.80	0.80
Case 23	0.82	0.82	0.82	0.83	0.82	0.82	0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.80	0.79	0.78	0.77	0.77	0.77	0.78	0.79
Case 24	0.82	0.82	0.82	0.82	0.82	0.81	0.80	0.79	0.78	0.78	0.77	0.77	0.77	0.76	0.76	0.75	0.75	0.75	0.76	0.78	0.78
Case 26	0.82	0.82	0.82	0.82	0.82	0.81	0.80	0.79	0.78	0.78	0.77	0.77	0.77	0.76	0.75	0.74	0.73	0.73	0.74	0.75	0.76

The debt ratios in Figure 9-6 are based on Hydro's existing net income policy, which is currently under review. Under the existing policy, the target level of net income is based on a split interest coverage formula, and in a given year is equal to 5% of interest charged to operations (ie, net interest), plus 50% of interest capitalized. For the purposes of long-term planning, net income is established as the greater of the above interest coverage target or the statutory debt retirement (SDR) appropriation. (The SDR appropriation, as defined under the provisions of the Power Corporation Act, is the amount required to accumulate, on a sinking fund basis over 40 years, with interest at 4% per year, a sum sufficient to retire an amount of debt equal to the value of fixed assets in service.)

In general, all of Ontario Hydro's financial performance indicators do not vary significantly between the Cases. Hydro's net income policy was designed to maintain satisfactory financial performance under different planning assumptions. For all the Cases, the debt ratio is expected to remain in the 0.75 to 0.81 range throughout most of the next 20 years, rising slightly whenever major new generating stations near completion. A comparison of debt ratios between Cases generally reflects similar trends to those of borrowing levels (ie, Cases having higher borrowing levels also have higher debt ratios).

9.4 REVIEW

The projected outlooks for electricity prices over the next twenty years for Cases 22, 24 and 26 are not significantly different from that for Case 15. The outlook is considerably less favourable under Case 23.

Borrowing levels vary considerably between Cases, with cumulative borrowing being highest for those Cases having the most nuclear generation. Ontario Hydro's debt ratio and other financial performance indicators remain at satisfactory levels under all the Cases.

